JAIPUR METRO RAIL CORPORATION LIMITED

Bidding Document: Contract ICB No.JP/EW/1C(Underground)/03

Contract ICB No.JP/EW/1C(Underground)/03: "Design and Construction of Twin Tunnel by Shield TBM, Underground Station (Ramganj Chaupar), Cut and Cover Tunnel Box and Underground Ramp from Badi Chaupar dead end Ch:10387.860 to Underground ramp end Ch:13040 of Jaipur Metro Phase-1C including Entry Exit Structures, Architectural finishing, water supply, Sanitary Installations and Drainage Works at Jaipur, Rajasthan, India.

SN	Bidding Document	Page No	Clause	Addendum/	Remarks
			No/Item No	Corrigendum	
1.	Volume-1 of 7: Notice	5	Clause: 1.1.2	Last Date of Bid	Replace Page 5
	Inviting Bid (NIB)		Key Details	Submission and	with 5 R1
				Opening is revised as	
				09.08.2023 (18:00 Hrs) and	
				10.08.2023 (16:00Hrs)	
				respectively.	
2.	Volume-1 of 7:	10	C 5.4(c)	Clause-C 5.4(c) is	Replace Page
	Instructions to Bidders			modified.	10 with 10 R1
	(ITB):				
3.	Volume-1 of 7:	12	C 12.3	Clause- C 12.3 is	Replace Page
	Instructions to Bidders			modified.	12 with 12 R1
	(ITB):				
4.	Volume-1 of 7:	13	C 14.1	Clause- C 14.1 is	Replace Page
	Instructions to Bidders			modified.	13 with 13 R1
5.	(ITB): Volume-1 of 7:	23	E 5.4	Clause- E 5.4 is Deleted.	Replace Page
5.	Instructions to Bidders	25	E J.4	Clause- E 3.4 is Deleteu.	23with 23 R1
	(ITB):				25 WITH 25 KI
6.	Volume-1 of 7:	41-42	Annexure-6	Annexure-6	Replace Page
	Instructions to Bidders			Is modified.	41-42 with 41
	(ITB):				R1 to 42 R1
7.	Volume-1 of 7:	46, 48	Annexure-7	Annexure-7	Replace Page
	Instructions to Bidders			Is modified.	46 and 48 with
	(ITB):				46 R1 and 48
					R1
8.	Volume-1 of 7:	51	Annexure-7A	Annexure-7A	Replace Page
	Instructions to Bidders			Is modified.	51 with 51 R1
9.	(ITB): Volume-1 of 7:	56	Annexure-7C	Annexure-7C	Replace Page
J.	Instructions to Bidders		Annexule-/C	Is modified.	56 with 56 R1
	(ITB):				
10.		57-58	Annexure-7D	Annexure-7D	Replace Page
	Instructions to Bidders			Is modified.	57-58 with 57
	(ITB):	Co			R1 to 58 R1

ADDENDUM/ CORRIGENDUM No.1 Summary Sheet

ICB No: Contract JP/ //1c/Underground)/03:Addendum/Corrigendum-01

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SN	Bidding Document	Page No	Clause	Addendum/	Remarks
			No/Item No	Corrigendum	
11.	Volume-1 of 7:	48-49	Appendix-30	Appendix-30	Replace Page
	Form of Bid(FOB):			Is modified.	48-49 with 48
					R1 to 49 R1
12.	Volume-2 of 7:	3	Clause 2	Clause 2	Replace Page 3
	Special Conditions of		Sub-Clause-3.2	Sub-Clause-3.2 Is	with 3R1
	Contract (SCC)			modified.	
13.	Volume-2 of 7:	4-5	Clause 6	Clause 6	Replace Page 4-
	Special Conditions of		Sub-Clause-	Sub-Clause-4.11	5 with 4 R1 to 5
	Contract (SCC)		4.11	Is modified.	R1
14.	Volume-2 of 7:	19	Schedule-1	Schedule-1	Replace Page
	Special Conditions of			Is modified.	19 with 19R1
	Contract (SCC)				
15.	Volume-2 of 7:	22-23	Schedule-2	Schedule-2	Replace Page
	Special Conditions of			Is modified.	22-23 with 22
	Contract (SCC)				R1 to 23 R1
16.	Volume-2 of 7:	15-16	Clause-4.2	Clause-4.2	Replace Page
	General Conditions of		Sub Clause-	Sub Clause-4.2.1	15-16 with 15
	Contract (GCC)		4.2.1	[1,2,3,4(2)]	R1 to 16 R1
			[1,2,3,4(2)]	Sub Clause-4.2.2	
			Sub Clause-	Sub Clause-4.2.3 (i) are	
			4.2.2	modified.	
			Sub Clause-		
			4.2.3 (i)		
17.	Volume-2 of 7:	20	Clause-4.6	Clause-4.6	Replace Page
	General Conditions of			is modified.	20 with 20 R1
	Contract (GCC)				
18.	Volume-2 of 7:	26-27	Clause-4.33.1	Clause-4.33.1	Replace Page
	General Conditions of		Sub-Clause(c):	Sub-Clause(c):	26-27 with 26
	Contract (GCC)		Debarment	Debarment from	R1 to 27 R1
			from bidding:	bidding:	
			(2)& (3)	(2)& (3) is modified.	
19.	Volume-2 of 7:	44, 45,46	Clause-10.10	Clause-10.10; Clause-	Replace Page
	General Conditions of	& 48	Clause-11;	11; Sub Clause-	44,45,46 & 48
	Contract (GCC)		Sub Clause-	11.1.1(iii); Sub-Clause-	with 44R1, 45
			11.1.1(iii);	11.1.4(ii); Sub-Clause-	R1, 46R1 and
			Sub-Clause-	11.2.1 (2nd Para);	48 R1
			11.1.4(ii);	Sub-Clause-11.3.3; are	
			Sub-Clause-	modified.	
			11.2.1 (2nd		
			Para);Sub-		
			Clause-11.3.3.		



SN	Bidding Document	Page No	Clause	Addendum/	Remarks
			No/Item No	Corrigendum	
20.	Volume-2 of 7: General Conditions of Contract (GCC)	53 and 54	Clause- 12.1[2,4(i), 4(i)(c) and 5]	Clause-12.1[2,4(i), 4(i)(c) and 5] are modified	Replace Page 53 and 54 with 53 R1 and 54 R1
21.	Volume- 3 of 7: Employer's Requirement (Functional)	24	Clause No-2.8 Construction Depot and Dumping Area	Clause No-2.8 Is modified.	Replace Page 24 with 24 R1
22.	Volume- 4 of 7: Outline Construction Specifications (OCS) Part-1	96	Clause-6.4.8 Anchorages	Clause-6.4.8 Is modified.	Replace Page 96 with 96R1
	Part-1	150	Clause-8.1.6 Pile Cap	Clause-8.1.6 Is modified.	Replace Page 150 with 150R1
	Part-1	151	Clause-8.1.7 (iii)	Clause-8.1.7 (iii) is modified.	Replace Page 151 with 151R1
	Part-1	179	Clause-9.1.3 (a)	Clause-9.1.3 (a) is modified.	Replace Page 179 with 179 R1
	Part 1	309	Annexure-A	Annexure-A is modified.	Replace Page 309 with 309 R1
23.	Volume- 4 of 7: Outline Design Specifications	17	Clause 6.7.5 Computation of Fundamental period of vibration	Clause- 6.7.5 Computation of Fundamental period of vibration is modified.	Replace Page 17 with 17 R1
24.	Volume- 4 of 7: Outline Design Specifications	81A to 90	Clause-7. Annexure-A: Load Combination	Clause-7. Annexure-A: Load Combination is modified.	Replace Pages 81A to 90 with 81AR1 to 90R1
25.	Volume-5 of 7: Bid Drawings	Bid Drawing No GEN- JMRC-TD- 003-R0	LIST OF DRAWINGS FOR UNDER GROUND STRETCH	Bid Drawing No GEN- JMRC-TD-003-R0 is revised.	Replace Bid Drawing No- GEN-JMRC-TD- 003-R0 with GEN-JMRC-TD- 003-R1



SN	Bidding Document	Page No	Clause	Addendum/	Remarks
26.	Volume-5 of 7: Bid	Drawing	No/Item No Bid Drawing	Corrigendum Bid Drawing Nos.	Replace Bid
	Drawings	SNo: 14,15,16,1 7 as per Index of Drawings. (GEN- JMRC-TD- 003-R0 (01 of 01))	Nos. GEN-JMRC-1C- ALG-TD-001-R0; GEN-JMRC-1C- ALG-TD-002-R0; GEN-JMRC-1C- ALG-TD-003-R0; GEN-JMRC-1C- ALG-TD-004-R0	GEN-JMRC-1C-ALG-TD- 001-R0; GEN-JMRC-1C-ALG-TD- 002-R0; GEN-JMRC-1C-ALG-TD- 003-R0; GEN-JMRC-1C-ALG-TD- 004-R0 Are revised.	Drawing Nos. GEN-JMRC-1C- ALG-TD-001-R0 with R1; GEN-JMRC-1C- ALG-TD-002-R0 with R1; GEN-JMRC-1C- ALG-TD-003-R0 with R1; GEN-JMRC-1C- ALG-TD-004-R0 with R1.
27.	Volume-5 of 7: Bid Drawings	Drawing SNo: 20 as per Index of Drawings CCV- JMRC-1C- STR-TD- 14003-R0	Bid Drawing Nos OPEN RAMP, CUT & COVER GENERAL ARRANGEMEN T (SHEET 1 OF 2), CCV-JMRC- 1C-STR-TD- 14003-R0	Bid Drawing Nos OPEN RAMP, CUT & COVER GENERAL ARRANGEMENT (SHEET 1 OF 2), CCV-JMRC-1C- STR-TD-14003-R0 Is revised.	Replace Bid Drawing Nos OPEN RAMP, CUT & COVER GENERAL ARRANGEMEN T (SHEET 1 OF 2), CCV-JMRC- 1C-STR-TD- 14003-R0 with R1
28.	Volume-7 of 7: Geotechnical Investigation Report	Page No- 01, 05 to 06	Point No-02 of Chapter-01: Details of Site & General Geological History. Point No-4.2: Field Investigation in Soil Strata.	Point No-02: Details of Site & General Geological History is modified. Point No-4.2: Field Investigation in Soil Strata.	Replace Page No-01, 05 to 06 with 01R1, 05R1 to 06R1
29.	Volume-7 of 7: Geotechnical Investigation Report			Picture of Rock Core Samples obtained from Bore Hole No-18	Page No 293 added to the report.
30.	Volume-7 of 7: Geotechnical Investigation Report	Corn		Geotechnical Investigation Report for Chainage 12490 m to 13040 m added with alignment drawing of the section.	Geotechnical Investigation Report for Chainage 12490 m to 13040 m added with alignment drawing of the section. (Total Pages 131)

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SN	Bidding Document	Page No	Clause No/Item No	Addendum/ Corrigendum	Remarks
31.	Volume-7 of 7: Topography Survey Report			Survey Report of section from Chainage 12440 m to 13040 m is added.	Survey Report of section from Chainage 12440 m to 13040 m is added. (Total Pages 01)
32.	Reply to bidder's queries received up to 11.07.2023 (12:00 Hrs)				Total Pages 35 Nos.

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	will be participating in such virtual meeting at least one day before the meeting (latest by 1100 hrs on 08.07.2023) to the registered official email of JMRC i.e. i.e. <u>imrc.phase1c.ug@ jaipurmetrorail.in</u> so that link having details such as software, meeting ID, password etc. can be mailed to these persons at least 12 hours before the scheduled virtual pre- bid meeting.
Last date of issuing addendum (if any)	20.07.2023
Date & time of Submission of Bid online	Bid submission start date: 21.07.2023 (0900 hrs). Bid submission end date: <u>09.08.2023</u> (1800 hrs).
Date & time of opening of Bid online	<u>10.08.2023</u> at 1600 hrs.
Authority for purchase of Bid documents (in case of physical Bids), seeking clarifications and submission of completed Bid documents	Director Project, Jaipur Metro Rail Corporation Ltd., 1st Floor, A-Wing, Admin Building, Bhrigu Path, Mansarovar Metro Depot, Mansarovar, Jaipur- 302020 Contact; +91-141-2822781 / 2822786 E-Mail id: - jmrc.phase1c.ug@ jaipurmetrorail.in;

To facilitate payment of Bid Fee, **E-Bidding Processing Fee** and Bid Security through RTGS, NEFT & IMPS, the details of bank account of JMRC is mentioned below

Name of Bank	Bank's Address	Account Name & No.	Account Type	IFSC code
Branch:-Tilak Marg, C-	Khanij Bhawan, Tilak Marg, C-Scheme, Jaipur-302005,	Jaipur Metro Rail Corporation	Current	ICIC0006786
Scheme, Jaipur.	Rajasthan	A/C:678605111973		

1.1.3 QUALIFICATION CRITERIA:

1.1.3.1 Eligible Applicants:

- i.
- The bids for this work will be considered only from those bidders (proprietorship firms, partnerships firms, companies, corporations, consortia or joint ventures) who meet requisite eligibility criteria prescribed in the sub-clauses of Clause 1.1.3 of NIB. In the case of a JV or Consortium, all members of the Group shall be jointly and severally liable for the performance of whole contract. Also, each member shall be individually responsible for its duties as specified in the MOU/JV agreement submitted by the bidder in terms of clause 1.1.3.1 vii d.

Performance of each JV/Consortium partner shall also be judged on quarterly basis. In case, the performance of the partner(s) is not found satisfactory, actions as deemed appropriate by the Employer may be taken including termination of contract or termination of any of JV/Consortium member(s) from the contract i.e Part Termination of the contract. In case of part termination of contract, the Performance Security(ies) submitted by the member(s) for their portion of work in contract as per their share in JV/Consortium shall be forfeited and the

Director (Project)

C3 Form of Bid

The Form of Bidder shall be completed and signed by a duly authorized and empowered representative of the Bidder. If the Bid comprises a partnership, consortium or a joint venture the Form of Bid shall be signed by a person who is duly authorized by each member or participant thereof or by authorized signatory of each member. Signatures on the Form of Bid shall be witnessed and dated. Copies of relevant powers of attorney shall be attached.

C4 Outline Quality Plan

The Bidder shall submit **Appendix-3** of Forms of Bid to form part of his Bid an Outline Quality Plan illustrating the intended means of compliance with the Employer's Requirements (Volume 3) and setting out in summary form an adequate basis for the development of the more detailed document required under Clause 16 of the SCC. The Outline Quality Plan shall contain sufficient information to demonstrate clearly the proposed method of achieving the Bidder's quality objectives with regard to the requirements of the Contract.

C5 Outline Safety & Health Plan and Outline Environment Plan

- C5.1 The Bidder shall submit Appendix-4 of Forms of Bid to form part of its Bid an Outline Safety & Health Plan and Outline Environment Plan which shall contain sufficient information to demonstrate clearly the Bidder's proposals for achieving effective and efficient safety & health and environment procedures. The Outline Safety & Health Plan and Outline Environment Plan should include an outline of the safety procedures and regulations to be developed and the mechanism by which they will be implemented for ensuring Safety & Health and Environment as required by the Employer's Requirements (Volume 3) and Clause 8 & 9 of the SCC.
- C5.2 The Outline Safety & Health Plan and Outline Environment Plan shall be headed with a formal statement of policy in relation to safety & health and environment and shall be sufficiently informative to define the Bidder's safety plans and set out in summary an adequate basis for the development of the Contract specific Site Safety & Health Plan and Site Environment Plan to be submitted in accordance with **Clause 8 & 9 of the SCC**.
- C5.3 The Bidder may be requested by JMRC in writing to amplify, explain or develop his Outline Safety & Health Plan and Outline Environment Plan prior to the date of acceptance of the Bid and to provide more details with a view to reaching provisional acceptance of such plans.

C5.4 C&D Waste Management and Use of Recycled Products in Jaipur/Rajasthan. -

Regarding Construction and Demolition(C&D) Waste management and use of recycled products in Jaipur / Rajasthan, the bidders must note that;

- a) They have to devise appropriate measures for management of Construction and Demolition(C&D) Waste generated including its processing and for using the recycled products in the best possible manner. The Bidder shall adhere Construction & Demolition (C&D) Waste Management Rules, 2016 notified by Govt. of India. The bidder should also take note of advisory of Govt. of Rajasthan in combating and mitigating climate change phenomenon and giving high priority to Swachh Bharat Mission of Govt. of India.
- b) Refer Clause No. 52 13 of Conditions of contract on Safety & Health and Environment.
- c) Compliance contrincate and details of compliance of these conditions shall be submitted by the Contractor along with respective running account bill. <u>The payment of running account bill</u> shall be released by the Employer after verification and certification by the Engineer.

C9.2 Maintenance

- C9.2.1 The Contractor shall be responsible for maintaining the Works until final hand over to the Employer and for the provision of relevant maintenance manuals and drawings.
- C9.2.2 The Contractor shall be responsible for making good any and all defects of materials and workmanship, in the Works for the period stated in the General Conditions of Contract
- C9.2.3 The Contractor shall be responsible for the security of the Site during the construction phase of the Contract, until the issuance of a Taking-Over Certificate.

C10. Payment Schedule:

The payment for items given in Bill of Quantity (Volume 6) shall be made on the basis of actually executed quantities.

C11. Sub-Contracts

- C11.1 Sub-contracting, excluding design work shall be generally limited to 50% of the Contract price. The terms and conditions of sub-contracts and the payments that have to be made to the sub-contractors shall be the sole responsibility of the Contractor.
- C11.2 For sub-contracts exceeding Rs.5 million, it will be obligatory for the Contractor to obtain a Notice of No Objection from the Engineer to the identity of the sub-contractor. The value of each sub-contract shall be provided by the Contractor to the Engineer. The Contractor shall certify that the cumulative value of the sub-contracts (including those up to Rs. 5 million each) awarded is within the aforesaid 50% limit. In this regard the Bidder's attention is invited to Clause 4 of SCC.
- C11.3 The Terms and Conditions of the sub-contract are the sole prerogative of the Contractor and are deemed to be included in the contract price.

C12. Staffing Schedule and Related Details

C12.1 The Bidder shall submit with his Bid (**Appendix-7** of Form of Bid) a staffing schedule containing the names, qualifications, professional experience and corporate affiliation of all proposed management personnel (above the level of shift supervisor) and specialists for this work. Details shall be included for all such personnel whether directly employed or engaged on a consultancy or advisory basis and whether associated with the design or the construction of the Works. The submission shall include a provisional management structure and organization chart showing areas of responsibility, relative seniorities and lines of reporting. The proposed staffing plan shall be in conformity with the **Annexure 3 and Annexure 4** of ITB.

- C12.2 The Bidder shall include his proposals for his Co-ordination Control Team and include the name and qualifications of the Team Leader responsible for the interface co-ordination with Designated Contractors.
- C12.3 The key staff for execution of this work shall be from that member of the JV/Consortia who has the experience of similar work and on whose experience the JV/Consortia qualifies the criteria of work experience. If the JV qualifies on the credentials of work eligibility by the foreign partner, then the Project Manager deployed shall be an expatriate having minimum 15 years of total experience out of which 05 years should be in projects of similar nature as mentioned in Annexure-3 & Annexure-4 of ITB. The Project Manager must be involved actively in the project execution. He will be required to attend all meetings/inspections conducted by JMRC officials or Its Engineer. **He must take prior permission from Engineer for obtaining leave during his tenure as Project Manager**. In case the JV do not follow these instructions, action shall be initiated under the conditions of contract windows penalty or to terminate the contract. The JV/Consortium members shall submit undersking to this effect in Appendix-6A of Form of Bid.

In case the successful bidder is a JV/Consortium having a foreign partner and if the experience of civil works for the purpose of qualifying the minimum eligibility criteria is fulfilled by the foreign partner then the foreign partner shall submit an additional Bank Guarantee (In addition of performance security) of an amount equal to 1% of the contract value as per LOA for the fulfillment of the condition of deployment of key staff and the expatriate Project Manager for the project.

The foreign partner shall submit bank guarantee from their respective bank account. Bank guarantee executed from the bank accounts of JV/Consortium or any other bank account shall not be accepted.

This bank guarantee shall be valid up to the completion period of the contract and shall be from Scheduled commercial Bank (including Scheduled Commercial Foreign Banks) in India in the currency in which the contract price is payable. This Bank Guarantee shall be furnished to the employer within 30 (thirty) days of receipt of the Letter of Acceptance. The form of this Bank Guarantee provided in **Annexure-7A** of ITB.

C13. Contractor's Equipment

C13.1 The contractor shall deploy plants and equipment required to complete the work as per the schedule and within the completion period with minimum of numbers given in Annexure-5 of ITB.

C14. Proposals for Use of Work Areas

- C14.1 The Bidder shall note the requirements of <u>Right to Fair Compensation and Transparency in</u> <u>Land Acquisition, Rehabilitation and Resettlement Act, 2013.</u>
- C14.2 The Bidder shall note the provision contained in Employer's Requirements.
- C14.3 The Bidder is to note that the Contractor will be fully responsible for the provision of all utility services like water, electricity, sewerage etc necessary for the construction and completion of the Works.

C15. Pricing Document

C15.1 The Pricing Document is included in Bill of Quantities; Volume 6. The Bidder shall complete the Pricing Document in accordance with the instructions given in Bill of Quantity/Pricing Document.

The completed Pricing Document including price of minor deviations in **Annexure-13A** of BOQ for such deviation as mentioned in **Appendix-13** of FOB shall be submitted.

- C15.2 The price of each such minor deviation will be the price which the bidder agrees to offer to the employer from his quoted offer in BOQ if deviation is agreed by the employer. Any such deviation without a price shall not be considered and will be treated as withdrawn by the bidder. Any other deviation mentioned anywhere in the submission other than in **Appendix-13** of FOB shall be considered as if mentioned inadvertently by the bidder and shall be considered as withdrawn without any confirmation from the bidder.
- C15.3 The Bidder is to note the S.No. (iv) of **Appendix-1 of FOB** for Liquidated Damage for delay in completion of the work.

C16. Currencies of Bid and Payment

C16.1 The Bidder shall give his priced offer for BOQ in Indian Rupees Only.



E5.2 Correction of Errors (Rule-64 of RTPPR-2013)

- E5.2.1 Bids determined to be technically acceptable after technical evaluation will be checked by the Employer for any arithmetical errors in computation and summation during financial evaluation. Errors will be corrected by the Employer as follows:
 - a) If there is a discrepancy between the unit price and the total amount derived from the multiplication of the unit price and the quantity, the unit price as quoted will normally govern unless in the opinion of the Employer there is an obviously gross misplacement of the decimal point in the unit price, in which event, the total amount as quoted will govern; and
 - b) if there is a discrepancy in total corresponding to the addition or subtraction of subtotals, the subtotals shall prevail and the total shall be corrected; and
 - c) If there is a discrepancy between amounts in figures and in words, the amount in words will govern in case of physical form of bidding unless the amount expressed in words is related to an arithmetic error, in which case the amount in figures shall prevail subject to clause (a) and (b) above. However, in case of e-bidding, amount in figures will govern: and
- E5.2.2 If a Bidder does not accept the correction of errors as outlined above, his Bid will be rejected and the Bid security shall be forfeited.

E5.3 Comparison of Bids

Bids will be compared in Indian Rupees only.

E5.4 Deleted.

- **E5.5** For the purpose of comparative evaluation of bids received, the sum total of following shall be considered:-
 - (i) The amount quoted as lump sum by the bidder for the given schedule-A, and
 - (ii) The total amount worked out from the quoted percentage (above/below/at par) by the bidder for the given Schedule-B & C.

The total value of above thus obtained in equivalent INR shall be compared amongst various bidders to determine the lowest evaluated bid. Provision of clause 1.2.1 (ix) of NIB shall also be considered for financial evaluation.

- **E5.6** If the lowest bidder as evaluated as per E5.5 has given some minor deviations then the Employer has right to accept some or all such minor deviation and the offer of the lowest will be reduced by the price of such accepted deviations.
- **E5.7** The Employer reserves the right to accept or reject any variation, deviation. Variations, deviations and other factors which are in excess of the requirements of the Bid Documents or otherwise result in the accrual of unsolicited benefits to the Employer shall not be taken into account in bid evaluation.

E6 Indigenisation

E6.1 Bidders are encouraged to involve domestic firms in the Contract organization and procurement processes.



Instructions to Bidders

Annexure 6 (As per Clause C 18.1)

FORM OF BANK GUARANTEE FOR BID SECURITY

(To be stamped in accordance with Stamp Act, if any, of the country of issuing bank)

- 2. WHEREAS......(Name of Bidder) (hereinafter called "the Bidder") has submitted its bid dated...... for(Name of the work as per clause 1.1.1 of NIB) hereinafter called the bid. AND WHEREAS the Bidder is required to furnish a Bank Guarantee for the sum of Rs. as Bid Security against the Bidder's offer as aforesaid. AND WHEREAS......(Name of Bank) have, at the request of the Bidder, agreed to give this guarantee as hereinafter contained.
- 3. We further agree as follows:

a. Deleted.

- b. That the guarantee hereinbefore contained shall not be affected by any change in the constitution of our Bank or in the constitution of the Bidder.
- C. That any account settled between the Employer and the Bidder shall be conclusive evidence against us of the amount due hereunder and shall not be questioned by us.
- e. That the expression 'the Bidder' and 'the Bank' herein used shall, unless such an interpretation is repugnant to the subject or context, include their respective successors and assigns.

4. THE CONDITIONS OF THIS OBLIGATION ARE:

- a. if the Bidder withdraws his Bid during the period of Bid validity specified in the Form of Bid, or
- b. if the Bidder does not accept the correction of his bid price in terms of Clause **E5.2** of the "Instructions to Bidders".
- C. if the Bidder having been notified of the acceptance of his bid by the Employer during the period of bid validity:
 - i. fails or refuses to furnish the Performance Security in accordance with Clause F 5.1 of the "Instructions to Bidders" and/or
 - ii. The section of th

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> d. <u>if the Bidder withdraws his bid after opening of his financial package (in two</u> package system during the period of validity of his bid or breaches any provision of code of integrity prescribed for bidders specified in the RTPP-Act-2012 and Chapter VI of RTPP-Rules-2013, or in case of (c) above, beside forfeiture of Bid Security, the bidder shall not only be debarred from participating in the re-bid of same work but also will be debarred from participating in any bid of JMRC for a period of three years from the date of withdrawal of his bid or from the date of issue of letter of annulment of LOA, as the case may be.

> We undertake to pay to the Employer mere on demand without demur up to the above amount upon receipt of his first written demand, without the Employer having to substantiate his demand provided that in his demand the Employer will note that the amount claimed by him is due to him owing to the occurrence of any one or more of the conditions (a), (b), (c) **and (d)** mentioned above, specifying the occurred condition orconditions.

5. Notwithstanding anything contained herein:

- b) This Bank Guarantee shall be valid upto.....
- c) We are liable to pay the guarantee amount or part thereof under this Bank Guarantee only & only if you serve upon us a written claim or demand on or before.....
- d) The amount covered under the above Bank Guarantee shall be automatically credited in the accounts of Jaipur Metro Rail Corporation in ICICI BANK LTD, Khanij Bhawan, Tilak Marg, C-Scheme, Jaipur-302005 through IFSC: ICIC0006786. Bank Account No. 678605111973 on the date of expiry or its validity, unless the agencies get it re-validated well before its expiry date or produce NOC from Jaipur Metro Rail Corporation Ltd. in writing for its release.

	Signature of
	Authorized Official of the Bank
Signature of Witness	Name of Official
Name :	Designation
Address :	Stamp/Seal
	of the Bank

Notes:

- 1 Please note that, as per clause C18.1, any deviation in Bid security with regard to amount, validity and format shall be considered as material deviation and bid shall be dealt accordingly.
- 2 The stamp papers of appropriate value shall be purchased in the name of the Bank, who issues the 'Bank Guarantee'.
- 3 The 'Bank Guarantee's hat be from the Scheduled Commercial Bank based in India, acceptable to Employer.
- 4 Bid Security to be furnished on appropriate non-judicial stamps & should be valid for the next 07 months from the did opening date

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Instructions to Bidders

Annexure 7 (As per ClauseF5.1)

FORM OF PERFORMANCE SECURITY (GUARANTEE) BY BANK

(To be given by a Scheduled Bank in India)

(To be executed on non-judicial stamp)

(Rule-75 & 75A of RTPPR-2013)

(Refer Clause F5 of "Instructions to Bidders")

(Rule-75 of RTPPR-2013)

- 1. This deed of Guarantee made this day of (month &year) between Bank of......(herein after called the "Bank")of the one part ,and Jaipur Metro Rail Corporation Limited (hereinafter called "the Employer") of the other part.
- **3.** AND WHEREAS the Contractor is bound by the said Contract to submit to the Employer a Performance Security for a total amount of Rs......(Amount in figures and words).
- 5. NOW THEREFORE, we hereby affirm that we are the Guarantor and responsible to you, on behalf of the Contractor and we hereby unconditionally, irrevocably and without demur undertake to immediately pay to the Employer upon first written demand and without cavil or argument, any sum or sums within limits of (Amount of Guarantee) as aforesaid without reference to the Contractor and without your needing to prove or show grounds or reasons for your demand for the sum specified therein. The Bank shall pay to the Employer any money so demanded notwithstanding any dispute/disputes raised by the Contractor in any suit or proceedings pending before any Court, Tribunal or Arbitrator/s relating thereto and the liability under this guarantee shall be absolute and unequivocal.
- **6.** This Guarantee is valid till (The initial period for which this Guarantee will be valid shall be as stated in Clause 4.2.1 of the "General Conditions of Contract".)
- 7. At any time during the period in which this Guarantee is still valid, if the Employer <u>agrees to grant a</u> <u>time extension to the Contractor or if the Contractor fails to complete</u> the Works within the time of completion as stated in the Contract, or fails to discharge himself of the liability or damages or debts as stated under Para 5, above, it is understood that the Bank will extend this Guarantee under the same conditions for the required time on demand by the Employer and at the cost of the Contractor.
- 8. The Bank agrees that no change, addition, modifications to the terms of the contract Agreement or to any documents, which have been or may be made between the Employer and the Contractor, will in the way release us from the liability under this Guarantee; and the Bank, hereby, waives any requirement for notice of any such change, addition or modification to the Bank.

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Notes:

- 1 The stamp papers of appropriate value shall be purchased in the name of the Bank, who issues the 'Bank Guarantee'.
- 2 The 'Bank Guarantee' shall be from the Scheduled Commercial Bank based in India, acceptable to Employer
- 3 The 'Bank Guarantee' must be issued on the Structured Financial Messaging System (SFMS) platform.
- 4 A separate copy of the BG has to be sent by the issuing bank to the Employer's bank through SFMS. The details of Employer's bank are as under.

ICICI BANK LTD; Jaipur Metro Rail Corporation. Branch:-Tilak Marg, C-Scheme, Jaipur. Khanij Bhawan, Tilak Marg, C-Scheme, Jaipur-302005, Rajasthan. A/C:678605111973 IFSC: ICIC0006786

5. <u>Following codes are to be used by issuing bank for the purpose of</u> <u>Confirmation and amendment in Bank Guarantees:-</u>

<u>Code</u>	<u>Purpose</u>
<u>MT760</u>	<u>Confirmation of bank</u> <u>guarantee</u>
<u>MT767</u>	<u>Amendment in bank</u> <u>guarantee</u>

6. <u>Bank Guarantee issued on the SFMS platform with any other code other than</u> <u>mentioned above for the purposes shall not be acceptable to the employer.</u>



Notes:

- 1. <u>The stamp papers of appropriate value shall be purchased in the name of the Bank, who issues</u> <u>the 'Bank Guarantee'.</u>
- 2. <u>The 'Bank Guarantee 'shall be from the Scheduled Commercial Bank based in India, acceptable</u> to Employer.
- 3. <u>The 'Bank Guarantee 'must be issued on the Structured Financial Messaging System (SFMS)</u> platform.
- 4. <u>A separate copy of the BG has to be sent by the issuing bank to the Employer's bank through</u> SFMS. The details of Employer's bank are as under.

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6. <u>Bank Guarantee issued on the SFMS platform with any other code other than</u> <u>mentioned above for the purposes shall not be acceptable to the employer.</u>



Instructions to Bidders (Annexure – 7D Clause F5.1.1) Performance Security Declaration (Rule-75 of RTPPR-2013) (To be executed on a non-judicial stamp)

 Date: ______ [insert date (as day, month and year)]

 Contract Name and No.: ______ [insert name and number of Contract]

 To: ______ [insert Designation and complete address of Procuring Entity]

 We, the undersigned, declare that :

- 1. We are a (Strike out which is not applicable. Please enclose an authentic certificate issued by the Administrative Department of respective government under which the bidder entity is constituted.):
 - (i) Departments/Boards of the State Government or Central Government; or
 - (ii) Government Companies as defined in clause (45) of section 2 of the Companies Act, 2013; or
 - (iii) Company owned or controlled, directly or indirectly, by the Central Government, or by any State Government or Governments, or partly by the Central Government and partly by one or more State Governments which is subject to audit by the Auditor appointed by the Comptroller and Auditor-General of India under sub-section (5) or (7) of section 139 of the Companies Act, 2013; or
 - (iv) Autonomous bodies, Registered Societies, Cooperative Societies which are owned or controlled or managed by the State Government or Central Government.
- 2. We understand that we are eligible for submission of a Performance Securing Declaration in lieu of Performance Security under Rule 75 (1) of RTPP Rules, 2013.
- We understand that, according to your conditions, the Contract must be supported by a Performance Security Declaration as a guarantee to ensure fulfillment of our all performance obligations under the Contract for _____ [insert name of subject matter of procurement]
- 4. We accept that we will automatically be suspended from being eligible for bidding in any contract with you for the period of time of 3 years as per section 46 of RTPP Act, 2012 [Procuring Entity to indicate here the period of time for which the Procuring Entity will declare a Bidder ineligible to be awarded a Contract if the performance Security Declaration is to be executed] starting on the date that we receive a notification from you, the bid accepting authority, MD / CMD, JMRC [Designation of the Procuring Entity] that our Performance Security Declaration is executed, if we are in breach of any of our performance obligation under the conditions of the Contract.
- 5. We understand this Performance Security Declaration shall expire after 60 days of completion of our all obligations under the Contract including Defect Liability, warranty/ Guarantee, operation, maintenance, etc. in accordance with the conditions of the Contract.



Signed: ______ [insert signature of person whose name and capacity are shown] In the capacity of: _____ [insert legal capacity of person signing the Performance Security Declaration] Name: _____ [insert complete name of person signing the Declaration] Duly authorized to sign the Contract for and on behalf of: _____ [insert complete name and address of the Bidder] Dated on day of _ [insert date of signing] Corporate Seal _____



FORM OF BID - Appendix-30

Power of Attorney for Authorized Signatory of Bidder Firm.

POWER OF ATTORNEY FOR SIGNING THE BID

Know all men by these presents, We.....(name of the firm and address of the registered office) do here by irrevocably constitute, nominate, appoint and authorize Mr./Ms.(name)..... Son/daughter/wife of..... and presently residing presently employed with at..... who is us position of.....as our true and holding the and lawful attorney (hereinafter referred to as the "Attorney")to do in our name and on our behalf, all such acts, deeds and things as are necessary or required in connection with or incidental to submission of our CONTRACT ICB No.JP/EW/1C(Underground)/03: "Design and Construction of Twin Tunnel by Shield TBM, Underground Station (Ramganj Chaupar), Cut and Cover Tunnel Box and Underground Ramp from Badi Chaupar dead end Ch:10387.860 to Underground ramp end Ch:13040 of Jaipur Metro Phase-1C including Entry Exit Structures, Architectural finishing, water supply, Sanitary Installations and Drainage Works at Jaipur, Rajasthan, India." including but not limited to signing and submission of all Bids, bids and other documents and writings, and other conferences and providing information/ responses to JMRC or its Engineer, representing us in all matters before JMRC or its Engineer, signing and execution of all contracts including the Contract and undertakings consequent to acceptance of our bids, and generally dealing with the JMRC or its Engineer in all matters in connection with or relating to or arising out of our Bid for the said Projects and/or upon award thereof /or till the entering into of the Contracts with JMRC.

AND we hereby agree to ratify and confirm and do hereby ratify and confirm all acts, deeds and things lawfully done or caused to be done by our said Attorney pursuant to and in exercise of the powers conferred by this Power of Attorney and that all acts, deeds and things done by our said Attorney in exercise of the powers hereby conferred shall and shall always be deemed to have been done us.

IN WITNESS WHEREOF WE ,THE ABOVE NAMED PRINCIPAL HAVE EXECUTED THIS POWER OF ATTORNEY ON THISDAY OF.......,(Month & Year).



For (Signature)

(Name, Title and Address) Witnesses:

Accepted

.....Signature)

(Name, Title and Address of the Attorney)

(Notarized)

Notes:

The mode of execution of the Power of Attorney should be in accordance with the procedure, if any, laid down by the applicable law and the chartered documents of the executants and when it is so required, the same should be under common seal affixed in accordance with the required procedure. Also, wherever required, the Applicant should submit for verification the extract of the chartered documents and documents such as a resolution/power of attorney in favors of the person executing this Power of Attorney for the delegation of power hereunder on behalf of the Applicant.

The Applicant should submit Board of Directors resolution in which proposal of authorizing a particular signatory was passed.



Special Conditions of Contract (SCC)

1	Sub-Clause 1.4	Contract Agreement The Form of Contract Agreement shall be in the format given in Schedule 2 to these Special Conditions of Contract.
2	Sub-Clause 3.2	Functions of Engineer
		In addition to the duties mentioned in Clause 3.2 of General Conditions of Contract:
		 (i) <u>Engineer</u> shall watch and inspect the Works, monitor the test results and examine any material to be used and workmanship employed by the Contractor in connection with the Works;
		 (ii) <u>Engineer</u> shall carry out such duties and exercise such powers vested in the Engineer in accordance with the provisions of the Contract;
		 (iii) <u>Engineer</u> shall issue instructions which in his opinion are necessary for the execution of the Works; and
		(iv) <u>Engineer</u> may issue any other instruction which in his opinion is desirable in connection with the Works.
		(v) Engineer will assist in Technical , Contractual and in Arbitration matter <u>and judicial forums</u> .
		(vi) Engineer shall submit one set of updated GFC to Employer as and when updated
		In case The Engineer is employee of any agency hired by the Employer, the Engineer shall take the approval of the Employer for all technical and financial matters otherwise he shall be deemed to have taken the approval of the Employer.
3	Sub-Clause 4.2.4	Guarantees, Warranties and Undertakings
		The forms of Contractor warranty shall be in the format given in the Schedule-1 of these Special Conditions of Contract.
4	Sub-Clause 4.5	Sub-Contractors
		The sub-contracting, excluding design work shall be limited to 50% of
	12	the Contract Value. The value of a sub-contract, other than for Design work as when awarded, should be intimated by the Contractor to the Engineer and it should also be certified that the cumulative value of the sub-contracts awarded so far is within the aforesaid limit of 50%. A copy of the contract between the Contractor and Sub-Contractor shall be given to the Engineer within 15 days of signing and in any case 7 days before the Sub Contractor starts the Work and thereafter the Contractor shall not carry any modification without the consent in writing of the Engineer. The terms and conditions of sub-contracts and the payments that have to be made to the sub-contractors shall be the sole responsibility of the Contractor. Payments to be made to such sub- contractors will be deemed to have been included in the Contract price. However, for major sub-contracts (each costing over Rs. 50 lacs), it will be obligatory on the part of the Contractor to obtain consent of the Employer. The Employer will give his consent after assessing and satisfying himself of the capability, experience and equipment protector.

resources of the sub-contractor. In case the Employer intends to withhold his consent, he should inform the Contractor within 15 days to enable him to make alternative arrangements to fulfil his programme.

The Contractor shall provide sufficient superintendence, whether on the site or elsewhere, to ensure that the work to be carried out by a subcontractor complies with the requirements of the Contract.

In the case of sub-contracts for electrical and mechanical works, which the Contractor intends to procure on the basis of outline design, design briefs and performance specification, the Contractor shall, prior to inviting bids from sub-contractors, submit such documents to the Engineer for review.

The proposed sub-contract terms and conditions shall impose on the sub-contractor such terms of the Contract as are applicable and appropriate to the part of the Works to be sub-contracted, to enable the Contractor to comply with his obligations under the Contract.

Notwithstanding any consent to sub-contract given by the Engineer, if in his opinion it is consider necessary, the Engineer shall have full authority to order the removal of any sub-contractor from the Site or off-Site place of manufacture or storage.

5 Sub-Clause 4.9 Site Data

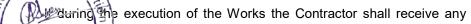
The Geotechnical and other related data provided by the Employer are based on the investigation conducted by JMRC and are for reference purposes only. The Bidder should satisfy himself with the data furnished and make his own investigations, if required, for submitting his offer. Any change in design or construction methodology later during execution on account of change will be borne by the Contractor.

The Contractor shall not be relieved from any risk or obligation imposed on or undertaken by him under the Contract on any such ground or on the ground that he did not or could not foresee any matter which may affect or have affected the execution of the Works, or compliance with his other obligations under the Contract.

6 Sub-Clause 4.11 Access Route

All operations for the execution of the Works shall be carried out so as not to interfere unnecessarily with the convenience of the public or the access to public or private roads or footpaths or properties owned by the Employer or by any other person.

The Contractor shall select routes, choose and use vehicles so that movement of Contractor's Equipment, Plant and Materials from and to the Site is limited so that traffic is not delayed and damage to highways and bridges is prevented. If there is any delay or damage or injury, the cost of rectification or reconstruction of highways or bridges shall be borne by the Contractor. The Contractor shall indemnify the Employer in respect of all claims, demands, proceedings, damages, costs,





matters.

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claim arising out of the execution of the Works in respect of damage to highways or bridges <u>or any other public utility or private property</u>, he shall immediately report the facts to the Engineer. The Contractor shall negotiate a settlement in respect of such claims and indemnify the Employer in respect of all claims, proceedings, damages, costs, charges and expenses in relation thereto.

7 Sub-Clauses 4.13 Programmes

The Contractor shall prepare and submit his detailed Programme of Work so as to achieve key dates of various activities. The Contractor shall complete the work in a phased manner fixing priorities to the different stretches of the work to give access to other interfacing contracts as per the requirement of project from time to time.

The Engineer on receipt of a programme shall inform the Contractor in writing within 21 days after receipt of the above information;

- (a) that the programme has received his consent; or
- (b) that the programme is rejected, in which case reasons for such rejection shall be given; or
- (c) that further information is required to clarify or substantiate the programme or to satisfy the Engineer as to its reasonableness, or
- (d) that the programme has received his consent subject to incorporation of comments attached to the Notice of No Objection.

Provided that if none of the above actions is taken within the 30 day period, the Engineer shall be deemed to have given consent to the programme submitted.

The Contractor shall, within 21 days of receiving notification under subparagraphs (c) or (d) above, provide further information requested or the programme shall be deemed to have been rejected. The Engineer shall, within 21 days of receipt of such further information, either reject the programme or give his consent.

In the event of a programme being rejected, or deemed to have been rejected, the Contractor shall, within 21 days thereafter, submit a revised programme taking account of the reasons given for the rejection or incorporating further information requested by the Engineer, as the case may be.

The Contractor, following receipt of consent to the Works Programme, may at any time, submit to the Engineer an amended version. In the event that the Engineer grants an extension of time, instructs an Employer's Variation, or on the occurrence of any event or happening or situation, which could materially affect the progress of the Works, the Contractor shall submit a revised programme to the Engineer for his consent.

If the Engineer feels that there is a significant deviation between the relaction or anticipated progress of the Works and the Works programme, the Engineer may require the Contractor to submit a revised/modified programme to ensure timely completion of Whole of Works or a Key Date of a milestone. The Contractor shall submit such revised

SCHEDULE-1

CONTRACTOR'S WARRANTY

(Refer clause 3 of SCC and Sub-Clause 4.2.4 of GCC)

(1) in favour of Jaipur Metro Rail Corporation by [Name of Contractor] [and [see Note 1]] ([Jointly] "the Contractor")

(2) [Jaipur Metro Rail Corporation Limited] [of]/[whose registered office is at] [1st Floor, A-Wing, Admin Building,bhrigu Path, Mansarovar Metro Depot, Jaipur-302020] (together with its successors and assigns, "the Employer").

WHEREAS

- (A) By a contract dated [] ("the Contract") made between (1) the Jaipur Metro Rail Corporation Limited ("the Employer") and (2) the Contractor, the Contractor has agreed to design, execute, complete, test and commission (including Integrated Testing and Commissioning) and remedy any defect in the Works upon the terms and conditions contained in the Contract.
- (B) [See <u>Note 3</u>].
- (C) At the request of the Employer and pursuant to the terms of the Contract the Contractor has agreed to enter into this Warranty.

NOW IT IS AGREED AS FOLLOWS:

- 1. The Contractor hereby warrants and undertakes that:
 - (a) He will design, execute, complete, test and commission (including Integrated Testing and Commissioning) and remedy any defect in the Works in accordance with the terms of the Contract; and
 - (b) he owes a duty of care to the Employer in relation to the performance of its duties under the Contract; and
 - (c) he will replace free of cost to the Employer any defect or failure of equipment provided in the Works for a period of _____ (as specified) months from the date of Taking Over of the last Section of the Works; and
 - (d) he agrees that should any design modification be required to any section or component due to any defect, the period of _____ (as specified) months shall recommence from the date when the modified part is commissioned into service, and such modification shall be carried out free of cost to the Employer in all sub-systems and systems for all sections; and
 - (e) he shall maintain the manufacture or spare of replacement parts for at least 10 years.
- 2. The liability of [the companies comprising [see <u>Note 3]</u>] the Contractor under this Warranty [shall be joint and several and [see <u>Note 3]</u>] shall not be released, diminished or in any way affected by any interpretent inquiry or investigation into the Works or any matter related to the Contract whether carried by or on behalf of the Employer or any liability or right of action which may also out of such inquiry or investigation.



SCHEDULE 2

FORM OF CONTRACT AGREEMENT

(Refer Clause F4 of ITB)

This Agreement is made at Jaipur on the day of (month) **2023** Between Jaipur Metro Rail Corporation Limited, 1st Floor, A-Wing, **Admin Building,bhrigu Path, Mansarovar Metro Depot, Jaipur-302020**

This agreement is signed between (for and on behalf of the Employer) and (for and on behalf of the Contractor).

NOW THIS AGREEMENT WITNESSETH as follows:

- 1. In this Agreement words and expression shall have the same meanings as are respectively assigned to them in the Conditions of Contract hereinafter referred to.
- - a) Notice Inviting Bid (NIB)
 - b) Instructions to Bidders (ITB)(Including Annexures)
 - c) Special Conditions of Contract (SCC)
 - d) General Conditions of Contract (GCC)
 - e) Conditions of contract on Safety & Health & Environment (SHE).
 - f) Outline Design Specifications
 - g) Outline Construction Specification for Civil Works
 - h) Technical Specification for Architecture & Finishing Works
 - i) Bid Drawings
 - j) Bill of Quantities
 - k) Form of Bid with Appendix
 - I) Letter of acceptance (LOA)
 - m) Contractor's proposal submitted along with the bid
 - n) Any other item as applicable

Director (Project)

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The modifications to the becocuments communicated through the Addenda (...... Numbers) hosted on the e-biscing portal at the time of bid have been incorporated in the consolidated contract documents.

Special Conditions of Contract (SCC)

- 3. In consideration of the payments to be made by the Employer to the Contractor as hereinafter mentioned, the Contractor hereby covenants with the Employer to execute and complete the works by **..... and remedy any defects therein in conformity in all respects with the provisions of the Contract.
- 4. The Employer hereby covenants to pay the Contractor in consideration of the execution and completion of the works and the remedying of defects therein, the Total Contract Price of **` being the sum stated in the letter of acceptance subject to such additions thereto or deductions there from as may be made under the provisions of the Contract at the times and in the manner prescribed by the Contract.

5. OBLIGATION OF THE CONTRACTOR

The contractor shall ensure full compliance with <u>all applicable laws in force in India</u> <u>including but not limited to</u> tax laws with regard to this contract and shall be solely responsible for the same. The contractor shall submit copies of acknowledgements evidencing filing of returns every year and shall keep the Employer fully indemnified against liability of tax, interest, penalty etc. of the contractor in respect thereof, which may arise.

6. JURISDICTION OF COURT

The Courts at Jaipur, Rajasthan, India shall have the exclusive jurisdiction to try all disputes arising out of this agreement between the parties.

IN WITNESS WHEREOF the parties hereto have caused their respective Common Seals to be hereunto affixed / (or have hereunto set their respective hands and seals) the day and year first above written.

For and on behalf of the Employer		
Signature of the authorized official		
Name of the official		
Stamp/Seal of the Employer		
By the said		
behalf of the Employer in the presence of :		
Witness		
Name :		
Address :		

Note :

- * To be made out by the Employer at the time of finalization of the Form of Agreement.
- ** Blanks to be filled by the Employer at the time of finalization of the Form of Agreement.
- *** To be deleted if not applicable

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f) the location of and the authorisation required for and the means of diversion of any services and facilities required for the purposes of the Works.

The Contractor shall whenever be required by the Engineer, submit details of the arrangement and methods which the Contractor proposed to adopt for the execution of the Works. No alteration to these arrangements or methods shall be made without the approval of the Engineer.

Performance	4.2
Security Amount	

4.2.1 (1) Performance security shall be <u>furnished within 30 days from the date of</u> issue of LOA by the successful bidder except the:-

(i) Departments/Boards of the State Government or Central Government;

(ii) Government Companies as defined in clause (45) of section 2 of the Companies Act, 2013;

(iii) Company owned or controlled, directly or indirectly, by the Central Government, or by any State Government or Governments, or partly by the Central Government and partly by one or more State Governments which is subject to audit by the Auditor appointed by the Comptroller and Auditor-General of India under sub-section (5) or (7) of section 139 of the Companies Act, 2013; or

(iv) Autonomous bodies, Registered Societies, Cooperative Societies which are owned or controlled or managed by the State Government or Central Government. However, a performance security declaration shall be taken from them. The State Government may relax the provision of performance security in a particular procurement or any class of procurement.

(2) The amount of performance security shall be ten percent of the amount of work order in case of procurement of works. In case of Small-Scale Industries of Rajasthan it shall be one percent of the amount of quantity ordered for supply of goods and in case of sick industries, other than Small Scale Industries, whose cases are pending before the Board of Industrial and Financial Reconstruction (BIFR), it shall be two percent of the amount of supply order.

(2A) Notwithstanding anything contained in sub-rule (2) above, where the State Government being of the opinion that there exist grave situations such as natural calamity or Pandemic or Epidemic diseases or floods etc. in which the economy is adversely affected, the State Government may, by order, direct the procurement entity to reduce the performance security taken in case of existing contracts of ongoing projects, from such date and on such conditions as may be specified in the order.

(3) Performance security shall be furnished in any one of the following forms-

(a) [Deleted]

Director

(Project)

AIPUR

(b) Bank Draft or Banker's Cheque of a scheduled bank;

(c) National Savings Certificates and any other script/instrument under National Savings Schemes for promotion of small savings issued by a Post Office in Rajasthan, if the same can be pledged under the relevant rules. They shall be accepted at their surrender value at the time of bid and formally transferred in the name of **Employer** with the approval of Head Post Master.

(d) Bank guarantee/s of a scheduled bank. It shall be got verified from the issuing bank. Other conditions regarding bank guarantee shall be same as Rail Compationed in the rule 42 of RTPPR, 2013;

(e) Fixed Deposit Receipt (FDR) of a scheduled bank. It shall be in the name of **Employer** on account of bidder and discharged by the bidder in

advance. The procuring entity shall ensure before accepting the Fixed Deposit Receipt that the bidder furnishes an undertaking from the bank to make payment/premature payment of the Fixed Deposit Receipt on demand to the **Employer** without requirement of consent of the bidder concerned. In the event of forfeiture of the performance security, the Fixed Deposit shall be forfeited along with interest earned on such Fixed Deposit.

(f) In case of procurement of works, the successful bidder at the time of signing of the contract agreement, may submit option for deduction of performance security from his each running and final bill @ 10% of the amount of the bill

(4) Performance security furnished in the form specified in clause (b) to (e) of sub-rule (3) shall remain valid for a period of sixty days beyond the date of completion of all contractual obligations of the bidder, including warranty obligations and maintenance and defect liability period.

Additional Performance Security-

(1) In addition to Performance Security as specified in clause 4.2.1, an Additional Performance Security shall also be taken from the successful bidder in case of unbalanced bid. The Additional Performance Security shall be equal to fifty percent of Unbalanced Bid Amount. The Additional Performance Security shall be deposited in lump sum by the successful bidder before execution of Agreement. The Additional Performance Security shall be deposited through Demand Daft, Banker's Cheque, Government Securities or Bank Guarantee. Explanation : For the purpose of this rule,-

- i. Unbalanced Bid means any bid below more than fifteen percent of Estimated Bid Value.
- ii. Estimated Bid Value means value of subject matter of procurement mention in bidding documents by the Procuring Entity.
- iii. Unbalanced Bid Amount means positive difference of eighty five percent of Estimated Bid Value minus Bid Amount Quoted by the bidder.

Enhanced performance security for variation: If the original contract price increased either by due to contractor's or due to employer's variation, the 10 % amount shall be deducted from the each running bill equal to amount of variation of the original contract price.

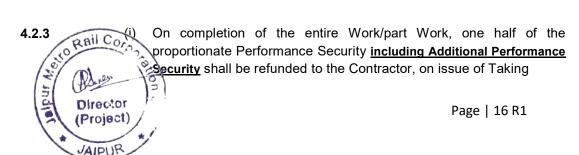
(2) <u>Performance Security and Additional Performance Security shall be</u> payable and encashable at Jaipur only.

4.2.2 Failure of the successful Bidder to furnish the required Performance Security and Additional Performance Security shall be a ground for the annulment of the award of Contract and forfeiture of the Bid Security.

> The whole of the Performance Security **including Additional Performance Security** amount shall be liable to be forfeited by the Employer at the discretion of the Employer, in the event of any breach of contract on the part of the Contractor. The forfeiture of the Performance Security amount by the Employer would be without prejudice to any amount(s) of money that the Employer may recover as Liquidated Damages or any other damages from the Contractor. The forfeiture of Performance Security amount by the Employer, would not operate as bar/set off/ adjustment from any amount of money which becomes recoverable or is recovered by the Employer. In case of the Performance Security Amount Bank Guarantee being invoked and forfeited by the Employer, the Contractor would immediately replenish the amount of Performance Security.

Release

Forfeiture



matters and payments amicably and speedily with the Sub-contractors.

4.5.4 The Contractor shall ensure that their Sub-contractors, material/equipment Suppliers, Consultants and other Agencies deployed by them in connection with execution of the Contract do not make any claim or raise any dispute before JMRC. For this, necessary provision is to be made in the agreement between Contractor and their Sub-contractors/Consultants/other Agencies. Similarly the agreement should also incorporate the provision of dispute resolution. An undertaking in the following format shall be submitted by Contractor in respect of each such agency:-

"Name of Work.....

In connection with above Work, M/s...., Contractor has/is engaging M/s..., as Sub-contractor(or Consultant or material/equipment Supplier or Service provider). For this, the terms and conditions of agreement include necessary provisions for resolution of dispute if any arising between Contractor and Sub-contractor.

It is confirmed by the Sub-contractor that any claim/dispute arising out of the above Work shall be resolved in terms of agreement and shall not be raised before JMRC and also shall not make any claim against JMRC before any forum/court.

Signature of Contractor

Assignment of
Contractor's and4.6The Contractor shall not assign a right or benefit under the Contract without
first obtaining Employer's prior written consent, otherwise than by charge in
favour of the Contractor's bankers of any money due or to become due
under the Contract.Obligationsunder the Contract.

- a. Deleted.
- b. Deleted.

If a Sub-contractor's obligations extend beyond the expiry date of Defects Liability Period then the Contractor shall assign the benefits of such obligations to the Employer.

In the event that a Sub-contractor of any tier provides to the Contractor or any other Sub-contractor a warranty in respect of Plant, Materials or Services supplied in connection with the Works, or undertakes a continuing obligation of any nature whatsoever in relation to such Plant, Materials or Services (including without limitation an obligation to maintain stocks of spare parts) extending for a period exceeding that of the Defects Liability Period or where there is more than one Defects Liability Period exceeding that of the latest Defects Liability Period, and if the Engineer so directs in writing within 21 days of the expiry of the Defects Liability Period or the latest Defects Liability Period (as the case may be), the Contractor shall immediately assign or obtain the assignment of the benefit of such warranty or obligation to the Employer or at the direction of the Employer, to any third Party referred to in Sub-Clause 2.4.

- Compensation for4.7Any breach of Sub-clauses 4.5 to 4.6 shall entitle the Employer to rescind the
Contract under Clause 13.2 of these conditions and also render the Contractor
liable for loss or damage arising due to such cancellation.
- Setting Out 4.8

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Accurate	Setting
Out	

- **4.8.1** The Contractor shall be responsible for
 - a) the accurate setting out of the Works in relation to the original points, lines and levels of reference given by the Engineer in writing
 - Rail the correctness of position, levels, dimensions and alignments of all parts of the Works

the provisions of all necessary instruments, equipment, apparatus and

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- a) the Contractor shall be responsible for keeping unauthorised persons off the Site; and
- b) Authorized persons shall be limited to the Employees of the Contractor, Sub-contractor or persons authorized by the Engineer.

Contractor's4.28Operations on SiteThe Contractor shall confine his operations to the Site, and to any additional
area which may be provided to the Contractor and agreed by the Engineer as
working areas. The Contractor shall take all necessary precautions to keep his
personnel and equipment within the Site and such additional areas, and to keep
and prohibit them from encroaching on adjacent land.

- **Discoveries 4.29** All fossils, coins, articles of value or antiquity, structures and other remains or things of geological or archaeological interest, in addition to oil and other minerals discovered on the Site shall be the absolute property of the Government of India. The Contractor shall take all the necessary precautions to prevent its workmen or its Sub-contractors' workmen or any other person from removing or damaging any such article or thing and shall immediately upon discovery thereof, acquaint the Engineer of such discovery and carry out the instructions of the Engineer.
- **Publicity** 4.30 The Contractor shall not publish or otherwise circulate alone or in conjunction with any other person, any articles, photographs or other materials relating to the Contract, the Site, the Works, the Project or any part thereof, nor impart to the Press, or any radio or television network any information relating thereto, nor allow any representative of the media access to the Site, Contractor's Works Areas, or off-Site place of manufacture, or storage except with the permission, in writing, of the Employer. The Contractor shall ensure that his Sub-contractors of any tier shall be bound by similar obligation and shall, if so required by the Employer, enforce the same at his own expense. The provisions of this Sub-clause shall not exempt the Contractor from complying with any statutory provision in regard to the taking and publication of photographs.
- **Disclosure of 4.31** If the Contractor or any partner of the Contractor or Director of the Contractor's **Relationship 4.31** If the Contractor or any partner of the Contractor or Director of the Contractor's company is closely related to any of the Officers of the Employer or the Engineer, or alternatively, if any close relative of an officer of the Employer or the Engineer has financial interest/stake in the Contractor's firm, the same shall be disclosed by the Contractor at the time of filing his Bid. Any failure to disclose the interest involved, shall entitle the Employer to rescind the Contract, without payment of any compensation to the Contractor. The Contractor shall note that he is prohibited from developing such interest during the Contract period **also**.
- **Use of Explosives 4.32** Explosives if required on the Work shall be used by Contractor only with prior Approval of the Engineer and in the manner and to the extent permitted by him. The Contractor shall be responsible for safe upkeep of such explosives in a special magazine as per the law on explosives as well as for taking all the precautions in the usage of the explosives with proper license and at Contractor's cost, sole risk and responsibility. The Contractor shall hold the Employer harmless and indemnify for the above.

Corrupt / 4.33 Fraudulent/ Collusive/ Coercive Practices Definition 4.33.

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4.33.1 The Employer requires that the Bidders/Contractors, their designated Contractors and/or their Agents observe the highest standards of ethics during Biding and execution of this Contract. In pursuance with this Policy, the Employer:

Rail Connes, for the purpose of these provisions, the terms set forth below as

i) Corrupt practice" means the offering, giving, receiving or soliciting of Director

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anything of value to any officer/employee of JMRC or Engineer or to any other person to influence in the procurement process or in Contract execution and/or after the execution of the Contract.

- ii) "fraudulent practice" means a concealment or misrepresentation of facts in order to influence a procurement process or during the execution of a Contract and/or after the execution of the Contract, which may or may not be to the detriment of the Employer and includes collusive practice among Bidders (prior to or after bid submission) designed to establish bid prices at artificial noncompetitive levels and to deprive the Employer of the benefits of free and open competition and further includes concealment or misrepresentation of facts leading to breach of any of the Contract condition during execution of the Contract which may or may not be to the detriment of the Employer.
- iii) "Collusive practice" means amongst Bidders (prior to or after bid submission) a scheme or arrangement designed to establish bid prices at artificial non-competitive levels and to deprive JMRC of the benefits of free and open competition.
- iv) "coercive practice" means impairing or harming or threatening to impair or harm directly or indirectly, any Agency or JMRC or its employees/ consultants or its property, to influence improperly the actions of an Agency or JMRC or its employees/ consultants, obstruction of any investigation or auditing of a Procurement/ Contract process.
- v) [Deleted].
- vi) [Deleted].
- vii) [Deleted].

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- b. If it is found that the Bidder/Contractor has indulged in corrupt/fraudulent/ collusive/coercive practices, actions such as rejection of bid/forfeiture of Bid Security or rescission/termination of Contract/forfeiture of Performance Security etc.
- c. Debarment from bidding.-

(1) A bidder shall be debarred by the State Government if he has been convicted of an offence -

(i) under the Prevention of Corruption Act, 1988 (Central Act No. 49 of 1988); or

(ii) under the Indian Penal Code, 1860 (Central Act No. 45 of 1860) or any other law for the time being in force, for causing any loss of life or property or causing a threat to public health as part of execution of a public procurement contract.

(2) A bidder debarred under sub-section (1) <u>of section 46 of RTPP Act-2012</u> shall not be eligible to participate in a procurement process of any procuring entity <u>of the State/JMRC</u> for a period not exceeding three years commencing from the date on which he was debarred.

(3) If a procuring entity finds that a bidder has breached the code of integrity prescribed in terms of section 11 <u>of RTPP Act-2012</u>, it may debar the bidder for a period not exceeding three years.

(4) Where the entire bid security or the entire performance security or any procuring entity in respect of any procurement process or procurement contract, the bidder may be debarred from participating in any procurement process undertaken by the procuring entity for a period not exceeding three years.

		Contractor reasonable notice of such date. If the Contractor fails to remedy the defect or damage by such date and the necessity for such Work is due to a cause stated in Sub-clause 10.2(a), (b) or (c), the Employer may (at his sole discretion):
		 a) carry out the Work himself or by others, in a reasonable manner and at the Contractor's risk and cost, but the Contractor shall have no responsibility for such Work: the costs incurred by the Employer in remedying the defect or damage shall be recoverable from the Contractor by the Employer;
		b) require the Engineer to determine and certify a reasonable reduction in the Contract Price; or
		c) if the defect or damage is such that the Employer has been deprived of substantially the whole of the benefit of the Works or parts of the Works, terminate the Contract in respect of such parts of the Works as cannot be put to the intended use, the Employer shall then be entitled to recover all sums paid for such parts of the Works together with the cost of dismantling the same, clearing the Site and returning Plant, Rolling Stock and Materials to the Contractor, and Sub-clause 13 shall not apply.
		Notwithstanding anything contained herein the Employer would be entitled in urgent and critical situation(s)/events to remedy the defects in the Work by himself or through others, at the Contractor's risk and cost. The cost incurred by the Employer in remedying the defect or damage shall be recoverable from the Contractor by the Employer.
Removal of Defective Work	10.5	If the defect or damage is such that it cannot be remedied expeditiously on the Site and if the Employer gives consent, the Contractor may, remove from the Site for the purposes of repair any part of the Works, which is defective or damaged. This consent may require the Contractor to increase the amount of Performance Security by the full replacement cost of these items or to provide other appropriate Security acceptable to the Employer.
Further Tests	10.6	If the remedying of any defect or damage is such that it may affect the performance of the Works, the Engineer may require that Tests on Completion, including Integrated Testing, be repeated to the extent necessary. The requirement shall be made by notice within 28 days after the defect or damage is remedied. Such Tests shall be carried out in accordance with Clause 7.11
Right of Access	10.7	Until the Performance Certificate has been issued, the Contractor shall have the right of access to all parts of the Works and to records of the working and performance of the Works, except as may be inconsistent with any reasonable security restrictions by the organisation responsible for operating the Works.
Contractor to Search	10.8	The Contractor shall, if required by the Engineer, search for the cause of any defect, under the direction of the Engineer. Unless the defect is one for which the Contractor is liable, the Cost of such search shall be added to the Contract Price.
Performance Certificate	10.9	The Contract shall not be considered to be completed until the Performance Certificate has been signed by the Engineer or authorized official of the Employer and delivered to the Contractor at the end of 'Defect Liability Period, stating the date on which the Contractor completed his obligations related to completion of works and rectification of defects during Defect Liability Period to the Engineer's satisfaction. Only the Performance Certificate shall be deemed to constitute approval of the Works.
		Notwithstanding anything contained herein the Contractor would continue to remain liable to the Employer for any cost, loss, damage or compensation which arises from hidden or latent defect in the work executed by the Contractor under the Contract, even if such hidden and latent defects arise after the expiry of Defect Liability period or grant of Performance Certificate by the Employer under the Contract to the Contractor. After the Performance Certificate has been issued, the Contractor and the
Unfulfilled Obligations	10.1000 Jundier	After the Performance Certificate has been issued, the Contractor and the impoloyer shall remain liable for the fulfilment of any obligation, which remains difference at that <u>time</u> . For the purposes of determining the nature and Director (Project) Page 44 R1

		extent of any such obligation, the Contract shall be deemed to remain in force.
Emergency defect rectification	10.11	If any defect or damage is one requiring immediate attention from safety, environmental or operational viewpoint, the Engineer has the authority to proceed with rectification in any manner suitable and deduct such sums from the Contract Price.
	11	Contract Price and Payment
The Contract Price Inclusions/ Exclusions	11.1	
	11.1.1	 Unless otherwise stated in the Special Conditions of Contract, the Contract Price, subject to any adjustment thereto in accordance with the Contract, shall be all inclusive (including all taxes, duties, royalties etc.)
		 Nothing extra shall be payable over the quoted rates, notwithstanding any provision to the contrary in any law for the time being in force, save and except what is specifically provided in General or Special Conditions of Contract.
		iii) The payment (as per this Sub-clause) of whatsoever nature shall be provided only for Permanent Works. No <u>payment</u> (as per this Sub-clause) shall be provided for Temporary Works and fuel.
Maintaining Records and Availing Exemptions	11.1.2	 i) In the event of exemption of custom duties, GST (CGST/IGST/SGST etc.) or any other cess/levy being granted by the Government in respect of the Works, the benefit of the same shall be passed on to Employer. The Contractor shall therefore maintain meticulous records of all the taxes and duties paid and provide the same as and when required by the Employer, so that the Employer is able to avail the reimbursement for which JMRC may issue a procedure order separately. Alternatively, the Employer may direct the Contractor to get the reimbursements based on exemption certificates / government's order and it shall be obligatory on part of the Contractor to get the reimbursements from the statutory authorities and pass on the benefit to JMRC. ii) In case of Contractor's failure in availing the exemptions as stipulated above, the recovery of equivalent amount will be made from Contractor's dues.
Adjust in Contract Price	11.1.3	Adjustment in Contract price shall be done if a "Price Variation Formula" is given in the Special Conditions Of Contract otherwise it will be a fixed price contract.
Change in Taxes/Duty	11.1.4	 i. The liability, if any, on account of quarry fees, royalties, octroi and any other taxes and duties in respect of materials actually consumed <u>on</u> public work, shall be borne by the Contractor. ii. If any rates of Tax are increased or decreased, a new tax is introduced in India only, an existing Tax is abolished, or any change in interpretation or application of any Tax resulting from a change or Introduction in India only due to any National or State Statute, Ordinance, Decree or other law or any regulation or bye-law of any local or other duly constituted authority in India only, in the course of performance of contract, which was or will be assessed on the Contractor, in connection with the performance of the Contract, an equitable adjustment of the Contract price shall be made to fully take into account any such change by addition to the Contract Price or deduction there from, as the case may be. However, these adjustments would be restricted to direct transactions between the Employer and Contractor only those items which are included in account of variation in deemed export benefits, if any. Any increase or developed to variation in deemed export benefits, if any. Any increase or developed to variation in deemed export benefits, if any. Any increase or developed to variation in deemed export benefits, if any. Any increase or developed to variation in deemed export benefits, if any. Any increase or developed to variation in deemed export benefits, if any. Any increase or developed to the proven the proven as which is included in price variation formula incorporated to the proven as the case of the performance or developed to the performance of the performance or developed to the performance or performance or developed to the performance or provention in deemed export benefits, if any. Any increase or developed to the performance or performance or performance or performance or performance or pe

in the contract shall not be accounted for this purpose. Such increase including GST shall not be made in the extended period of contract for which the contractor alone is responsible for delay as determined by authority for extension of time.

Advances 11.2 In respect of works costing more than Rs. 50.00 Crore (Rs. Fifty Crore) only the JMRC will, Mobilisation 11.2.1 Advance if provided in bidding document and requested by the Contractor to make mobilization advance, payment to the Contractor (at 9% per annum interest compounded annually basis) to assist in defraying the initial expenses that necessarily be incurred by the Contractor for mobilization. The total of such advance payments and the number & timing of installments is stated here under-The total amount of Advance shall not be more than 10% of the original contract value. Payment of Mobilization Advance shall be made in two equal installments, the first installment shall not be more than 5% of the original contract value and on compliance of the requisite conditions as stated in the bid document, the remaining amount of original contract value shall be in second installment. **Release of Mobilization Advance:** On recommendation of the Engineer-in-charge, Mobilization Advance shall be released, as follows: (i) Execution of the Agreement by the parties thereto, (ii) Submission by the Contractor of an unconditional and irrecoverable bank guarantee in amounts and currencies equal to the advance payment being requested. Such bank guarantee shall be issued either by a Nationalized or Scheduled Bank as declared by the RBI, should be encashable in Rajasthan and acceptable to JMRC. The guarantee shall remain effective until the full recovery of the advance payment with total interest payable thereon. If the advance payment has not been repaid by the date 28 days prior to expiry date of B.G. the contractor shall extend the validity of B.G. until the advance payment has been repaid. (iii) The mobilization advance payments shall be made in two installments as stated above, subject to the conditions described below. The advance payments shall be used by the Contractor exclusively for mobilization expenses, as per the programme approved by the Engineer-in-charge. (iv) For this purpose, the Contractor shall open a dedicated Contract Bank Account in a bank located at office headquarter or in case of non-functioning of bank's branch at office headquarter than at the nearest place to office headquarter in Rajasthan and the JMRC will transfer or deposit the advance

headquarter in Rajasthan and the JMRC will transfer or deposit the advance payments directly into the aforesaid dedicated Bank Account of the Contractor. The Contractor will not be permitted to use these funds for any purpose other than for expenditures under the Contract and the JMRC will be entitled to verify that the transactions from this account are used exclusively for the purposes for which they are intended. In case the advance payment is not utilized by the Contractor as per the approved programme and within the stipulated period to the satisfaction of the Engineer-in-charge, default proceedings as per the relevant clause of Contract, shall be initiated against the Contractor.

Release of First Installment: The JMRC will make, payment of the first installment of the mobilization advance only after the Contractor has fulfilled the following conditions :-

(a) Contractor has executed the agreement with JMRC

(b) Requisite Bank Guarantee has been deposited by the contractor.

(c) Established the dedicated Contract Bank Account.

Red Gary other condition mentioned in bid document in order to release installment.

Second Installment: After the first installment of the advance payment has been utilized as per the approved programme, substantiated by

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Contract in this regard.

The Contractor, if required by the Engineer shall provide the details of utilisation of Mobilization Advance.

Provisional 11.3 Payment Against Material at Site

11.3.1 A provisional payment on account of main construction materials required for the Permanent Works, shall be paid on request of the Contractor after these materials are brought to Site, against an Indemnity Bond in a form acceptable to Employer is duly executed. The payment shall be limited to 80% of the actual value or assessed value of these materials and the total of such provisional payment on account of construction materials at a time shall be limited to three percent of Original Contract Value or likely average consumption of such materials for three months, whichever is less and at any time the total outstanding provisional payment against material at site shall not exceed four percent of the Original Contract Value. The valuation of the average consumption of such main construction materials shall be approved by the Engineer, whose decision shall be final.

11.3.2 The provisional payments as admissible, shall be payable only on Contractor's written request to the Employer/Engineer.

for Advances/ Provisional Payment against Material at Site Recovery of 11.3.3 Provisional Payment against

Material at Site

Written Request

a. Deleted.

- b. Deleted.
- c. In case of provisional payment against Materials, the amount consumed every month shall be recovered from the next month's on-account bill and the recovery to be completed in 3 monthly installments. In case recovery could not be made due to any reason, interest will be charged at the rate equal to State Bank of India's Marginal Cost of fund based Lending Rate (MCLR) applicable for tenure of 01 year prevailing on the due date of recovery.

Application for Interim Payment Certificates 11.4

11.4.1 In case of 'Lump Sum' Contract with cost centre and Milestone payment, the fixed Lump Sum Price shall be apportioned by the Contractor amongst the various Cost Centres. The amount thus apportioned under each Cost Centre will be further apportioned amongst various Milestones with the approval of the Employer. The Contractor shall be entitled to submit to the Engineer requests for interim payments only upon the achievement of one or more of the Milestones described in the Cost Centre.

At the beginning of each month, the Engineer shall issue to the Contractor certificate in respect of each Milestone due to be achieved in the preceding month stating:

(i) the date on which the Milestone was achieved; or

(ii) the non-achievement of the Milestone.

beginning of each month, in a form approved by the Engineer, showing

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procures less than the quantity specified in the bidding documents due to change in circumstances, the bidder shall not be entitled for any claim or compensation except otherwise provided in the bidding documents.

(2) Orders for extra items may be placed by the procuring entity in accordance with the Schedule of Powers of JMRC, up to 5% of the value of the original contract, if allowed in the bidding documents. The fair market value of such extra items payable by the procuring entity to the contractor shall be determined by the procuring entity in accordance with guidelines prescribed by the <u>administrative</u> deptt.

(3) Orders for additional quantities may be placed, if allowed in the bidding documents, on the rates and conditions given in the contract and the original order was given after inviting open competitive bids. Delivery or completion period may also be proportionately increased. The limits of orders for additional quantities shall be as under :-

(a) 50% of the quantity of the individual items and 50% of the value of original contract in case of works; and

(b) 50% of the value of goods or services of the original contract.

Provided that in exceptional circumstances and without changing the scope of work envisaged under the contract, a procuring entity may procure additional quantities beyond 50% of the quantity of the individual items as provided in the original work order with prior approval of the administrative deptt. as follows :-

(i) the procuring entity shall obtain prior approval for revised requirements from the competent authority for reasons to be recorded in writing. Wherever necessary, due to the quantum of orders for additional quantities, the procuring entity shall obtain prior and revised technical, financial and administrative sanctions from the competent authorities;

(ii) that the additional quantities so procured shall be part and parcel of the work being executed;

(iii) that the limit of 50% of the value of original contract shall not be exceeded in any case

(4) Deriving Rates For New Items / Negotiation :

This Sub-clause shall be applicable to all Schedules of BOQ including Lump-Sum Schedule.

(i) In case Engineer introduces an item for which the Contract does not contain any rates or prices applicable to the varied Works, the rate of such items shall be derived, wherever possible, from rate for similar items available in the Bill of Quantities of the accepted Tender. In case this is not possible, the rate may be decided on the following basis:

a) Cost of Materials at current market price, as actually utilized in the final finished Permanent Works, including a reasonable percentage for wastage and transportation.

b) Cost of enabling works if any (unless provided for separately) worked out on the above basis but with less stringent quality. Specifications minus salvage value of serviceable material released after completion of Work and cost of material released as scrap.

c) Cost of labour actually used at the site of Work at rates under Payment of Minimum Wages Act for the area of Work for each category of worker, further enhanced by a percentage of 10% of the aforesaid rates to account for labour not directly utilised at Site and other ancillary and incidental expenses on labour.

d) Hire charges for Plant & Machinery, scaffolding, shuttering, forms, etc., required to be used at the site of the work. The tools used by the various trades shall not be counted as Plant & Machinery for this purpose.

An amount of 20% of items $\underline{4}(i)$ a), b), c) and d) above to allow for Contractor's overheads including water/electricity charges and labour cess etc., profits and porporate taxes etc. No such percentage shall be applicable to the

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estimated cost of Materials supplied free of cost to the Contractor.

f) In all cases where extra items of Work are involved, for which there are no rates in the accepted Bill of Quantities, the Contractor shall give a notice to the Engineer, of at least 7 days before the need for its execution arises.

(5).Value Engineering:

The Contractor may, at any time, submit to the Engineer-in- charge a written proposal which (in the Contractor's opinion) will, if adopted, (i) accelerate completion, (ii) reduce the Cost to the **Employer** of executing, maintaining or operating the Works, (iii) improve the efficiency or value to the **Employer** of the completed Works, or (iv) otherwise be of benefit to the **Employer**.

The proposal shall be prepared at the Cost of the Contractor and shall include the items such as Deviations, Variations and Pricing.

If a proposal, which is approved by the Engineer-in-charge, includes a change in the design of part of the Permanent Works, then unless otherwise agreed by both Parties:

- i. the Contractor shall design this part,
- ii. Contractor's General Obligations as per GCC 4.1 shall apply, and
- iii. If this change results in a reduction in the Contract value of this part, the Engineer-in-charge shall proceed in accordance with Clause 3.5 to agree or determine a fee, which shall be included in the Contract Price.

	13	Termination of the Contract	
Notice to Contractor	13.1	If the Contractor fails to carry out any of his obligations, or if the Contract not executing the Works in accordance with the Contract, the Engine give notice to the Contractor requiring him to make good such faile remedy the same within such time as the Employer / Engineer may dee reasonable.	eer may ure and
Termination of Contract Due to Contractor's Default	13.2		
Conditions Leading to	13.2.1	The Employer shall be entitled to terminate the Contract if the Contractor one of its constituents,	or any
termination of Contract		a) fails to comply with a notice under Sub-clause 13.1	
Contract		b) abandons or repudiates the Contract	
		c) without reasonable excuse acceptable to the Engineer, fails to cor the Works in accordance with the Contract	nmence
		d) Sub-contracts the whole of the Works or assigns the Contract approval of the Employer	without
	10	Recomes bankrupt or insolvent or goes into liquidation except ve inquidation for the purpose of amalgamation or reconstruction	oluntary
	* Jeipur A.e.	 c) without reasonable excuse acceptable to the Engineer, fails to cor the Works in accordance with the Contract d) Sub-contracts the whole of the Works or assigns the Contract approval of the Employer c) comments bankrupt or insolvent or goes into liquidation except verification for the purpose of amalgamation or reconstruction c) persistently disregards instructions of the Engineer or contravenes ar D) rector Page 54 I 	יא R1

- (a) Provision in NIT,
- (b) Outline Design Specifications / Outline Construction Specifications for Civil Works, Technical specifications Architectural & Finishing works
- (c) MORTH Specification for road & Bridges,
- (d) CPWD specifications,
- (e) Standard Codes of Practice

In case of discrepancy among Standard Codes of Practice, the order of precedence will be IRS, IRC, IS, EURO, DIN, BS.

2.6 DIMENSIONS

- 2.6.1 As regards errors, omissions and discrepancies in Specifications and Drawings, relevant clause of Special Conditions of Contract will apply.
- 2.6.2 The levels, measurements and other information concerning the existing site as shown on the conceptual / layout drawings are believed to be correct, but the Contractor should verify them for himself and also examine the nature of the ground as no claim or allowance whatsoever will be entertained on account of any errors or omissions in the levels or strata turning out different from what is shown on the drawings.

2.7 ASSOCIATED WORKS

Works to be performed shall also include all general works, preparatory works for the construction and works of any kind necessary for the design and satisfactory construction, completion and maintenance of the works to the intent and meaning of the drawings adopted and Outline Construction Specifications for Civil Works & Technical specifications Architectural & Finishing works, to best Engineering standards and orders that may be issued by the Engineer from time to time, compliance by the agency with all Conditions of Contract, supply of all materials, apparatus, plants, equipment, tools, fuel, water, strutting, timbering, transport, offices, stores, workshop, staff, labour and the provision of proper and sufficient protective works, diversion, temporary fencing, lighting and watching required for the safety of the public and protection of works on adjoining land; first-aid equipment, sanitary accommodation for the staff and workmen, effecting and maintenance of all insurances, the payment of all wages, salaries, fees, royalties, duties or the other charges arising out of the erection of works and the regular clearance of rubbish, clearing up, leaving the site perfect and tidy on completion.

2.8 CONSTRUCTION DEPOT & DUMPING AREA

For casting yard, batching plant and other activities a plot of land of approx. **35000 Sam**. will be made available by JMRC on as is where is basis within **45 Km** from the work site free of cost. This land shall be made good for such offsite activities as needed by the Contractor at no extra cost to the employer. The land shall be cleared from debris, all structures made by the contractor including, RCC footings and rafts etc. and reinstated to the line, level and to the same conditions as existed before the work started before handing over back to the Employer within 60 days after Taking over Certificate. The final bill shall be released to the contractor after all structures from the construction depot are removed & clearance of site. The cost of setting of yard & reinstatement is included in lump sum price in schedule 'A'.

A mechanical tyre washing plant shall have to be installed by the contractor for the vehicles leaving the depot and construction sites to avoid the spillage on the connecting roads.

C&D waste generated of one construction depot, site and station during construction to be transported to ocation designated for this purpose by JMRC within 25 Km lead from the



6.4.5 Protection of Prestressing Steel

Prestressing steel shall be continuously protected against corrosion, until grouted. 'The corrosion protector shall have no deleterious effect on the steel or concrete or on the bond strength of steel to concrete. Grouting shall conform to these specifications or as directed by the Engineer.

6.4.6 Sheathing

The joints of all sheathings shall be water-tight. Special attention shall be paid to the junction at the anchorage end, where the sheathing must tightly fit on the protruding trumpet end of anchorage and thereafter sealed preferably with adhesive water proof tape as per approved manufacturer.

The sheathing and all joints shall be water tight. Any temporary opening in the sheathing shall be satisfactorily plugged and all joints between sheathing and any other part of the prestressing system shall be effectively sealed to prevent entry of mortar, dust, water or other deleterious matter. Sheathing shall be neatly fitted at joints without internal projection or reduction of diameter. Sheathing shall be firmly tied so that while concreting they should not float up. Sheathing shall be aligned accurately with respect to vertical and horizontal coordinate. Enlarged portions of the sheathing at couplings or anchorages shall be of sufficient length to provide for the extension of the tendons.

6.4.7 Grout Vents

Grout vents of at least 20 mm diameter shall be provided at both ends of the sheathing and at all valleys and crests along its length. Additional vents with plugs shall also be provided along the length of sheathing such that the spacing of consecutive vents does not exceed 20 m. Each of the grout vents shall be provided with a plug or similar device capable of withstanding a pressure of 1.0 MPa without the loss of water, air pressure or grout.

6.4.8 Anchorages

All bearing surfaces of the anchorages shall be cleaned prior to concreting and tensioning. Anchor cones, blocks and plates shall be securely positioned and maintained during concreting such that the centre line of the duct passes axially through the anchorage assembly. The anchorages shall be recessed from the concrete surface as per drawings.

After the prestressing operations are completed and prestressing strands are cut, the surface shall be painted with two coats of epoxy of suitable formulation having a dry film thickness of 80 microns per coat and entire recess shall be filled with concrete or non-shrink/pre-packaged mortar or epoxy concrete within 7 days of grouting(in case of stressing and grouting are done in two or more stages, the recess filling should be done within 7 days of last stage grouting but in no case it shall be more than 14 days)

6.4.9 Handling and Storage

Care shall be taken Gowood mechanically damaging, work-hardening or heating prestressing rendons while handling. All prestressing tendons shall be stored clear of the



8.1.5 Alignment of Piles:

- i) Piles shall be installed as accurately as possible according to the drawings either vertically or to the specified batter. All deviations will be measured at the cut off level of the piles. The deviation from the true axis shall not be more than 1.5% for vertical piles and 4% for rake piles. Piles should not deviate in location by more than 75mm when used in groups. For single or 2 piles used under columns, deviation shall not be more than 50mm.
- ii) The Contractor shall maintain a record of actual pile locations in the form of drawing and submit the information to the Engineer at suitable intervals.

8.1.6 Pile Cap:

Pile caps shall be of reinforced concrete. A minimum offset of 250 mm shall be provided beyond the outer faces of the outer most piles in the group. If the pile cap is in contact with earth at the bottom, a leveling course of minimum 75 mm thickness of PCC of grade M15 shall be provided or as shown in the drawings.

The attachment of the pile head to the cap shall be adequate for the transmission of loads and forces. A portion of pile top may be stripped of concrete and the reinforcement anchored into the cap. Manual chipping may be permitted after three days of pile casting while pneumatic tools for chipping shall not be used before seven days after pile casting. The top of pile after stripping shall project at least <u>50mm</u> into the pile cap. Concreting of the pile cap shall be carried out in dry conditions. All the operations and tools required for making the pile in dry condition is included in the item.

The road surface after casting of pile cap should be repaired immediately. If the surface is not repaired immediately, penalty will be imposed as decided by the Engineer.

8.1.7 Testing of Piles:

- iii) The load tests shall be in accordance with the Indian Standard Code of Practice for Design and Construction of Pile Foundations IS 2911 (Part IV) Load Tests on Piles. For initial load test, test load will be 2.5 times the theoretical designed capacity of pile. For initial load, test arrangement to be designed shall also cater for additional 25% above test load and nothing extra will be paid on this account. Permissible stresses in test arrangement (steel truss or plate girder) to cater for test load plus additional 25% load shall be within permissible stresses as per IS: 800 (as for permanent structure). For test frame, steel of Grade –B conforming to IS: 2062 shall be used.
- iv) Engineer will decide the locations of initial and routine horizontal and vertical load test. One no. initial load test is to be performed in each km for each diameter of pile being used in viaduct. The contractor shall undertake test piles required for initial pile load test in the initial stages of work using the same methodology and equipment"s which will be subsequently used for working piles. These tests shall be undertaken well in advance of working pile. No working pile would be allowed to undertaken till initial satisfactory initial pile load tests have been completed.



Non-granting of permission for pile/ pile cap by Engineer in such respect will not be considered as reason for delay or any claim thereof. The test arrangement to be employed shall be of nature which is quick to install and remove and easily transferable. <u>At every</u> one KM of viaduct initial load test both vertical and horizontal are to be performed by the contractor for each type of pile. Also one initial load test both vertical and horizontal per station are to be performed by the contractor for each type of pile.

- iii) Routine horizontal & vertical load tests are performed as a check on the load carrying capacity and settlements of the pile foundations. At least one routine test shall be performed for every 100 piles unless otherwise specified by the Engineer. <u>Initial and routine vertical and horizontal load test shall be conducted on different piles.</u>
- iv) The Contractor shall give the Engineer at least 48 hours notice of the commencement of construction of these piles which are to be subjected to Initial Tests.
- v) The load tests shall not normally be conducted unless the concrete is at least 28 days old. However in special circumstances, permission can be given by Engineer for prior testing.
- vi) All testing shall be done under the direction of experienced personnel conversant with the equipment and the testing procedure.
- vii) Before the commencement of the tests all the particulars regarding the test pile including boring data and concrete cube strengths shall be made available at site and shall form a part of the test report.
- viii) On completion of each load test the Contractor shall submit a report of the load test which shall include the following information.
 - a) Description of soil conditions, ground water table, actual boring and installation records, concrete cube test results.
 - b) Method of load application
 - c) Load settlement readings during loading and unloading
 - d) Time load-settlement curve
 - e) All other observation relevant to the test being conducted.
- ix) Integrity test

Two types of pile integrity tests will be performed:

Dynamic Integrity Test:

The Dynamic Integrity test using pile driving analyser or approved equivalent for pile integrity shall be performed on all the piles. The top of the pile shall be made accessible, chipped off up to hard concrete, levelled by trimming it back as far as practicable. The reinforcing bars of the piles tested shall be bent sideways. The test shall be performed after removal of bad/ weak concrete at top so that the wave propagation is steady through hard concrete. The test shall be carried out at minimum 3 locations on each pile in such a way that the entire cross section of the piles tested with a minimum age of



Grades of raw elastomer of proven use in elastomeric bearings, with low crystallization Grades of raw elastomer of proven shelf life (o.g. Neoprene WRT, Bayprene 110 Skyprene B- and Denka S-40V) as indicated in latest revision of IRC-83, Part II) shall be used.

No reclaimed rubber or vulcanized wastes or natural rubber shall be used.

The raw elastomer content of the compound shall not be lower than 60 per cent by its weight. The ash content shall not exceed 5 percent (as per tests conducted in accordance with ASTM D-297, sub-section 10).

EPDM and other similar candidate elastomer for bridge bearing use shall not be permitted.

b) Properties

The elastomer shall conform to the properties specified in Clause 4.3.1 of the IRICEN publication titled "Bearings for Railway Bridges" and those specified in Table 2000-1 of the publication titled "Specifications for Road and Bridge Works", published by IRC on behalf of MORTH (Roads Wing).

c) Fabrication and Tolerances

Fabrication and Dimensional tolerances shall be governed by the specifications laid down in Clause 4.3.2 of the IRICEN publication & Clause 2005.3 of the MORTH specifications mentioned above.

d) Acceptance Specifications

For inspection and testing requirement Clause 4.4 of the above mentioned IRICEN publication shall be referred with modifications of lot size as mentioned below:-

Sampling testing and acceptance consideration will be made on a lot basis. A lot shall be defined as those bearings presented for inspection at a specific time or date. A lot shall be further defined as the smallest number of bearings as determined by the following criteria.

- i. A lot shall not exceed a single contract or project quantity;
- ii. A lot shall not exceed 50 bearings;
- iii. A lot shall consist of those bearing of the same type regardless of load capacity.

Accepting and testing requirements shall also conform to the specifications laid down in Clause 2005.4 of the referred MORTH specifications.

In addition to tests mentioned above, all bearings shall be also weight actually and compared with the theoretical weight.

All bearings shall carry a warrantee of not less than 15 years in an approved format. The contractor shall be responsible for immediate repair or replacement of the bearings in case of failure / distress to the satisfaction of the owner at no extra cost to the Owner within the warrantee period.

Criteria for Selection of bearing manufacturer shall conform to requirement of Most letter No-RW/NH-34057(1) / 95-(S & R) dated 2^{nd} November,2000. It is necessary that all manufacturers of all elastomeric bearings shall have in house facilities for carrying

out Infrared Spectro-Photometry as per ASTM D-3677.

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ANNEXURE A

SPECIFICATION OF CRYSTALLINE PRODUCTS

Product - Integral Crystalline Waterproofing/Durability Admixture

CRYSTALLINE ADMIX

Dosage - minimum 0.8% by weight of cement + cementitious material (OR such lower dosage as recommended by Manufacturer at which product meets the product qualification criteria listed in this document- Duly approved by JMRC).

Integral Waterproofing/ Durability admixture should be SINGLE part cementitious powder consisting of hydrophilic chemicals. When added to plastic mix, will permanently create impermeable hardened concrete by developing insoluble needle like crystals to seal the pores, capillaries, micro-cracks in the whole mass of concrete and enhances the durability of concrete. The crystalline admixture must be compatible with any other concrete admixture confirming to ASTM D494 and IS 9103. It shall be used for all underground structures (including shortcrete in tunnel lining). In addition, the waterproofing admixture must confirm to the following requirements:

- i. It shall possess CE approval as per EN934-2.
- ii. The crystalline admixture shall be compatible with any other concrete admixture confirming to ASTM D494. The product shall be approved by MORTH & must have IRC accreditation for durability enhancement.
- iii. At the manufacturer's recommended dosage, material must fulfil the requirements of American Concrete Institute Guidelines ACI-212-3R-10 Chapter 15 and fall under PRAH (Permeability reducing Admixtures for HYDROSTATIC conditions) and must reduce Coefficient of Permeability of concrete by more than 90%(preferably zero permeability), when compared to control concrete and tested as per DIN 1048 Part 5 by carrying out 4 cycles each of 5 bar Hydrostatic Pressure for 72 hours and drying for 48 hours between the cycles & Coefficient of Permeability calculated as per Darcy's Formula/ Valenta equation by incorporating penetration values obtained at the end of fourth cycle pressure.
- iv. At the manufacturer's recommended dosage rate, the material must reduce Chloride Diffusion Co-efficient by minimum 45% when tested as per ASTM C 1556 -4 / or its equivalent and compared with the control concrete, thereby prolonging the durability & service life of the treated concrete structure.
- v. At the manufacturer's recommended dosage rate, the crystalline admixture treated concrete must be able to withstand high hydrostatic pressure of 16 bar (156 M of water head) when tested as per DIN 1048



6.7.4 Response Reduction Factor

Response Reduction Factor "R" as per IRS Seismic code Table -3 shall be as given below

S.No.	Elements	Response Reduction Factor "R"
1	RCC Pier with ductile detailing	3.0
2	PSC Pier/Pier cap/Portal beam	2.0
3	Portal Pier with ductile detailing	3.0-In Longitudinal direction
	(Beam integral with pier)	4.0-In transverse direction
4	Bearing/Superstructure	2.0
5	Stopper	1.0
6	Foundations	2.0

Note: In addition to the response reduction factor given above, reinforcement detailing of Piers/Portal Piers shall conform to ductility/capacity design requirements as per Annexure-B of IRS Seismic Code.

6.7.5 Vertical Seismic Coefficient

The seismic zone factor & time period (of Vertical motion) for calculating vertical seismic coefficient shall be considered as per clause 7.3.2 & 9.4.2 of IRS seismic code. The Zone factor for calculating the vertical seismic coefficient will be 2/3*Zone factor i.e. 2/3*0.1=0.067. For Pier & foundations, while calculating vertical seismic coefficient R=1 shall be considered.

6.7.6 Computation of Fundamental period of vibration

The fundamental time period shall be calculated by any rational method of analysis. Each pier is considered as a single degree of freedom oscillator with mass placed at the Centre of Gravity (COG) of the deck.

The time period can also be calculated based on expression given in Clause 8.1 of IRS Seismic Code, which is as follows:

$$T = 2\pi \sqrt{\frac{\delta}{g}}$$

Where δ = horizontal displacement at the top of pier due to horizontal force (= mg) Where m = lumped mass at the top of pier.

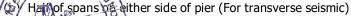
a) Mass

Permanent masses (Self Weights, SIDL) of:

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(a) Full span longitudinally, which can be resisted by reaction blocks of POT/Spherical bearings during earthquake, at one side of the perior barrow of the



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7. ANNEXURE-A : LOAD COMBINATION

						ULSS	STATIC				
		1001	1002	1003	1004	1005	1101	1102	1103	1104	1105
L/C	Descriptions of Load Case	S	ubmerged Soi	I -Design Wat	er Level Ca	se		Sat	urated / Dry (Case	
No.	Descriptions of Load Case	(MAX H - MAX V)	(MAX H - MAX V) without LL	(MAX H - MIN V)	(MIN H - MAX V)	(MIN H - MAX V) without LL	(MAX H - MAX V)	(MAX H - MAX V) without LL	(MAX H - MIN V)	(MIN H - MAX V)	(MIN H - MAX V) without LL
1	Self Weight	1.5	1.5	1.0	1.5	1.5	1.5	1.5	1.0	1.5	1.5
2	SIDL	1.5	1.5	1.0	1.5	1.5	1.5	1.5	1.0	1.5	1.5
3	Soil Back Fill	1.5	1.5	1.0	1.5	1.5	1.5	1.5	1.0	1.5	1.5
4	Live Load on concourse & platform	1.5	0	0	1.5	0	1.5	0	0	1.5	0
5	Train Live Load	1.5	0	0	1.5	0	1.5	0	0	1.5	0
6	Lateral Earth Pressure (WL @ Design Water Level*) K0	1.5	1.5	1.5	0	0	0	0	0	0	0
7	Lateral Earth Pressure (WL @ Design Water Level*) Ka	0	0	0	1.0	1.0	0	0	0	0	0
8	Lateral Earth Pressure Sat_K0 (#)	0	0	0	0	0	1.5	1.5	1.5	0	0
9	Lateral Earth Pressure Dry_ Ka (#)	0	0	0	0	0	0	0	0	1.0	1.0
10	Vertical Surcharge Load	1.5	1.5	0	1.5	1.5	1.5	1.5	0	1.5	1.5
11	Lateral Surcharge load (Towards Right)	0	0	0	0	0	0	0	0	0	0
12	Lateral Surcharge load (Towards Left)	0	0	0	0	0	0	0	0	0	0
13	Lateral Surcharge load (Both Sides)	1.5	1.5	1.5	0	0	1.5	1.5	1.5	0	0
14	Water Pressure at Design Water Level* (Lateral)	1.5	1.5	1.5	1.0	1.0	0	0	0	0	0
15	Water Pressure at Design Water Level* (Vertical) (Uplift)	1.5	1.5	1.0	1.5	1.5	0	0	0	0	0
16	0.075 g Racking Point Force (Towards Right)	0	0	0	0	0	0	0	0	0	0
17	0.075 g Racking Point Force (Towards Left)	0	0	0	0	0	0	0	0	0	0
18	0.075 g Racking Distribution Force (Towards Right)	0	0	0	0	0	0	0	0	0	0
19	0.075 g Racking Distribution Force (Towards Left)	0	0	0	0	0	0	0	0	0	0
20	0.15 g Racking Point Force (Towards Right)	0	0	0	0	0	0	0	0	0	0
21	0.15 g Racking Point Force (Towards Left)	0	0	0	0	0	0	0	0	0	0
22	0.15 g Racking Distribution Force (Towards Right)	0	0	0	0	0	0	0	0	0	0
23	0.15 g Racking Distribution Force (Towards Left)	0	0	0	0	0	0	0	0	0	0

Note:

* During Construction stage HRL shall be considered instead of Design water table for all load combinations. Lateral Earth pressure shall be calculated based on submerged density up to water table and saturated density above water table. # Lateral Earth Pressure Dry_Ka shall be calculated with saturated soil density up to GL and Lateral Earth Pressure Dry_Ka shall be calculated with dry soil density up to GL.

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						ULS SEIS	MIC (RACKING 0.07) CORRESPON '5a	DING TO				
		2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012
						Subm	Witho	ut LL gn Water Level	C 222				
L/C	Descriptions of Load		(MAX H	- MAX V)		Subm		- MIN V)	Case		(MIN H -	MAX V)	
No.	Case	Point Rak	1	Distributed F	Raking Force	Point Rak	king Force	Distributed R	aking Force	Point Rak	(Distributed R	aking Force
		Surcharge/	Surcharge/	Surcharge/	Surcharge/	Surcharge/	Surcharge/	Surcharge/	Surcharge/	Surcharge/	Surcharge/	Surcharge/	Surcharge/
		Raking	Raking	Raking	Raking	Raking	Raking	Raking	Raking	Raking	Raking	Raking	Raking
		Towards Right	Towards Left	Towards Right	Towards Left	Towards Right	Towards Left	Towards Right	Towards Left	Towards Right	Towards Left	Towards Right	Towards Left
1	Self Weight	1.5	1.5	1.5	1.5	1.0	1.0	1.0	1.0	1.5	1.5	1.5	1.5
2	SIDL	1.5	1.5	1.5	1.5	1.0	1.0	1.0	1.0	1.5	1.5	1.5	1.5
3	Soil Back Fill	1.5	1.5	1.5	1.5	1.0	1.0	1.0	1.0	1.5	1.5	1.5	1.5
4	Live Load on concourse & platform	0	0	0	0	0	0	0	0	0	0	0	0
5	Train Live Load	0	0	0	0	0	0	0	0	0	0	0	0
6	Lateral Earth Pressure (WL @ Design Water Level*) K0	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	0	0	0	0
7	Lateral Earth Pressure (WL @ Design Water Level*) Ka	0	0	0	0	0	0	0	0	1.0	1.0	1.0	1.0
8	Lateral Earth Pressure Sat_K0 (#)	0	0	0	0	0	0	0	0	0	0	0	0
9	Lateral Earth Pressure Dry_Ka (#)	0	0	0	0	0	0	0	0	0	0	0	0
10	Vertical Surcharge Load	1.5	1.5	1.5	1.5	1.0	1.0	1.0	1.0	1.5	1.5	1.5	1.5
11	Lateral Surcharge load (Towards Right)	1.5	0	1.5	0	1.5	0.0	1.5	0.0	1.0	0	1.0	0
12	Lateral Surcharge load (Towards Left)	0	1.5	0	1.5	0	1.5	0	1.5	0	1.0	0	1.0
13	Lateral Surcharge load (Both Sides)	0	0	0	0	0	0	0	0	0	0	0	0
14	Water Pressure at Design Water Level* (Lateral)	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.0	1.0	1.0	1.0
15	Water Pressure at Design Water Level* (Vertical) (Uplift)	1.5	1.5	1.5	1.5	1.0	1.0	1.0	1.0	1.5	1.5	1.5	1.5
16	0.075 g Racking Point Force (Towards Right)	1.5	0	0	0	1.5	0	0	0	1.0	0	0	0
17	0.075 g Racking Point Force (Towards Left)	0	1.5	0	0	0	1.5	0	0	0	1.0	0	0
18	0.075 g Racking Distribution Force (Towards Right)	0	0	1.5	0	0	0	1.5	0	0	0	1.0	0
19	0.075 g Racking Distribution Force (Towards Left)	0	0	0	1.5	0	0	0	1.5	0	0	0	1.0
20	0.15 g Racking Point Force (Towards Right)	0	0	0	0	0	0	0	0	0	0	0	0
21	0.15 g Racking Point Force (Towards Left)	0	0	0	0	0	0	0	0	0	0	0	0
22	0.15 g Racking Distribution Force (Towards Right)	RailCor	0	0	0	0	0	0	0	0	0	0	0
23	0.15 g Racking Distribution Force (Towards Left)	0 - 75	0	0	0	0	0	0	0	0	0	0	0
	10 PUL VI	Director (Project)											

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						ULS SEIS		i) CORRESPO 75a	NDING TO				
		2025	2026	2027	2028	2029	2030	2031	2032	2033	2034	2035	2036
			•	•	•	•	Witho		•	•	•	•	
L/C							Saturated						
No.	Descriptions of Load Case		· · ·	- MAX V)			(MAX H				(- MAX V)	
		Point Rak		Distributed F		Point Rak		Distributed R		Point Rak		Distributed F	
		Surcharge/	Surcharge/	Surcharge/	Surcharge/	Surcharge/	Surcharge/						
		Raking Towards	Raking Towards	Raking Towards	Raking Towards	Raking Towards	Raking Towards						
		Right	Left	Right	Left	Right	Left	Right	Left	Right	Left	Right	Left
1	Self Weight	1.5	1.5	1.5	1.5	1.0	1.0	1.0	1.0	1.5	1.5	1.5	1.5
2	SIDL	1.5	1.5	1.5	1.5	1.0	1.0	1.0	1.0	1.5	1.5	1.5	1.5
3	Soil Back Fill	1.5	1.5	1.5	1.5	1.0	1.0	1.0	1.0	1.5	1.5	1.5	1.5
4	Live Load on concourse & platform	0	0	0	0	0	0	0	0	0	0	0	0
5	Train Live Load	0	0	0	0	0	0	0	0	0	0	0	0
6	Lateral Earth Pressure (WL @ Design Water Level*) K0	0	0	0	0	0	0	0	0	0	0	0	0
7	Lateral Earth Pressure (WL @ Design Water Level*) Ka	0	0	0	0	0	0	0	0	0	0	0	0
8	Lateral Earth Pressure Sat_K0 (#)	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	0	0	0	0
9	Lateral Earth Pressure Dry_ Ka (#)	0	0	0	0	0	0	0	0	1.0	1.0	1.0	1.0
10	Vertical Surcharge Load	1.5	1.5	1.5	1.5	1.0	1.0	1.0	1.0	1.5 1.0	1.5	1.5 1.0	1.5
11	Lateral Surcharge load (Towards Right) Lateral Surcharge load (Towards Left)	1.5	0 1.5	1.5	0	1.5	0.0	1.5	0.0		0		0
12 13	Lateral Surcharge load (Towards Left)	0	0	0	1.5 0	0	1.5 0	0	1.5 0	0	0	0	1.0 0
13	Water Pressure at Design Water Level*	0	0	0	0	0	0	0	0	0	0	0	0
14	(Lateral)			Ŭ	Ŭ							Ŭ	_
15	Water Pressure at Design Water Level* (Vertical) (Uplift)	0	0	0	0	0	0	0	0	0	0	0	0
16	0.075 g Racking Point Force (Towards Right)	1.5	0	0	0	1.5	0	0	0	1.0	0	0	0
17	0.075 g Racking Point Force (Towards Left)	0	1.5	0	0	0	1.5	0	0	0	1.0	0	0
18	0.075 g Racking Distribution Force (Towards Right)	0	0	1.5	0	0	0	1.5	0	0	0	1.0	0
19	0.075 g Racking Distribution Force (Towards Left)	0	0	0	1.5	0	0	0	1.5	0	0	0	1.0
20	0.15 g Racking Point Force (Towards Right)	0	0	0	0	0	0	0	0	0	0	0	0
21	0.15 g Racking Point Force (Towards Left)	0	0	0	0	0	0	0	0	0	0	0	0
22	0.15 g Racking Distribution Force (Towards Right)	0	0	0	0	0	0	0	0	0	0	0	0
23	0.15 g Racking Distribution Force (Towards Left)	0	0	0	0	0	0	0	0	0	0	0	0



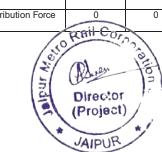
						ULS SEISMIC	(RACKING) C	ORRESPOND	ING TO 0.15g				
		2101	2102	2103	2104	2105	2106	2107	2108	2109	2110	2111	2112
				•			Witho	but LL				•	
						Subme	erged Soil -Des	ign Water Leve	el Case				
L/C	Descriptions of Load Case		(MAX H	- MAX V)			(MAX H	- MIN V)			(MIN H	- MAX V)	
No.	Descriptions of Load Case	Point Rak	ing Force	Distributed F	Raking Force	Point Rak	ing Force	Distributed F	aking Force	Point Rak	king Force	Distributed R	aking Force
		Surcharge/	Surcharge/	Surcharge/	Surcharge/	Surcharge/	Surcharge/	Surcharge/	Surcharge/	Surcharge/	Surcharge/	Surcharge/	Surcharge/
		Raking	Raking	Raking	Raking	Raking	Raking	Raking	Raking	Raking	Raking	Raking	Raking
		Towards	Towards	Towards	Towards	Towards	Towards	Towards	Towards	Towards	Towards	Towards	Towards
		Right	Left	Right	Left	Right	Left	Right	Left	Right	Left	Right	Left
1	Self Weight	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
2	SIDL	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
3	Soil Back Fill	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
4	Live Load on concourse & platform	0	0	0	0	0	0	0	0	0	0	0	0
5	Train Live Load	0	0	0	0	0	0	0	0	0	0	0	0
6	Lateral Earth Pressure (WL @ Design Water Level*) K0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	0	0	0	0
7	Lateral Earth Pressure (WL @ Design Water Level*) Ka	0	0	0	0	0	0	0	0	1.0	1.0	1.0	1.0
8	Lateral Earth Pressure Sat_K0 (#)	0	0	0	0	0	0	0	0	0	0	0	0
9	Lateral Earth Pressure Dry_Ka (#)	0	0	0	0	0	0	0	0	0	0	0	0
10	Vertical Surcharge Load	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
11	Lateral Surcharge load (Towards Right)	1.0	0	1.0	0	1.0	0.0	1.0	0.0	1.0	0	1.0	0
12	Lateral Surcharge load (Towards Left)	0	1.0	0	1.0	0	1.0	0	1.0	0	1.0	0	1.0
13	Lateral Surcharge load (Both Sides)	0	0	0	0	0	0	0	0	0	0	0	0
14	Water Pressure at Design Water Level* (Lateral)	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
15	Water Pressure at Design Water Level* (Vertical) (Uplift)	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
16	0.075 g Racking Point Force (Towards Right)	0	0	0	0	0	0	0	0	0	0	0	0
17	0.075 g Racking Point Force (Towards Left)	0	0	0	0	0	0	0	0	0	0	0	0
18	0.075 g Racking Distribution Force (Towards Right)	0	0	0	0	0	0	0	0	0	0	0	0
19	0.075 g Racking Distribution Force (Towards Left)	0	0	0	0	0	0	0	0	0	0	0	0
20	0.15 g Racking Point Force (Towards Right)	1.0	0	0	0	1.0	0	0	0	1.0	0	0	0
21	0.15 g Racking Point Force (Towards Left)	0	1.0	0	0	0	1.0	0	0	0	1.0	0	0
22	0.15 g Racking Distribution Force (Towards Right)	0	0	1.0	0	0	0	1.0	0	0	0	1.0	0
23	0.15 g Racking Distribution Force (Towards Left)	0	0	0	1.0	0	0	0	1.0	0	0	0	1.0



					UL	S SEISMIC (R	ACKING) COF	RESPONDIN	G TO 0.15g				
		2125	2126	2127	2128	2129	2130	2131	2132	2133	2134	2135	213 6
							Without	LL					
							Saturated / D						
			(MAX H	- MAX V)			(MAX H	- MIN V)			(MIN H - M		
L/C		Point Rak	ing Force	Distributed F	Raking Force	Point Rak	ing Force	Distributed F	Raking Force	Point Rak	king Force	Distributed I Force	Raking
No.	Descriptions of Load Case	Surcharge/ Raking Towards Right	Surcharge/ Raking Towards Left	Surcharge/ Raking Towards Right	Sur cha rge/ Rak ing To war ds Left								
1	SelfWeight	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
2	SIDL	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
3	Soil Back Fill Live Load on concourse & platform	1.0 0	1.0 0										
5	Train Live Load	0	0	0	0	0	0	0	0	0	0	0	0
6	Lateral Earth Pressure (WL @ Design Water Level*) K0	0	0	0	0	0	0	0	0	0	0	0	0
7	Lateral Earth Pressure (WL @ Design Water Level*) Ka	0	0	0	0	0	0	0	0	0	0	0	0
8	Lateral Earth Pressure Sat_K0 (#)	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	0	0	0	0
9	Lateral Earth Pressure Dry_Ka (#)	0	0	0	0	0	0	0	0	1.0	1.0	1.0	1.0
10	Vertical Surcharge Load	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
11	Lateral Surcharge load (Towards Right)	1.0	0	1.0	0	1.0	0.0	1.0	0.0	1.0	0	1.0	0
12	Lateral Surcharge load (Towards Left)	0	1.0	0	1.0	0	1.0	0	1.0	0	1.0	0	1.0
13	Lateral Surcharge load (Both Sides)	0	0	0	0	0	0	0	0	0	0	0	0
14	Water Pressure at Design Water Level* (Lateral)	0	0	0	0	0	0	0	0	0	0	0	0
15	Water Pressure at Design Water Level* (Vertical) (Uplift)	0	0	0	0	0	0	0	0	0	0	0	0
16	0.075 g Racking Point Force (Towards Right)	0	0	0	0	0	0	0	0	0	0	0	0
17	0.075 g Racking Point Force (Towards Left)	0	0	0	0	0	0	0	0	0	0	0	0
18	0.075 g Racking Distribution Force (Towards Right)	0	0	0	0	0	0	0	0	0	0	0	0
19	0.075 g Racking Distribution Force (Towards Left)	0	0	0	0	0	0	0	0	0	0	0	0
20	0.15 g Racking Point Force (Towards Right)	1.0	0	0	0	1.0	0	0	0	1.0	0	0	0
21	0.15 g Racking Point Force (Towards Left)	0	1.0	0	0	0	1.0	0	0	0	1.0	0	0
22	0.15 g Racking Distribution Force (Towards Right)	ail Corp	0	1.0	0	0	0	1.0	0	0	0	1.0	0
23	0.15 g Racking Distribution Forces (Towards Left)		··	0	1.0	0	0	0	1.0	0	0	0	1.0
		lirector	on .										

Director (Project)

						ULS SEISM		G) CORRESPC	ONDING TO				
		2201	2202	2203	2204	2205	2206	2207	2208	2209	2210	2211	2212
						Subm		h LL sian Water Leve					
L/C	Descriptions of Load			- MAX V)		Subme		- MIN V)	el Case			- MAX V)	
No.	Case	Point Pol	king Force	,	Raking Force	Point Pak	ting Force	Distributed F	Paking Force	Point Pak	king Force	Distributed F	Paking Force
			0				0						0
		Surcharge/ Raking	Surcharge/ Raking	Surcharge/ Raking	Surcharge/ Raking	Surcharge/ Raking	Surcharge/ Raking						
		Towards	Towards	Towards	Towards	Towards	Towards						
		Right	Left	Right	Left	Right	Left	Right	Left	Right	Left	Right	Left
1	Self Weight	1.2	1.2	1.2	1.2	1.0	1.0	1.0	1.0	1.2	1.2	1.2	1.2
2	SIDL	1.2	1.2	1.2	1.2	1.0	1.0	1.0	1.0	1.2	1.2	1.2	1.2
3	Soil Back Fill	1.2	1.2	1.2	1.2	1.0	1.0	1.0	1.0	1.2	1.2	1.2	1.2
	Live Load on concourse &	0.6	0.6	0.6	0.6	0.5	0.5	0.5	0.5	0.6	0.6	0.6	0.6
4	platform												
5	Train Live Load	0.6	0.6	0.6	0.6	0.5	0.5	0.5	0.5	0.6	0.6	0.6	0.6
6	Lateral Earth Pressure (WL @ Design Water Level*) K0	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2	0	0	0	0
7	Lateral Earth Pressure (WL @ Design Water Level*) Ka	0	0	0	0	0	0	0	0	1.0	1.0	1.0	1.0
8	Lateral Earth Pressure Sat_K0 (#)	0	0	0	0	0	0	0	0	0	0	0	0
9	Lateral Earth Pressure Dry_Ka (#)	0	0	0	0	0	0	0	0	0	0	0	0
10	Vertical Surcharge Load	1.2	1.2	1.2	1.2	1.0	1.0	1.0	1.0	1.2	1.2	1.2	1.2
11	Lateral Surcharge load (Towards Right)	1.2	0	1.2	0	1.2	0.0	1.2	0.0	1.0	0	1.0	0
12	Lateral Surcharge load (Towards Left)	0	1.2	0	1.2	0	1.2	0	1.2	0	1.0	0	1.0
13	Lateral Surcharge load (Both Sides)	0	0	0	0	0	0	0	0	0	0	0	0
14	Water Pressure at Design Water Level* (Lateral)	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.0	1.0	1.0	1.0
15	Water Pressure at Design Water Level* (Vertical) (Uplift)	1.2	1.2	1.2	1.2	1.0	1.0	1.0	1.0	1.2	1.2	1.2	1.2
16	0.075 g Racking Point Force (Towards Right)	1.2	0	0	0	1.2	0	0	0	1.0	0	0	0
17	0.075 g Racking Point Force (Towards Left)	0	1.2	0	0	0	1.2	0	0	0	1.0	0	0
18	0.075 g Racking Distribution Force (Towards Right)	0	0	1.2	0	0	0	1.2	0	0	0	1.0	0
19	0.075 g Racking Distribution Force (Towards Left)	0	0	0	1.2	0	0	0	1.2	0	0	0	1.0
20	0.15 g Racking Point Force (Towards Right)	0	0	0	0	0	0	0	0	0	0	0	0
21	0.15 g Racking Point Force (Towards Left)	0	0	0	0	0	0	0	0	0	0	0	0
22	0.15 g Racking Distribution Force (Towards Right)	0	0	0	0	0	0	0	0	0	0	0	0
23	0.15 g Racking Distribution Force (Towards Left)	0 Bail Con	0	0	0	0	0	0	0	0	0	0	0



						ULS S	EISMIC (RAC	KING) CORRE 0.075g	SPONDING T	0			
		2225	2226	2227	2228	2229	2230	2231	2232	2233	2234	2235	2236
								With LL					
								ated / Dry Case	9				
L/C	Descriptions of		(MAX H	- MAX V)			(MAX H	I - MIN V)				N H - MAX V)	
No.	Load Case	-	ing Force	Distributed F			king Force	Distributed F			king Force		ed Raking Force
		Surcharge/ Raking Towards Right	Surcharge/ Raking Towards Left	Surcharge/ Raking Towards Right	Surcharge/ Raking Towards Left								
1	Self Weight	1.2	1.2	1.2	1.2	1.0	1.0	1.0	1.0	1.2	1.2	1.2	1.2
2	SIDL	1.2	1.2	1.2	1.2	1.0	1.0	1.0	1.0	1.2	1.2	1.2	1.2
3	Soil Back Fill	1.2 0.6	1.2 0.6	1.2 0.6	1.2 0.6	1.0 0.5	1.0 0.5	1.0 0.5	1.0 0.5	1.2 0.6	1.2 0.6	1.2 0.6	1.2 0.6
4	Live Load on concourse & platform	0.0	0.0	0.0	0.0	0.5	0.5	0.5	0.5	0.0	0.0	0.0	0.0
5	Train Live Load	0.6	0.6	0.6	0.6	0.5	0.5	0.5	0.5	0.6	0.6	0.6	0.6
6	Lateral Earth Pressure (WL @ Design Water Level*) K0	0	0	0	0	0	0	0	0	0	0	0	0
7	Lateral Earth Pressure (WL @ Design Water Level*) Ka	0	0	0	0	0	0	0	0	0	0	0	0
8	Lateral Earth Pressure Sat_ K0 (#)	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2	0	0	0	0
9	Lateral Earth Pressure Dry_ Ka (#)	0	0	0	0	0	0	0	0	1.0	1.0	1.0	1.0
10	Vertical Surcharge Load	1.2	1.2	1.2	1.2	1.0	1.0	1.0	1.0	1.2	1.2	1.2	1.2
11	Lateral Surcharge load (Towards Right)	1.2	0	1.2	0	1.2	0.0	1.2	0.0	1.0	0	1.0	0
12	Lateral Surcharge load (Towards Left)	0	1.2	0	1.2	0	1.2	0	1.2	0	1.0	0	1.0
13	Lateral Surcharge load (Both Sides)	0	0	0	0	0	0	0	0	0	0	0	0
14	Water Pressure at Design Water Level* (Lateral)	0	0	0	0	0	0	0	0	0	0	0	0
15	Water Pressure at Design Water Level* (Vertical) (Uplift)	0	0	0	0	0	0	0	0	0	0	0	0
16	0.075 g Racking Point Force (Towards Right)	1.2	0	0	0	1.2	0	0	0	1.0	0	0	0
17	0.075 g Racking Point Force (Towards Left)	0	1.2	0	0	0	1.2	0	0	0	1.0	0	0
18	0.075 g Racking Distribution Force (Towards Right)	0	0	1.2	0	0	0	1.2	0	0	0	1.0	0
19	0.075 g Racking Distribution Force (Towards Left)	ORA	1 Corp	0	1.2	0	0	0	1.2	0	0	0	1.0
20	0.15 g Racking Point Force (Towards Right)	1.07	0 0	0	0	0	0	0	0	0	0	0	0
21	0.15 g Racking Point Force (Towards Left)			0	0	0	0	0	0	0	0	0	0
22	0.15 g Racking Distribution Force (Towards Right)		oject)	0	0	0	0	0	0	0	0	0	0
87		* JA	IPUR *										

23	0.15 g Racking	0	0	0	0	0	0	0	0	0	0	0	0
	Distribution Force (Towards Left)												

						ULS SEISMIC	(RACKING) C	ORRESPOND	DING TO 0.15g				
		2301	2302	2303	2304	2305	2306	2307	2308	2309	2310	2311	2312
								n LL	1.0				
			(- MAX V)		Subme	erged Soil -Des (MAX H		el Case	-	(MIN H ·		
L/C No.	Descriptions of Load Case	Deint Del	· ·	,	Raking Force	Deint Del	(MAX H	Distributed F	aking Faras	Deint Del	(MIN H	,	Raking Force
	Case	Point Rak Surcharge/	Surcharge/	Surcharge/	Surcharge/	Surcharge/	Surcharge/	Surcharge/	Surcharge/	Surcharge/	Surcharge/	Surcharge/	Surcharge/
		Raking	Raking	Raking	Raking	Raking	Raking	Raking	Raking	Raking	Raking	Raking	Raking
		Towards	Towards	Towards	Towards	Towards	Towards	Towards	Towards	Towards	Towards	Towards	Towards
		Right	Left	Right	Left	Right	Left	Right	Left	Right	Left	Right	Left
1	Self Weight	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
2	SIDL	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
3	Soil Back Fill	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
4	Live Load on concourse & platform	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
5	Train Live Load	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
6	Lateral Earth Pressure (WL @ Design Water Level*) K0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	0	0	0	0
7	Lateral Earth Pressure (WL @ Design Water Level*) Ka	0	0	0	0	0	0	0	0	1.0	1.0	1.0	1.0
8	Lateral Earth Pressure Sat_ K0 (#)	0	0	0	0	0	0	0	0	0	0	0	0
9	Lateral Earth Pressure Dry_ Ka (#)	0	0	0	0	0	0	0	0	0	0	0	0
10	Vertical Surcharge Load	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
11	Lateral Surcharge load (Towards Right)	1.0	0	1.0	0	1.0	0.0	1.0	0.0	1.0	0	1.0	0
12	Lateral Surcharge load (Towards Left)	0	1.0	0	1.0	0	1.0	0	1.0	0	1.0	0	1.0
13	Lateral Surcharge load (Both Sides)	0	0	0	0	0	0	0	0	0	0	0	0
14	Water Pressure at Design Water Level* (Lateral)	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
15	Water Pressure at Design Water Level* (Vertical) (Uplift)	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
16	0.075 g Racking Point Force (Towards Right)	0	0	0	0	0	0	0	0	0	0	0	0
17	0.075 g Racking Point Force (Towards Left)	0	0	0	0	0	0	0	0	0	0	0	0
18	0.075 g Racking Distribution Force (Towards Right)	0	0	0	0	0	0	0	0	0	0	0	0
19	0.075 g Racking Distribution Force (Towards Left)	0	0	0	0	0	0	0	0	0	0	0	0
20	0.15 g Racking Point Force (Towards Right)	1.0	0	0	0	1.0	0	0	0	1.0	0	0	0
21	0.15 g Racking Point Force (Towards Left)	RailCor	1.0	0	0	0	1.0	0	0	0	1.0	0	0
22	0.15 g Racking Distribution Force (Towards Right) 0.15 g Racking Distribution	0	DE.	1.0	0	0	0	1.0	0	0	0	1.0	0
23	Force (Towards Left)	(Pd sen	190	0	1.0	0	0	0	1.0	0	0	0	1.0
		Director (Project)	+r										
L/C No	Descriptions of	(110)001	*/			ULS SEISMI	C (RACKING)	CORRESPON	DING TO 0.15၀	3			
	× ×	VAIPUR											
88R1			-										

	Load Case	2325	2326	2327	2328	2329	2330	2331	2332	2333	2334	2335	2336
								ih LL					
				- MAX V)		F		/ Dry Case I - MIN V)		r		- MAX V)	
		Point Rak		,	Raking Force	Point Rak	`	/	Raking Force	Point Pol	king Force		Raking Force
		Surcharge/	Surcharge/	Surcharge/	Surcharge/	Surcharge/	Surcharge/	Surcharge/	Surcharge/	Surcharge/	Surcharge/	Surcharge/	Surcharge/
		Raking	Raking	Raking	Raking	Raking	Raking	Raking	Raking	Raking	Raking	Raking	Raking
		Towards	Towards	Towards	Towards	Towards	Towards	Towards	Towards	Towards	Towards	Towards	Towards
		Right	Left	Right	Left	Right	Left	Right	Left	Right	Left	Right	Left
1	Self Weight	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
2	SIDL	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
3	Soil Back Fill	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
4	Live Load on concourse & platform	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
5	Train Live Load	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
6	Lateral Earth Pressure (WL @ Design Water Level*) K0	0	0	0	0	0	0	0	0	0	0	0	0
7	Lateral Earth Pressure (WL @ Design Water Level*) Ka	0	0	0	0	0	0	0	0	0	0	0	0
8	Lateral Earth Pressure Sat_ K0 (#)	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	0	0	0	0
9	Lateral Earth Pressure Dry_ Ka (#)	0	0	0	0	0	0	0	0	1.0	1.0	1.0	1.0
10	Vertical Surcharge Load	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
11	Lateral Surcharge load (Towards Right)	1.0	0	1.0	0	1.0	0.0	1.0	0.0	1.0	0	1.0	0
12	Lateral Surcharge load (Towards Left)	0	1.0	0	1.0	0	1.0	0	1.0	0	1.0	0	1.0
13	Lateral Surcharge load (Both Sides)	0	0	0	0	0	0	0	0	0	0	0	0
14	Water Pressure at Design Water Level* (Lateral)	0	0	0	0	0	0	0	0	0	0	0	0
15	Water Pressure at Design Water Level* (Vertical) (Uplift)	0	0	0	0	0	0	0	0	0	0	0	0
16	0.075 g Racking Point Force (Towards Right)	0	0	0	0	0	0	0	0	0	0	0	0
17	0.075 g Racking Point Force (Towards Left)	0	0	0	0	0	0	0	0	0	0	0	0
18	0.075 g Racking Distribution Force (Towards Right)	0	0	0	0	0	0	0	0	0	0	0	0
19	0.075 g Racking Distribution Force (Towards Left)	0	0	0	0	0	0	0	0	0	0	0	0
20	0.15 g Racking Point Force (Towards Right)	1.0	0	0	0	1.0	0	0	0	1.0	0	0	0
21	0.15 g Racking Point Force (Towards Left)	0	1.0	0	0	0	1.0	0	0	0	1.0	0	0
22	0.15 g Racking Distribution Force (Towards Right)	0	0	1.0	0	0	0	1.0	0	0	0	1.0	0
23	0.15 g Racking Distribution Force (Towards Left)	0	0	0	1.0	0	0	0	1.0	0	0	0	1.0

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13	~	Man JE						SLS				
1 =	1	(1000)	3001	3002	3003	3004	3005	3101	3102	3103	3104	3105
12		-Director		Submerged S	Soil -Design W	ater Level C	ase		5	Saturated / Dry C	Case	
1	Ý	(Project)										

L/C

No.	Descriptions of Load Case	(MAX H - MAX	(MAX H - MAX V) without LL	(MAX H - MIN V)	(MIN H - MAX V)	(MIN H - MAX V) without LL	(MAX H - MAX V)	(MAX H - MAX V) without LL	(MAX H - MIN V)	(MIN H - MAX V)	(MIN H - MAX V) without LL
		V)									
1	Self Weight	1	1	1	1	1	1	1	1	1	1
2	SIDL	1	1	1	1	1	1	1	1	1	1
3	Soil Back Fill	1	1	1	1	1	1	1	1	1	1
4	Live Load on concourse & platform	1	0	0	1	0	1	0	0	1	0
5	Train Live Load	1	0	0	1	0	1	0	0	1	0
6	Lateral Earth Pressure (WL @ Design Water Level*) K0	1	1	1	0	0	0	0	0	0	0
7	Lateral Earth Pressure (WL @ Design Water Level*) Ka	0	0	0	1	1	0	0	0	0	0
8	Lateral Earth Pressure Sat_K0 (#)	0	0	0	0	0	1	1	1	0	0
9	Lateral Earth Pressure Dry_Ka (#)	0	0	0	0	0	0	0	0	1	1
10	Vertical Surcharge Load	1	1	0	1	1	1	1	0	1	1
11	Lateral Surcharge load (Towards Right)	0	0	0	0	0	0	0	0	0	0
12	Lateral Surcharge load (Towards Left)	0	0	0	0	0	0	0	0	0	0
13	Lateral Surcharge load (Both Sides)	1	1	1	0	0	1	1	1	0	0
14	Water Pressure at Design Water Level* (Lateral)	1	1	1	1	1	0	0	0	0	0
15	Water Pressure at Design Water Level* (Vertical) (Uplift)	1	1	1	1	1	0	0	0	0	0
16	0.075 g Racking Point Force (Towards Right)	0	0	0	0	0	0	0	0	0	0
17	0.075 g Racking Point Force (Towards Left)	0	0	0	0	0	0	0	0	0	0
18	0.075 g Racking Distribution Force (Towards Right)	0	0	0	0	0	0	0	0	0	0
19	0.075 g Racking Distribution Force (Towards Left)	0	0	0	0	0	0	0	0	0	0
20	0.15 g Racking Point Force (Towards Right)	0	0	0	0	0	0	0	0	0	0
21	0.15 g Racking Point Force (Towards Left)	0	0	0	0	0	0	0	0	0	0
22	0.15 g Racking Distribution Force (Towards Right)	0	0	0	0	0	0	0	0	0	0
23	0.15 g Racking Distribution Force (Towards Left)	0	0	0	0	0	0	0	0	0	0

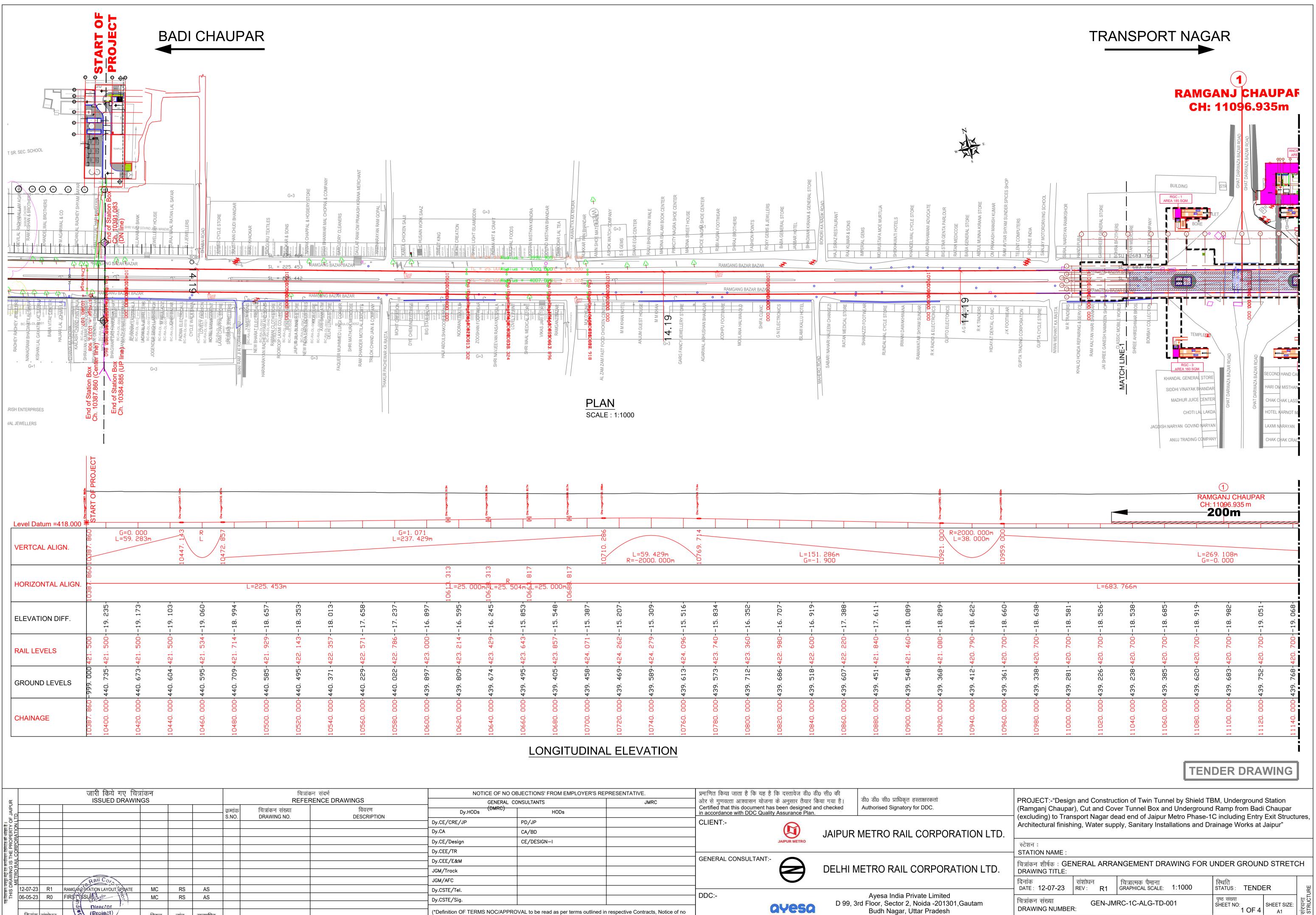


	F DRAWINGS FOR UNDER GROUND STRETCH		
S.NO.	DRAWING TITLE	DRAWING NO.	REVISION
1	LIST OF DRAWINGS FOR UNDER GROUND STRETCH	GEN-JMRC-TD-003	R1
2	GENERAL NOTES	GEN-JMRC-TD-004	RO
ARCHIT	ECTURE DRAWING		
RAMGAN	IJ CHAUPAR STATION		
3	FINISHING SCHEDULE	JMRC-STN-RGC-TED-ARP-11000	RO
4	GROUND LEVEL PLAN	JMRC-STN-RGC-TED-ARP-11001	RO
5	CONCOURSE LEVEL PLAN	JMRC-STN-RGC-TED-ARP-11002	RO
6	PLATFORM LEVEL PLAN	JMRC-STN-RGC-TED-ARP-11003	RO
7	UNDERCROFT LEVEL PLAN	JMRC-STN-RGC-TED-ARP-11004	RO
8	TOP OF BOX LEVEL PLAN	JMRC-STN-RGC-TED-ARP-11005	RO
9	ANCILLARY BLOCK PLANS & SECTION	JMRC-STN-RGC-TED-ARP-11006	RO
10	CROSS SECTION	JMRC-STN-RGC-TED-ARP-13001	RO
11	LONG SECTION	JMRC-STN-RGC-TED-ARP-13002	RO
12	ENTRY STRUCTURE DETAILS	JMRC-STN-RGC-TED-ARP-15001	RO
13	SS RAILING WITH GLASS PANELS (AT PUBLIC STAIRCASE) TYPICAL DETAIL (UNDERGROUND STATION)	JMRC-STN-TYT-TED-ARP-19001	RO
STRUCT			
GENERAL	ARRANGEMENT DRAWING		
14	GENERAL ARRANGEMENT DRAWING FOR UNDER GROUND STRETCH(SHEET 1 OF 4)	GEN-JMRC-1C-ALG-TD-001	R1
15	GENERAL ARRANGEMENT DRAWING FOR UNDER GROUND STRETCH(SHEET 2 OF 4)	GEN-JMRC-1C-ALG-TD-002	R1
16	GENERAL ARRANGEMENT DRAWING FOR UNDER GROUND STRETCH(SHEET 3 OF 4)	GEN-JMRC-1C-ALG-TD-003	R1
17	GENERAL ARRANGEMENT DRAWING FOR UNDER GROUND STRETCH(SHEET 4 OF 4)	GEN-JMRC-1C-ALG-TD-004	R1
UNDER G	ROUND TUNNEL, CUT & COVER, UG RAMP, CROSS PASSAGE DRAWINGS	1	I
18	DETAILS OF TBM SEGMENT LINING (SHEET 1 OF 2)	TUN-JMRC-1C-STR-TD-14001	RO

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			क्रमांक S NO	चित्रांकन संख्या DRAWING NO.	विवरण DESCRIPTION	Dy.HODs	HODs		Certified that this document has been de in accordance with DDC Quality Assurar	esigned and cl ince Plan.	hecked Authorised Signatory for DDC.	(Ramganj Chaupar), Cut and C (excluding) to Transport Nagar			
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ORPO						Dy.CEE/E&M			GENERAL CONSULTANT:-				WINGS FOR UNDER GROUND	STRETCH	
						JGM/Track					DELHI METRO RAIL CORPORATION LTD.	DRAWING TITLE:			
	RailCorp					JGM/AFC						दिनांक संशोधन	चित्रात्मक पैमाना GRAPHICAL SCALE:	स्थिति STATUS :	
, W						Dy.CSTE/Tel.			1			DATE : 12-07-2023 REV : R1	GRAPHICAL SCALE:	STATUS :	TENDER
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06-05-2023	0 FIRE ISSUE	RS AS							aye	260	D 99, 3rd Floor, Sector 2, Noida -201301,Gautam	The Company and the second of the second sec	GEN-JMRC-TD-003	SHEET NO:	SHEET SIZE:
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DATE F	EV. CRESCRIPTION * DRAWN C	HECKED APPROVED					ing accorded for design principal only.)				Tel.: +(91) 120 490 8800, Email: dcdd05@ayesa.com	This drawing must not be either loaned, copied or otherwise repr	oduced in whole or in part or used for any purpose withou	the prior written permission of JMRC	C.

LIST O	F DRAWINGS FOR UNDER GROUND STRETCH		
S.NO.	DRAWING TITLE	DRAWING NO.	REVISION
19	DETAILS OF TBM SEGMENT LINING (SHEET 2 OF 2)	TUN-JMRC-1C-STR-TD-14002	RO
20	OPEN RAMP, CUT & COVER GENERAL ARRANGEMENT (SHEET 1 OF 2)	CCV-JMRC-1C-STR-TD-14003	R1
21	OPEN RAMP, CUT & COVER GENERAL ARRANGEMENT (SHEET 2 OF 2)	CCV-JMRC-1C-STR-TD-14004	RO
22	BORED TUNNEL - WALKWAY (SHEET 1 OF 3)	TUN-JMRC-1C-STR-TD-14005	RO
23	BORED TUNNEL - WALKWAY (SHEET 2 OF 3)	TUN-JMRC-1C-STR-TD-14006	RO
24	BORED TUNNEL - WALKWAY (SHEET 3 OF 3)	TUN-JMRC-1C-STR-TD-14007	RO
25	DETAILS OF TEMPORARY BARRICADING(1m.HEIGHT)	TUN-JMRC-1C-STR-TD-14008	RO
26	DETAILS OF TEMPORARY BARRICADING(2m.HEIGHT)	TUN-JMRC-1C-STR-TD-14009	RO
27	DIMENSION DETAIL OF TWIN BORED TUNNEL	TUN-JMRC-1C-STR-TD-14010	RO
28	INSTRUMENTATION AND MONITORING GENERAL NOTES	INT-JMRC-1C-STR-TD-15001	RO
29	INSTRUMENTATION AND MONITORING DETAILS OF ARRAYS (SHEET 1 OF 3)	INT-JMRC-1C-STR-TD-15002	RO
30	INSTRUMENTATION AND MONITORING DETAILS OF ARRAYS (SHEET 2 OF 3)	INT-JMRC-1C-STR-TD-15003	RO
31	INSTRUMENTATION AND MONITORING DETAILS OF ARRAYS (SHEET 3 OF 3)	INT-JMRC-1C-STR-TD-15004	RO
32	TYPICAL DETAILS OF SHEAR CONNECTORS	GEN-JMRC-1C-STR-TD-16001	RO
33	RUNNING TUNNELS SUMP CROSS PASSAGE GENERAL ARRANGEMENT	TUN-JMRC-1C-STR-TD-17001	RO
34	RUNNING TUNNELS CROSS PASSAGE GENERAL ARRANGEMENT	TUN-JMRC-1C-STR-TD-17002	RO
35	RUNNING TUNNELS CROSS PASSAGE GENERAL ARRANGEMENT (SHOWING SERVICES)	TUN-JMRC-1C-STR-TD-17003	RO
36	TYPICAL DETAILS OF STEEL GRILL	TUN-JMRC-1C-STR-TD-18001	RO
37	TYPICAL DETAILS OF BOUNDARY WALL	TUN-JMRC-1C-STR-TD-19001	RO
38	UNDERCROFT LEVEL - EARTHMAT LAYOUT (SHEET 1 OF 2)	RGC-JMRC-1C-STR-TD-00601	RO
39	UNDERCROFT LEVEL - EARTHMAT LAYOUT (SHEET 2 OF 2)	RGC-JMRC-1C-STR-TD-00602	RO

TENDER DRAWING

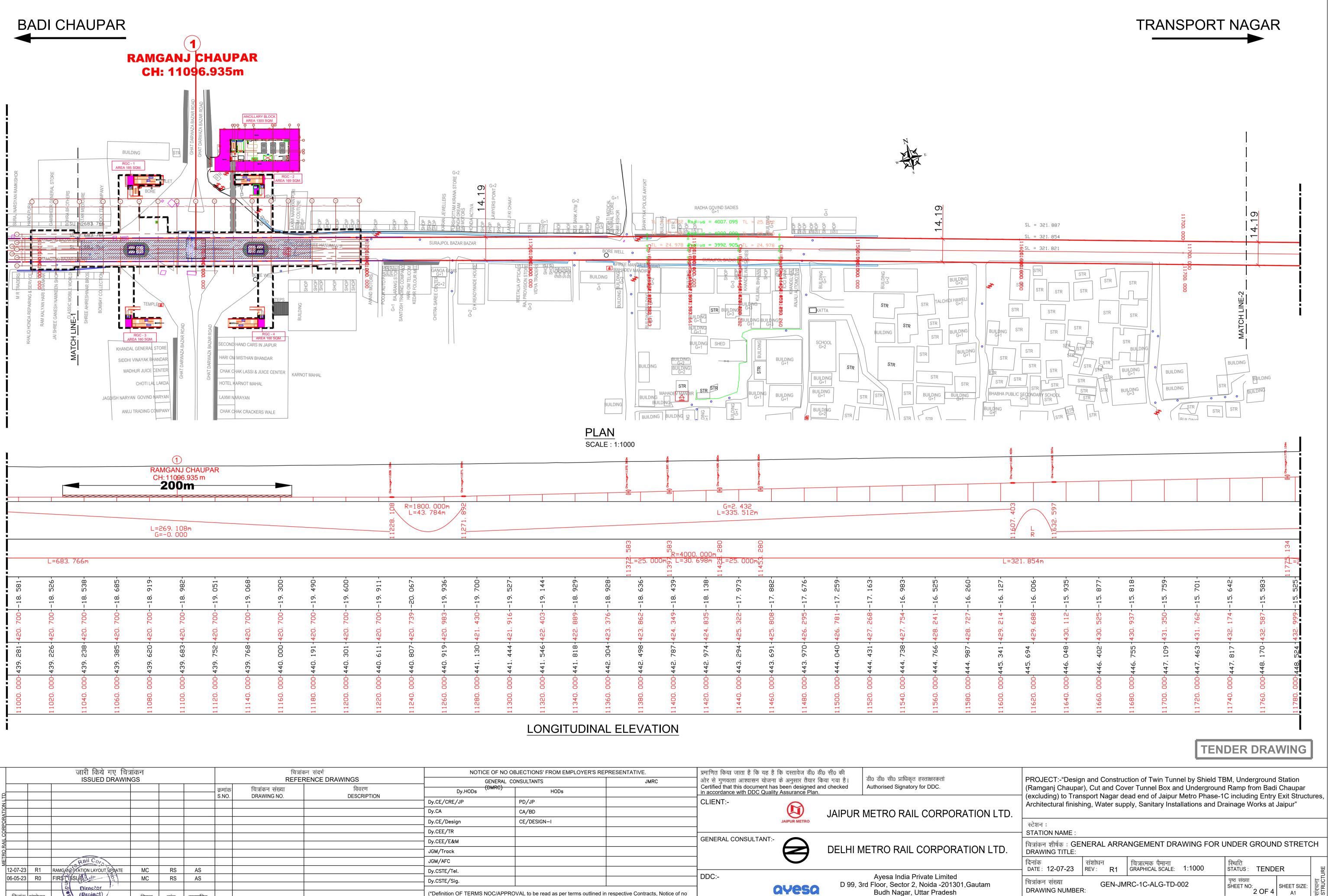


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OC/APPR	OVAL to be read as per terms outlined	in respective Contracts, Notice of no		ayesa	,	Budh Nagar, Uttar Pradesh
s being acc	corded for design principal only.)				Tel.: +(91) 120 490 8800, Email: dcdd05@ayesa.com

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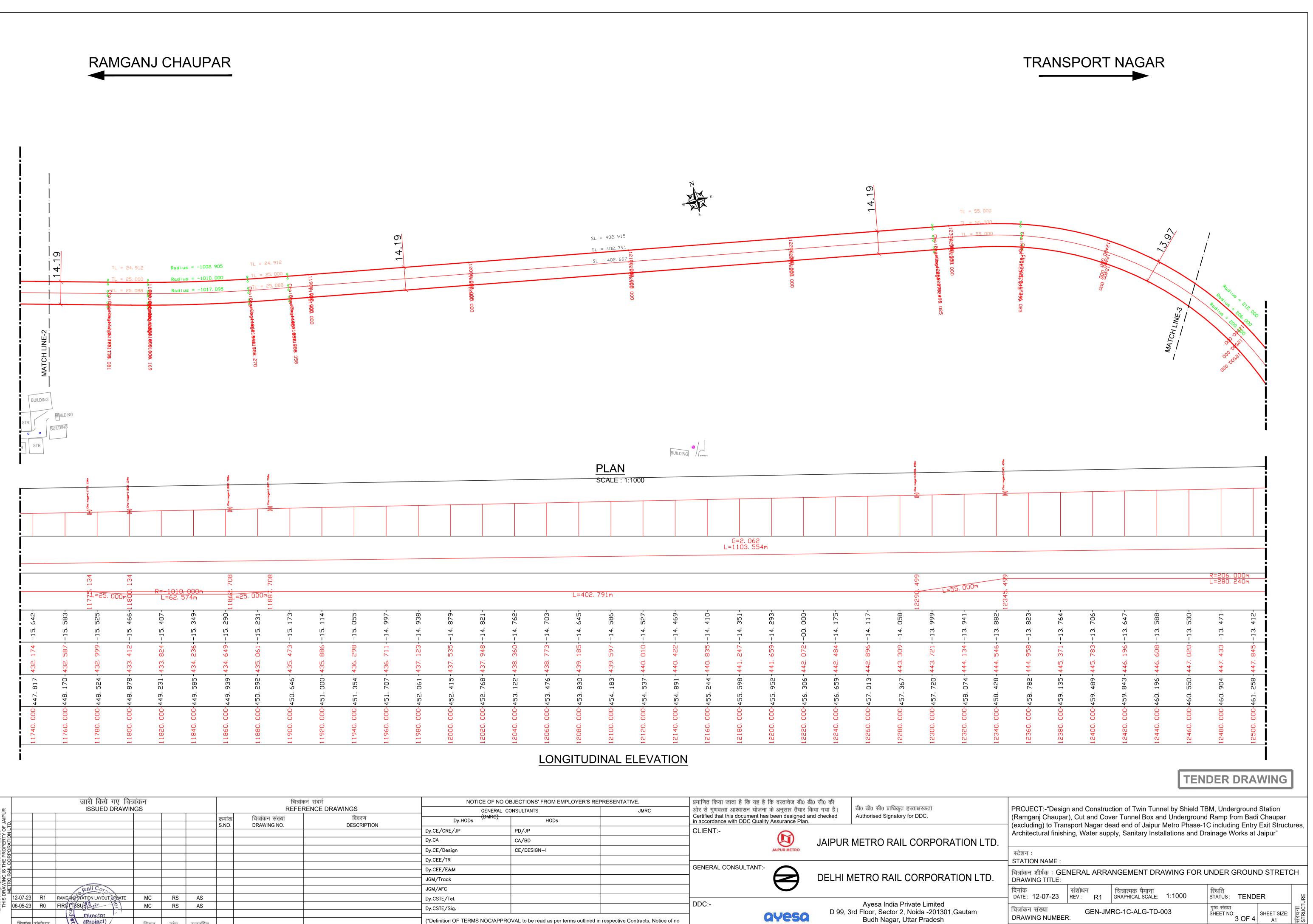
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OF NO O	BJECTIONS' FROM EMPLOYER'S R	EPRESENTATIVE.	प्रमाणित किया जाता है कि यह			
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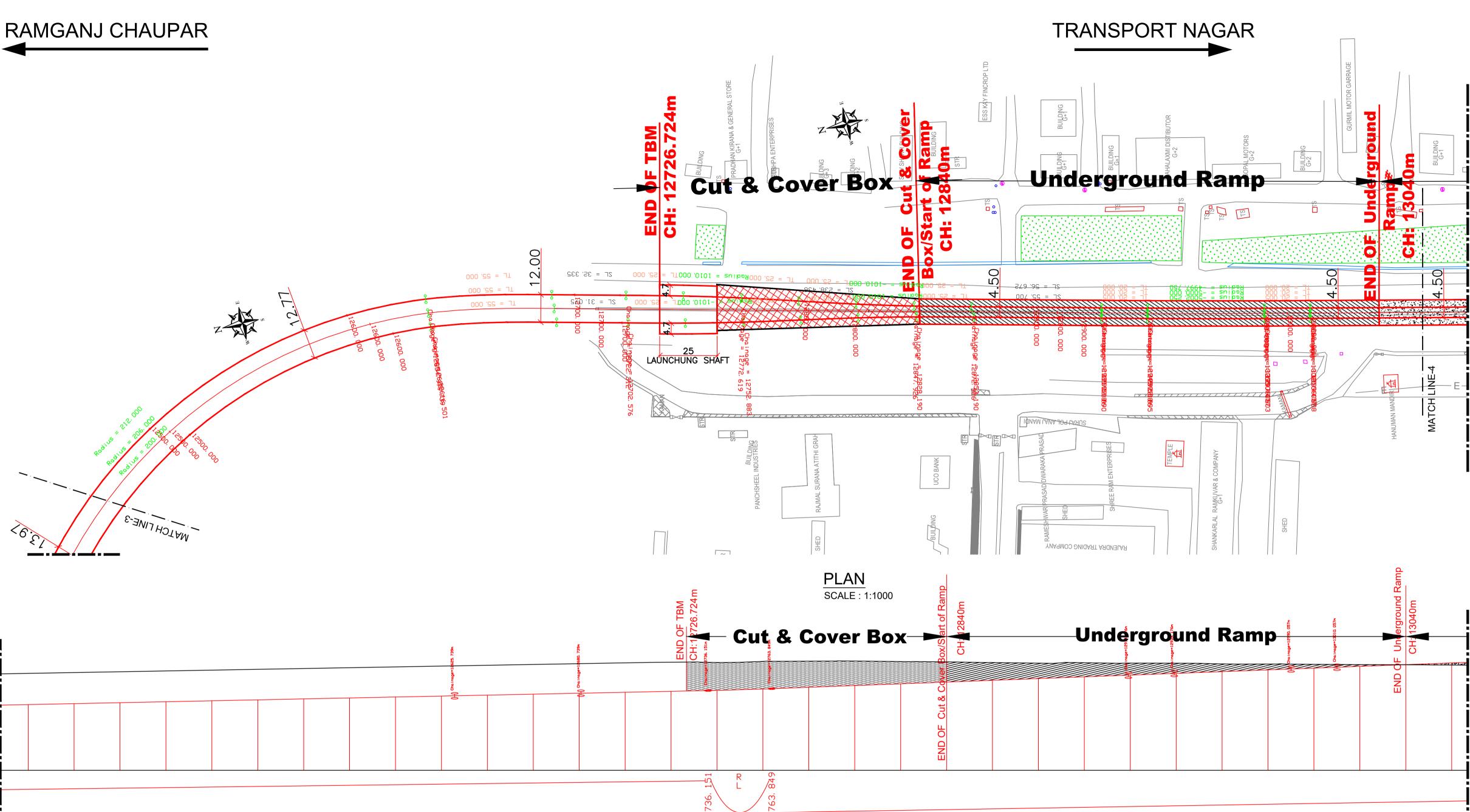


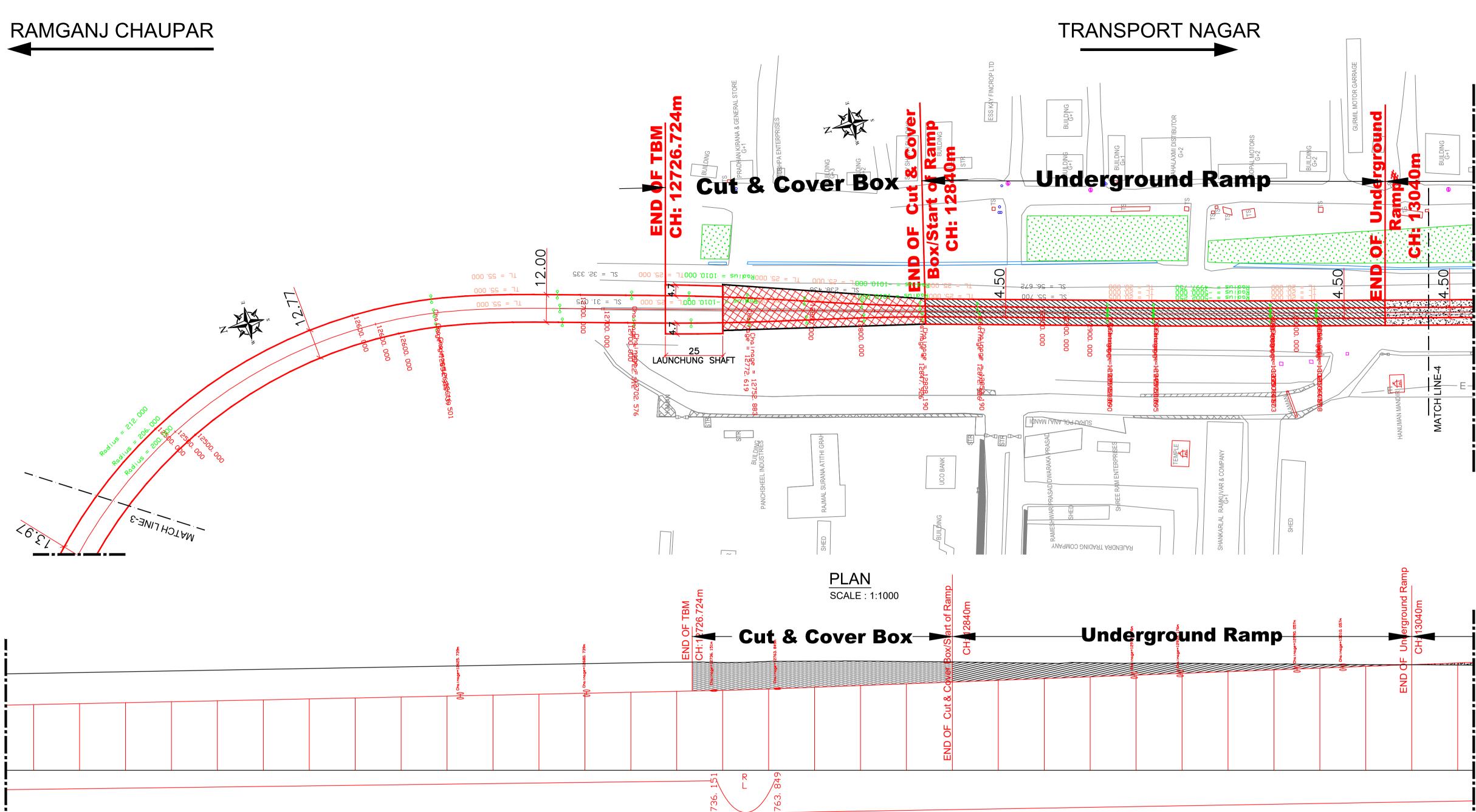
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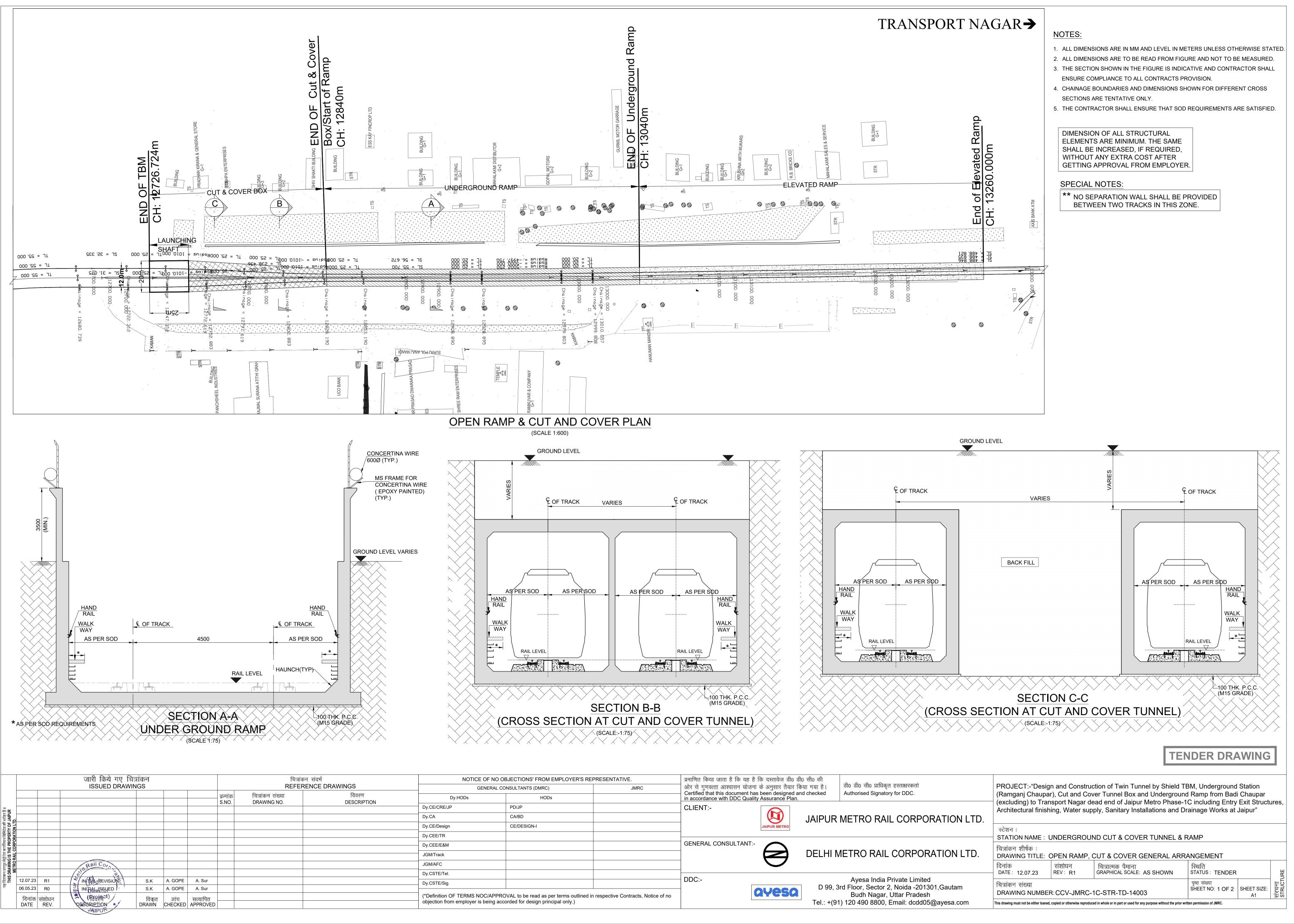
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Geo-technical Investigation work for Extension of underground and elevated section E-W Corridor from Badi Chouper to Transport Nagar (2.85Km) Phase-1C and Mansarovar to Ajmer Road (Chauraha) (1.35 km) Phase-1D of Jaipur Metro Rail Corporation at Jaipur.

CHAPTER 1 GENERAL

1.0 INTRODUCTION

The work for conducting "Geo-technical Investigation work for Extension of underground and elevated section E-W Corridor from Badi Chouper to Transport Nagar (2.85Km) Phase-1C and Mansarovar to Ajmer Road (Chauraha) (1.35 km) Phase-1D" of Jaipur Metro Rail Corporation at Jaipur" was awarded to CEG Test House & Research Centre Pvt. Ltd. (CEGTH) by M/s Jaipur Metro Rail Corporation Ltd. vide work order no. FN:7 (C-430)/JMRC/ Phase-1C&1D/Geo/2023/02 Dated 04.04.2023.

The objective of this detailed geotechnical investigation work is to assess the nature and strength characteristics of the sub strata and to evaluate the soil / Rock core parameters required for design of suitable foundations for various structures.

Field work including drilling of boreholes, conducting various other field tests and collection of soil samples was carried out in the presence of Engineer in charge. Laboratory tests were conducted on selected soil samples to determine the design parameters, conforming to relevant specifications and as per guidelines received from the client.

This report includes the detailed Methodology of Investigation, collection of soil samples, field test results, laboratory test results and analysis of results based on soil / rock core samples collected from the locations of 23 boreholes carried out at underground section for metro project.

2.0 DETAILS OF SITE & GENERAL GEOLOGICAL HISTORY

The location of proposed site is situated in between Jhotwara and Bagru block of district Jaipur in the state of Rajasthan. As per IS 1893, the site falls under seismic zone II (Seismic intensity – Low), which corresponds to a Modified Mercalli Intensity of VI. In seismic design, Zone factor Z of 0.10 is recommended for Zone-II.

From Field Investigation study, it was observed that strata is in cohesionless in nature. The strata observed at site is generally of medium dense to dense below EGL which becomes very dense as the depth increases.

Local Geology

CEG Test House & Kesearch Centre Pvt. Ltd.

AIPUR

The generalized geological sequence as observed in the field can be summarized as under:

Jaipur district is located in the eastern part of Rajasthan. It is bounded in the north by Sikar district, in the east by Alvar and Dausa districts, in the south by Tonk districts and in the west by Ajmer and Nagaur districts. It stretches between 26° 26' 08.11" to 27° 51' 52.11" north latitude and 74° 54'

- Atterberg's Limits 0
 - (a) Liquid limit
 - (b) Plastic limit
 - (c) Plastic Index
- Specific gravity 0
- Bulk and dry densities 0
- Consolidation tests 0
- Triaxial tests 0
- Direct shear test Ο
- Chemical tests on soil samples

• On rock samples

- Moisture content, porosity & Density 0
- Specific gravity 0
- Unconfined compression test (both at saturated and in-situ water content) 0
- Point load strength index 0
- Submitting draft report including all field records and laboratory test results, graphs etc. all complete as per specification.

4.1 **FIELD INVESTIGATION**

For geotechnical investigation work, drilling rig was installed at the specified borehole location along with the required men & machineries for conducting the requisite field work. The location of borehole is shown vide location plan attached under Appendix - A1. The details of borehole locations are shown here in below:-

S. No.	Chainage (km)/Struct ure	BH No.	Depth of Water Table below EGL	Depth of Borehole below EGL (m)		nates (m)
			(m)	、 <i>,</i>	E	Ν
1		BH-01			582249.000	2978146.000
2		BH-02	Not Encountered	40	582353.000	2978119.000
3		BH-03			582463.000	2978080.000
4	Underground section	BH-04			582567.000	2978046.000
5	Section Rail C	BH-05			582676.000	2978047.000
6	allo http://	BH-06			582788.000	2978022.000
7	E Ray	B€€-07			583035.000	2977962.000
CEG Test Ho	Use & Research Cen	itre Pvt. Ltd.	5 R1 of 292			CEGTH CEG TEST HOUSI

Table 1.1: Details of Borehole Locations

SR-837_23-24

Geo-technical Investigation work for Extension of underground and elevated section E-W Corridor from Badi Chouper to Transport Nagar (2.85Km) Phase-1C and Mansarovar to Ajmer Road (Chauraha) (1.35 km) Phase-1D of Jaipur Metro Rail Corporation at Jaipur.

	*			
8	BH-08	5	83134.000	2977927.000
9	BH-09	5	83240.000	2977907.000
10	BH-10	5	83335.000	2977897.000
11	BH-11	5	83426.000	2977864.000
12	BH-12	5	83532.000	2977857.000
13	BH-13	5	83655.000	2977804.000
14	BH-14	5	83776.000	2977804.000
15	BH-15	5	83871.000	2977775.000
16	BH-16	5	83966.000	2977752.000
17	BH-17	5	84034.000	2977720.000
18	BH-18	5	84169.000	2977715.000
19	BH-19	5	84252.000	2977669.000
20	RJST-01	5	82888.000	2978033.000
21	RJST-02	5	82863.000	2977984.000
22	RJST-03	5	82916.000	2977951.000
23	RJST-04	5	82933.000	2978009.000

4.2 FIELD INVESTIGATION IN SOIL STRATA

Following practices were followed at site:

- > The locations of 23 boreholes, were marked on the ground as per the layout given by the Engineer in charge. These locations are shown in **Appendix-A1** attached subsequently.
- In soils, boreholes of 150mm dia. were drilled as per the standard procedure laid in IS: 1892 as per specifications
- > Boreholes were properly cleaned before taking any sample in soil.
- Standard Penetration Tests & collection of undisturbed / disturbed soil samples were conducted at the locations of various boreholes as per the specifications and at specified double

depths.

The detailed procedure adopted for conducting various field tests are described in the following paragraphs:

4.2.1 Standard Penetration Test

The Standard Penetration Test was conducted in boreholes at regular interval in depth as per IS 2131. The test was carried out using the standard split spoon sampler to measure the number of blows 'N'. Standard split spoon sampler was attached to an 'A' rod. It was driven from borehole bottom to a distance of 45 cm using a standard hammer of 63.5 kg falling freely from a height of 75 cm to the required depth. While driving, the number of blows required to penetrate every 15 cm are recorded. The total number of blows required for the last 30 cm is taken as 'N' value at that particular depth of the borehole. Wherever the total penetration was less than 45cm, the no. of blows & the depth penetrated is recorded in the respective bore logs.

SPT 'N' values were correlated with relative density of non-cohesive stratum and with consistency of cohesive stratum as given below:-



6 R1 of 292



Geo-technical Investigation work for Extension of underground and elevated section E-W Corridor from Badi Chouper to Transport Nagar (2.85Km) Phase-1C and Mansarovar to Ajmer Road (Chauraha) (1.35 km) Phase-1D of Jaipur Metro Rail Corporation at Jaipur.

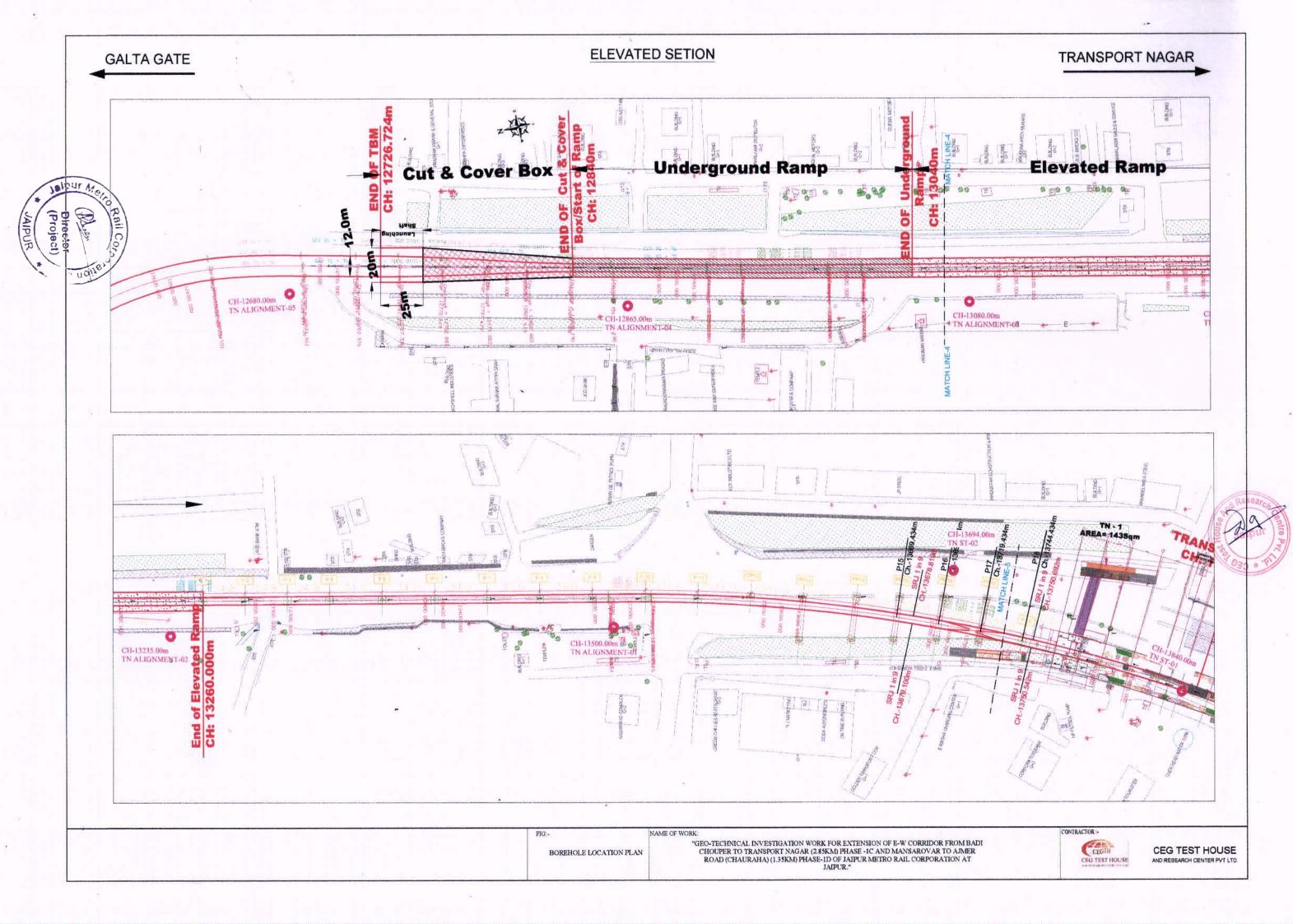
COREBOX PHOTOGRAPHS



UNDERGROUND_BH-18







Geotechnical Investigation Report

Elevated Section (Galta Gate to Transport Nagar)

SR NO. : 837_23-24

GEO-TECHNICAL INVESTIGATION WORK FOR EXTENSION OF UNDERGROUND AND ELEVATED SECTION E-W CORRIDOR FROM BADI CHOUPER TO TRANSPORT NAGAR (2.85KM) PHASE-1C AND MANSAROVAR TO AJMER ROAD (CHAURAHA) (1.35 KM) PHASE-1D OF JAIPUR METRO RAIL CORPORATION AT JAIPUR IN THE STATE OF RAJASTHAN

CLIENT

M/s. JAIPUR METRO RAIL CORPORATION LTD.

PROGRAMME

APRIL - 2023

SR. No.	Report No.	Revision No.	Date
837_23-24	CEGTH/JMRCL/SR-837/2023-24/374_(07 BHs)	01	30.06.2023
837_23-24	CEGTH/JMRCL/SR-837/2023-24/195_(07 BHs)	00	05.06.2023



B-11(G), Malviya Industrial Area, Jaipur-302017Tel. : 91-141-4046599, Fax : 91-141-2751806E-mail : info@cegtesthouse.com., www.cegtesthouse.com

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Njai

Nehal Jain

General Manager-Geotechnical

Tamoghna Dasgupta Geotechnical Manager



Geo-technical Investigation work for Extension of underground and elevated section E-W Corridor from Badi Chouper to Transport Nagar (2.85Km) Phase-1C and Mansarovar to Ajmer Road (Chauraha) (1.35 km) Phase-1D of Jaipur Metro Rail Corporation at Jaipur

CEGTH/JMRCL/SR-837/2023-24/374

Date: - 30.06.2023

To,

Jaipur Metro Rail Corporation Ltd., 1st Floor, Administrative Building Wing-A, Bhrigu Path, Mansarovar Metro Depot, Jaipur - 302020 Tel. No. 0141-2822781 E Mail - dp@jaipurmetrorail.in

Subject :- Geo-technical Investigation work for Extension of underground and elevated section E-W Corridor from Badi Chouper to Transport Nagar (2.85Km) Phase-1C and Mansarovar to Ajmer Road (Chauraha) (1.35 km) Phase-1D of JAIPUR METRO RAIL CORPORATION at Jaipur

Dear Sir,

We are pleased to submit this report of 07 boreholes for elevated section (Galta Gate to Transport Nagar) for the proposed project.

The accompanying report presents field and laboratory test results, interpretation of test results as required for design and construction of foundations.

Should there be any clarifications regarding the contents please contact us at your most convenient time.

We value the opportunity to participate in this project and look forward a pleasant association on future projects.

Very truly yours, CEG Test House & Research Centre Pvt. Ltd.

AIPUR

Njoil

Nehal Jain General Manager - Geotechnical Authorized Signatory

Technical Advisor

Dr. Sarvesh Chandra (Geotechnical Expert) Former Professor, IIT Kanpur

SR. No. **Report Ref. No. Revision No.** Date CEGTREMARGD/SR-837/2023-24/374_(07 BHs) 837_23-24 01 30.06.2023 CEGTH/JMRCL/SR-837/2023-24/194_(07 BHs) 837_23-24 00 05.06.2023 Director CEG Test House & Kestarch Centre Vt. Ltd. CEGTH



Tamoghna Dasgupta Geotechnical Manager

CEG TEST HOUSE

Geo-technical Investigation work for Extension of underground and elevated section E-W Corridor from Badi Chouper to Transport Nagar (2.85Km) Phase-1C and Mansarovar to Ajmer Road (Chauraha) (1.35 km) Phase-1D of Jaipur Metro Rail Corporation at Jaipur

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SR-837_23-24

Geo-technical Investigation work for Extension of underground and elevated section E-W Corridor from Badi Chouper to Transport Nagar (2.85Km) Phase-1C and Mansarovar to Ajmer Road (Chauraha) (1.35 km) Phase-1D of Jaipur Metro Rail Corporation at Jaipur

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Geo-technical Investigation work for Extension of underground and elevated section E-W Corridor from Badi Chouper to Transport Nagar (2.85Km) Phase-1C and Mansarovar to Ajmer Road (Chauraha) (1.35 km) Phase-1D of Jaipur Metro Rail Corporation at Jaipur

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Local Geology

The generalized geological sequence as observed in the field can be summarized as under:

Jaipur district is located in the eastern part of Rajasthan. It is bounded in the north by Sikar district, in the east by Alvar and Dausa districts, in the south by Tonk districts and in the west by Ajmer and Nagaur districts. It stretches between 26° 26' 08.11" to 27° 51' 52.11" north latitude and 74° 54'

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Geo-technical Investigation work for Extension of underground and elevated section E-W Corridor from Badi Chouper to Transport Nagar (2.85Km) Phase-1C and Mansarovar to Ajmer Road (Chauraha) (1.35 km) Phase-1D of Jaipur Metro Rail Corporation at Jaipur

52.59" to 76°17' 34.36" east longitude covering an approximate area of 11,136 sq kms. The district is drained by several rivers viz., Banganga, Banas, Sabi and Shekhawati rivers and streams like: Bandi, Mashi, Dhund, Morel, Mendha, Gumti ka Nala, Madhobini, Sota etc.

Geologic succession of Jaipur district is quite wide ranging in terms of age and rocks from Archean to Recent age are present in the area. Most of the north eastern part of the district is covered by younger and older alluvium which is predominantly sandy and clayey in nature. In some parts of western Jaipur eolian sand is also present as a thin cover above the alluvium sediments. Some parts in the northeastern region also show presence of Delhi Super Group quartzites, schists, phyllites and marbles. Most of the southern half of the district is occupied by Gneisses and schists of Bhilwara Super Group.

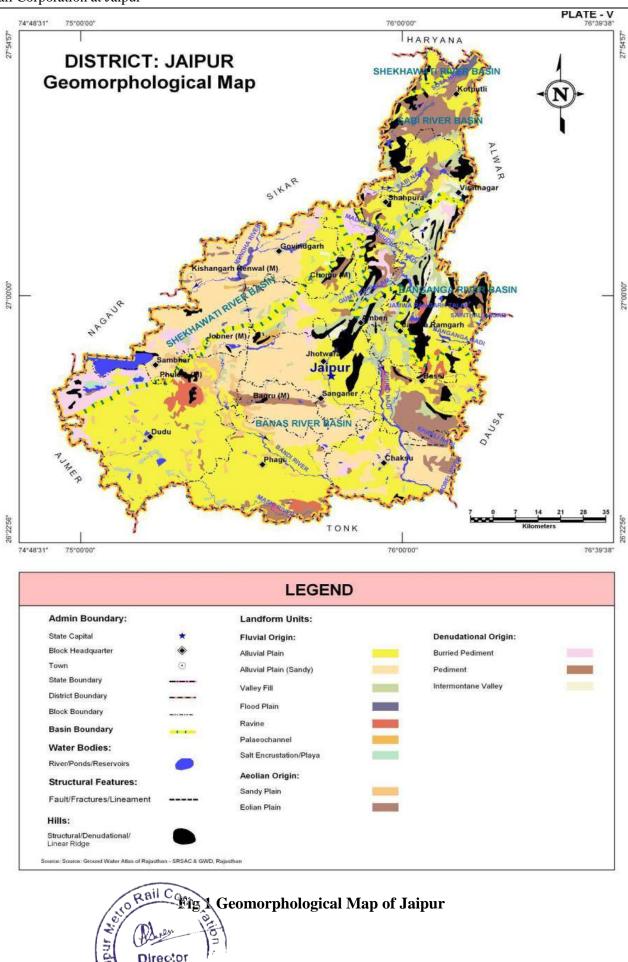
Super Group	Group	Formation
-	Recent to sub-recent	Sand, Clay, Clay Kankar etc.
Post Delhi		Granite, Pegmatite, amphobolite (intrusive)
Delhi	Ajabgarh	Schists, Phyllites, Marble and Quartzite
	Alwar	Quartzite, Conglomerate and Schists
	Raialo	Dolomitic marble and Quartzite
Bhilwara	-	Gneisses, Schists and Migmatites

Table:	Geologic	succession
	000008-0	

The proposed site is placed in alluvial plain (sandy) which is flat to gentle undulating plain formed due to fluvial activity, mainly consists of gravels, sand, silt and clay with unconsolidated material of varying lithology, predominantly sand along river.









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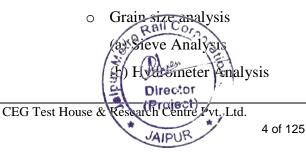
CLIMATIC CONDITION

Jaipur district has a semi-arid climate. There are three distinct seasons in a year. The winter season from November encompassing four months to February are mild and pleasant, with average temperatures in the 15°-18° C range and low humidity. December and January are the coldest months when temperature varies between 5°C and 10°C. There are however, occasional cold waves that lead to significant reduction of temperatures. March is a pleasant transition month to summer. The summer months of April to June record average daily temperature of around 35°C. May and June are the hottest months in Jaipur district. Temperature reaches up to 48°C in these months. Most of the annual rainfall is received in the monsoon months between June (end of June) and September.

3.0 SCOPE OF WORK

The stipulated scope of work involved carrying out the following operations:-

- Mobilization & Demobilization of drilling rig and all other required equipment, tool & tackles for carrying out investigation work on-land investigation.
- Shifting from one structure to other structure and set up to rigs and manpower along with other tools.
- Drilling of 150 mm dia boreholes in all type of soil/ rock up to required depth below existing ground surface and conducting standard penetration test at 1.5 meter interval on every change of strata as per IS-2131-1981 including collection of disturbed/undisturbed soil samples at every 1.5m interval and recording depth of ground water table, conducting the lab tests analyzing the test results including determination of SBC & penetration of report.
- Wherever refusal strata with characteristics of rock is encountered before achieving the required depth, boreholes as above are to be further extended up to required depth in all types of rock using hydraulic feed rotary drill and triple tube core barrel with diamond bit including collection of core samples.
- Carrying out the following Laboratory tests on the selected Soil samples in order to establish their engineering characteristics :
- On soil samples
 - o Moisture content





- Atterberg's Limits
 - (a) Liquid limit
 - (b) Plastic limit
 - (c) Plastic Index
- Specific gravity
- Bulk and dry densities
- Consolidation tests
- Triaxial tests
- Direct shear test
- Chemical tests on soil samples

• On rock samples

- Moisture content, porosity & Density
- Specific gravity
- Unconfined compression test (both at saturated and in-situ water content)
- Point load strength index
- Submitting draft report including all field records and laboratory test results, graphs etc. all complete as per specification.

4.0 FIELD INVESTIGATION

For geotechnical investigation work, drilling rig was installed at the specified borehole location along with the required men & machineries for conducting the requisite field work. The location of borehole is shown vide location plan attached under **Appendix - A1**. The details of borehole locations are shown here in below:-

S. No.	Chainage (km)/Stru cture	BH No.	Depth of Water Table below EGL	Depth of Borehole below	Co-ordinates (m)	
			(m)	EGL (m)	E N	Ν
1		TNST-01		40	583984.000	2976349.000
2		TN Alignment-01		40	584086.000	2976670.000
3		TNST-02		40	584079.000	2976467.000
4	Elevated Section	TN Alignment-05	Not Encountered	40	584247.000	2977483.000
5		TN Alignment-02	Lincountered	40	584132.000	2976927.000
6	A A A A A A A A A A A A A A A A A A A	TN Alignment-03		40	584164.000	2977091.000
7	N. N	Alignment-04		40	584201.000	2977289.000
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Table 1.1: Details of Borehole Locations



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4.1 FIELD INVESTIGATION IN SOIL STRATA

Following practices were followed at site:

- The locations of 07 boreholes, were marked on the ground as per the layout given by the Engineer in charge. These locations are shown in Appendix-A1 attached subsequently.
- In soils, boreholes of 150mm dia. were drilled as per the standard procedure laid in IS: 1892 as per specifications
- > Boreholes were properly cleaned before taking any sample in soil.
- Standard Penetration Tests & collection of undisturbed / disturbed soil samples were conducted at the locations of various boreholes as per the specifications and at specified depths.
 - > The detailed procedure adopted for conducting various field tests is given here in below.

The detailed procedure adopted for conducting various field tests are described in the following paragraphs:

4.1.1 Standard Penetration Test

The Standard Penetration Test was conducted in boreholes at regular interval in depth as per IS 2131. The test was carried out using the standard split spoon sampler to measure the number of blows 'N'. Standard split spoon sampler was attached to an 'A' rod. It was driven from borehole bottom to a distance of 45 cm using a standard hammer of 63.5 kg falling freely from a height of 75 cm to the required depth. While driving, the number of blows required to penetrate every 15 cm are recorded. The total number of blows required for the last 30 cm is taken as 'N' value at that particular depth of the borehole. Wherever the total penetration was less than 45cm, the no. of blows & the depth penetrated is recorded in the respective bore logs.

SPT 'N' values were correlated with relative density of non-cohesive stratum and with consistency of cohesive stratum as given below:-

Correlation for Cla	y / Plastic silt	Correlation for Sand / Non-Plastic silt		
Consistency	SPT 'N' Value	Compactness	SPT 'N' Value	
Very Soft	0 - 2	Very Loose	0 - 4	
Soft	2 - 4	Loose	4 - 10	
Medium	4 - 8	Medium	10 - 30	
Stiff	8 - 15	Dense	30 - 50	
Very Stiff Rail Co	15 - 30	Very Dense	> 50	
Hard	≥ 30			

Table 1.2: Soil compactness as per SPT N values (cl. 9.7, table 9.3 & 9.4, page 330_text book of V.N.S. Murthy)

The field SPT N values were corrected as per the guidelines given in IS: 2131 as follows:



(*b*) *Due to dilatancy* :- Wherever N values observed below water table in fine sand, silty sand or silt was greater than 15, then corrected N values were corrected as under:

N' =15 + $\frac{1}{2}$ (N-15)

4.1.2 Undisturbed Sampling (Soil) in boreholes

Undisturbed soil samples were collected using MS tubes of required size and length with Area ratio as per clause 4.1.1 (c) of IS: 1892 (latest) fitted to an adopter with ball and socket arrangement. Before taking any sample, sampling tube was properly greased. Immediately after taking on undisturbed sample in a tube, the adopter head was removed along with the disturbed material. The visible ends of the sample were trimmed off any wet disturbed soil. The ends were coated alternately with four layers of just molten wax. More molten wax was added to give a total thickness of min. 25 mm. The samples were carefully labeled and transported to the laboratory for testing. Undisturbed samples wherever slipped during lifting were duly marked in the field logs as well as in the soil profile.

4.1.3 Disturbed Soil sampling in boreholes

Disturbed soil samples were collected at regular interval & at every identifiable change of strata. Samples were immediately sealed, labeled and carefully transported to the laboratory for testing.

4.1.4 IN-SITU PERMEABILITY TEST

(A) CONSTANT HEAD METHOD

Introduction:

In-situ permeability test shall be conducted to determine the water percolation capacity of overburden soil. This test shall be performed inside the bore hole at specified depths or in each layer or as per the directions of the Engineer. The type of test shall be either pump in or pump-out test depending on the sub soil and ground water conditions.

Constant Head Method:

This test shall be conducted in bore holes where soil has a high permeability; water shall be allowed in to the bore hold through a metering system ensuring gravity flow at constant head so as to maintain a steady water level in the bore hole. A reference mark shall be made a convenient level which can be easily seen on the casing pipe to note down the fluctuations of water level. The fluctuations shall be constant at a varying the quantity of water flowing in to the bore hole. The Director

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elevation of water shall be observed at every 5 minute interval. When three consecutive readings show constant value, the necessary observations such as flow rate, elevation of water surface above test depth, diameter of casing pipe, etc. shall be made and recorded as per the proforma recommended in IS: 5529,Part-I.

The test was repeated till Constant records of water level was achieved.

The result of in-situ field permeability tests are given below:

(B) Falling Head Method

In-situ permeability test using Falling Head method were conducted to determine the water percolation capacity of overburden soil. This test was performed inside the bore hole at specified depths or in each layer or as per the directions of the Engineer.

The coefficient of permeability was evaluated on the basis of Darcy's law which states that the rate of flow through a porous media is proportional to the hydraulic gradient.

In this method the water level in the test hole was allowed to fall and the equivalent permeability is computed from the data of rate of fall of the water level.

For conducting the test, a borehole upto the level of the test depth was drilled. Then the BH was cleaned and casing of 150mm dia. was inserted above the test depth and fill the borehole with water up to the top of the casing and record the rate of fall of water.

The permeability of soil overburden by falling head method is obtained by using the following expression:

 $K = (d^2/8L) \log [(L/r)(\log_e(h_1/h_2)/(t_2-t_1)]$

where,

K = coefficient of permeability

d = diameter of intake pipe

L = length of test zone

 h_1 = head of water at time t_1

 $h_2 = head of water at time t_2$

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r = radius of hole.

The fall in the water level was recorded at regular intervals as mentioned in IS: 5529, Part-I.

Sr. No.	BH No	Depth of test section below EGL	Test Section Length (m)	Coefficient of permeability
	pail Co.	(m)	()	k (cm/s)
1	TEN CTN 01	20.25 - 21.00	0.75	2.34 x 10 ⁻⁴
2		30.25 - 31.00	0.75	2.74 x 10 ⁻⁴
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Table 1.3 (B): In-situ Soil Permeability Test



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3	- TN STN 02	12.00 - 12.75	0.75	2.59 x 10 ⁻⁴
4		20.00 - 20.75	0.75	2.77 x 10 ⁻⁴

Note: The results of field permeability tests are shown vide Appendix – A4.

4.1.5 FIELD INVESTIGATION IN ROCK STRATA

Drilling was done by rotary core drilling method using Double tube core barrels as per the guidelines of IS: 6926-1196, because of its ability in retaining higher quality of rock samples. A core barrel and Nx sized bits were used for drilling and recovering rock cores. Recovered rock cores were numbered serially and preserved in good quality sturdy wooden core boxes as specified in IS: 4078-1980. Rock core recovery and Rock Quality Designation (RQD) were computed for every run length. Water was used as the drilling fluid. The ratio of total length of rock pieces collected to length drilled, expressed as percentage and known as core recovery was recorded. To obtain RQD (Rock Quality Designation), only those pieces of rock which were 10 cm and longer were measured for the total length. The above length divided by length drilled, expressed as percentage, was recorded as RQD. The Core Recovery and RQD value were assigned based on Standard procedure given in IS: 11315 (Part 11).

Thus

- (a) Core recovery in % = (Length of Core / Length of run) x 100
- (b) RQD in % = (Length of core in pieces of 100mm and above / Length of run) x100

Rock classification in terms of weathering, state of fractures & strength was carried out in the following manner as tabulated below:-

Terms	Description	Grade		
Fresh	No visible sign of rock material weathering; perhaps slight discoloration on major discontinuity surfaces.	Ι		
Slightly Weathered	Discoloration indicates weathering of rock material and discontinuity surfaces. All the rock material may be discolored by weathering and may be somewhat weaker externally that in its fresh condition.	П		
Moderately Weathered	Less than half of the rock material is decomposed or disintegrated to a soil. Fresh or discolored rock is present either as a continuous framework or as core stones.	III		
Highly Weathered	More than half of the rock material is decomposed and/or disintegrated to a soil. Ereship consolored rock is present either as a discontinuous framework or as one stones.	IV		
Completely Weathered	Alt ock merial redecomposed and/or disintegrated to soil. The original mass structure is still largely intact.	V		
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Table 1.2: Scale of Weathering Grades of Rock Mass [cl. 3.6.2.2 of IS: 4464]



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Terms	Description	Grade
Residual Soil	All rock material is converted to soil. The mass structure and material fabric are destroyed. There is a large change in volume, but the soil has not been significantly transported.	VI

As per IS 4464 it should be understood that all grades of weathering may not be seen in a given rock mass and that in some cases a particular grade may be present to a very small extent. Distribution of the various weathering grades of rock material in the rock mass may be decided related to the porosity of the rock material and the presence of open discontinuities of all types in the rock mass.

Rock classification based on their physical condition and Unconfined Compressive Strength based on Clause 8.2 and Table -2 of IRC: 78-2014 as follows:-

Rock Type	Description	Unconfined Compressive Strength (UCS) in MPa
Extremely Strong	Cannot be scratched with knife or sharp pick. Breaking of specimen could be done by sledge hammer only.	> 200
Very Strong	Cannot be scratched with knife or sharp pick. Breaking of specimens requires several hard blows of geologists' pick.	100 to 200
Strong	Can be scratched with knife or pick with difficulty. Hard blow of hammer required to detach hand specimen.	50 to 100
Moderately Strong	Can be scratched with knife or pick, 6mm deep gouges or grooves can be made by hand blow of geologists' pick. Hand specimen can be detached by moderate blow.	12.5 to 50
Moderately weak	Can be grooved or gouged 1.5mm deep by firm pressure on knife or pick point. Can be broken into pieces or chips of about 2.5mm maximum size by hard blows of the geologists' pick.	5 to 12.5
Weak	Can be grooved or gouged easily with knife or pick point. Can be break down in chips to pieces several cm's in size by moderate blows of pick point. Small thin pieces can be broken by finger pressure.	1.25 to 5
Very Weak	Can be carved with knife. Can be broken easily with point of pick. Pieces 25mm or more in thickness can be broken by finger pressure. Can be scratched easily by finger nail.	< 1.25

Relation between Role and In-situ Rock Quality

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Rock quality is further measured by frequency of natural joints in rock mass. RQD is used to define state of fractures at massiveness of rock. Following table defines the quality of rock mass as per

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	- •
Rock Type	RQD (%)
Excellent	90 - 100
Good	75 - 90
Fair	50 - 75
Poor	25 - 50
Very Poor	< 25

Table 1.4: Core Quality

5.0 LABORATORY INVESTIGATION

5.1 LABORATORY TESTS ON SOIL SAMPLES

The details of various test conducted on selected undisturbed/disturbed soil samples are given below:

Description of Test	Standard Code Applicable	Undisturbed Soil Samples	Disturbed Soil / SPT Samples
Sieve Analysis / Hydrometer	IS: 2720 (Part – 4)	\checkmark	\checkmark
Liquid LimitPlastic Limit	IS: 2720 (Part – 5) IS: 2720 (Part – 5)	\checkmark	\checkmark
Natural Moisture Content / Bulk / Dry density	IS : 2720 (Part – 2)	\checkmark	-
Specific Gravity	IS: 2720 (Part – 3)	\checkmark	\checkmark
Direct Shear Test	IS: 2720 (Part – 13)	\checkmark	\checkmark
Triaxial shear test	IS: 2720 (Part – 11)	-	-
Consolidation Test	IS: 2720 (Part – 15)	_	-
Chemical Analysis of Soil Samples	IS: 2720 (Part – 26, 27)	\checkmark	

• The results of various laboratory tests conducted on selected soil samples are shown vide **Appendix – B.**

The detailed procedure adopted for conducting various laboratory tests is described in the following paragraphs:

5.1.1 Grain Size Analysis (IS: 2720- Part-4)

Wet sieve analysis:

For determination of particle sizes finer than 75 micron, wet sieve analysis test was conducted. For this test, oven dried sample of known quantity was taken in a container and soaked with dispersing agent. The soaked soil sample was washed thoroughly over 75 micron IS sieve until the water passing sieve was substantiantly clean.

Fraction retained in 75 minron hos eve was carefully collected in a container without any loss in material and place into rector drying.

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Dry sieve analysis:

For this test, the oven dried soil sample after wet sieving was sieved through the set of IS sieves 20 mm, 10 mm, 4.75 mm, 2.0 mm, 425 micron and 75 micron. The amounts of soil retained on each sieve were noted down. The % retained, cumulative % retained and % passing were computed accordingly. Wherever the soil sample % passing 75 micron sieve was significant, Hydrometer method was used to find the percentage of silt and clay fraction.

Grain size analysis for the fraction passing 75 micron IS Sieve (Hydrometer method)

Calibration of Hydrometer

Hydrometer was calibrated to determine a relationship (an equation) between the effective depth H_R and corresponding hydrometer reading R_h (obtained during test).

50 to 100 gm of soil sample passing through 75 micron IS Sieve was taken. It was mixed with 100 ml of sodium hexametaphosphate solution and the mixture was warmed for about 10 minutes. It was then transferred to the cup of the mechanical mixer and the soil suspension was stirred for 15 minutes. The soil suspension was transferred into 1000 ml measuring cylinder and distilled water was added to make 1000ml solution. This solution was mixed vigorously. The measuring cylinder was then allowed to stand and the stopwatch was started. Hydrometer was immersed in the solution and reading were taken after half, one, two and four minutes. The hydrometer was then removed slowly and kept in distilled water at the same temperature as the soil suspension. Readings were taken after the periods of 8, 15 and 30 minutes, and one, two and four hours. Hydrometer was removed, rinsed and placed in the distilled water after each reading. After 4 hours reading was taken once or twice within 24 hours. Finally a reading was taken at the end of 24 hours. The temperature of the suspension was observed and recorded.

Calculations

Diameter of the particles (D):

$$D = \sqrt{\frac{30\mu}{980(G-1)}} \times \sqrt{\frac{H_R}{t}} = \sqrt[M]{\frac{H_R}{t}}$$

Where,

= diameter of particle in suspension, in mm; D

= co-efficient of viscosity of water at the temperature of the suspension at the time of μ taking the hydrometer reading, in poise;

$$G$$
 = specific gravity cot the soil fraction used in the sedimentations analysis;

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$$H_R$$
 = effective depth corresponding to R_n , in cm.

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t = time elapsed between the beginning of sedimentation and taking of hydrometer reading in minutes

$$M = \sqrt{\frac{30\mu}{980(G-1)}} = \text{a constant factor for given values of } \mu \text{ and } G \text{ at the temperature of the}$$

suspension.

Percentage finer than diameter D:

The percentage by mass (w) of particles smaller than corresponding equivalent particle diameters (D) was calculated from the formula:

$$w = \frac{100G_s}{W_b(G_s - 1)} \times R_f$$

Where

w = percentage finer

 G_s = specific gravity of soil particle

 W_b = weight of soil

 R_h = Hydrometer reading

5.1.2 Liquid Limit (IS: 2720- Part-5)

By Cone Penetrometer Method

The 'Cone Penetrometer Apparatus' is a variant of the fall-cone and consists of a cone with a smooth polished surface and angle of $30^{\circ} \pm 1/2^{\circ}$. The weight of the cone, together with its associated shaft is $80g \pm 0.5g$. A support assembly with an automatic cone release mechanism and cone height adjustment mechanism used to hold the cone vertically. The angle and weight of the cone were calibrated at regular intervals, and the sharpness of the cone tip was checked daily.

Distilled water was added and thoroughly mixed with the soil sample to produce a homogeneous paste. The paste was then placed in a cup with a diameter of at least 55mm and a depth of at least 40mm. The surface of the soil was smoothed off level and parallel to the base. The support assembly was used to position the tip of the cone so that it was just touching the top surface of the soil, and the automatic tripping mechanism was released. The cone was allowed to penetrate into the soil for a period of 5 (\pm 1) s, then the cone was locked off to stop further movement and the penetration was recorded. The cup was refilled and the test was repeated. The two recorded penetrations need to be within 0.5mm of each other, otherwise a third test is performed, when the three test vary by many than trime the test was repeated.

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Further tests were conducted, at varying water contents, in order to produce a series of cone penetrations (usually 4) in the range 15mm to 25mm. The resulting cone penetrations were plotted verses the water content of the test specimens. The Liquid Limit (W_L) was read off the graph, being the water content at which the line of best fit through the test points crosses 20mm penetration.

5.1.3 Plastic Limit (IS: 2720-Part-5)

For this test, soil sample was prepared in the same way as for liquid limit test. A ball of soil sample weighed about 5 gm was formed. The ball was rolled between the fingers of one hand and the glass plate with pressure sufficient to reduce the mass into a thread of about 3 mm in 5 to 10 complete forward and back movements. When a diameter of 3 mm was reached, soil was again remolded into a ball. The process of rolling and remolding was repeated until the thread started just crumbing at a diameter of 3 mm. The crumbled thread was immediately transferred to an airtight container for determination of its moisture content by oven drying method.

This water content has been termed as plastic limit. (WP)

5.1.4 Plasticity Index (IS: 2720-Part-5)

The plasticity index Ip was given by

I_p=W_L-W_P (in percent)

5.1.5 Direct Shear Test (IS:2720-Part-13):

For this test shear box test apparatus was used. The prepared specimen from remolded/undisturbed sample was placed carefully in the box. The plain grid was kept on top of the specimen with its directions at right angles to the direction of shear. The upper porous stone was placed on the grid and loading pad on the stone. The box with specimen was gently placed in the container (water jacket). The specimen was submerged with water. The container was mounted with the shear box and the specimen inside, on the shearing machine. The upper part of the box was so adjusted that it touched the proving ring. The jack was brought forward to bear up against the box container. The proving ring dial gauge was set to read zero.

The steel ball was placed in the recess of the loading pad. The loading yoke was set in contact with the steel ball on the loading pad. Vertical displacement dial gauge to read zero in contact with the top of the yoke. The normal load was applied and any change in thickness of specimen was recorded. Shear displacement dial gauge was also set to read zero. The locking screw was now removed and two parts of the shear box were separated by advancing the spacing screws.

The specimen was sheared at constant rate of strain. The readings of the proving ring dial gauge were noted down event is seconds for the first one-minute and then every 30 seconds thereafter. The reading of the same the thickness dial gauge and shear displacement dial gauge were also recorded at the same tip recorder val. The test was continued until the specimen fails. The specimen

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was assumed to fail when the proving ring dial gauge started receding or at shear displacement of approximately 15% of the length took place.

The soil was removed from the box and test was repeated on the identical specimen under increased normal load.

5.1.6 Triaxial Shear Test_UUT (IS: 2720-Part-11)

For this test, Triaxial Shear Test apparatus was used. The plain disc was placed on the pedestal of the triaxial cell. The specimen was placed centrally on the disc. A correct size rubber membrane was fitted inside the stretcher with ends of membrane folded over those of the stretcher. Vacuum was applied to stretch the membrane to the inside surface of the stretcher which was carefully slipped around the specimen kept on the pedestal. The vacuum on the membrane was released. Its bottom part was rolled down into the pedestal. plain disc was placed on the top of the specimen and then loading pad was placed. The top part of membrane was rolled on to the loading pad. Then the stretcher was removed and ends were sealed with 'O' rings. With the properly sealed specimen placed centrally on the pedestal, the cell was assembled, keeping the loading piston initially clear of the loading pad of the specimen, the assembly was placed in the loading frame.

For unconsolidated undrained test, the bottom drainage value (BDV) and top drainage value (TDV) of cell, was closed and air release valve (ARV) was opened. The cell was filled with water through the cell water value CWV. ARV was closed when water begins to escape through it. The cell pressure was raised to the desired value and kept constant till the end of the test.

When the cell pressure was applied, the load piston rises upward, the loading machine was operated at the anticipated rate to bring the load piston slightly above the loading pad of the specimen and the load measuring dial gauge on proving ring was set to zero.

The piston was brought just in contact with loading pad by hand operation of the machine. The axial compression dial gauge was mounted and set to read zero.

The axial loading was started at 1.25 mm/min rate of strain. Simultaneous readings on the load and compression dial gauges were noted down. The test was continued until a recession of the axial load is observed or 20% of strain.

After failure, the specimen was unloaded by reversing the loading machine, cell pressure was reduced and cell water was drained out through BRV. The cell was dismantled and the specimen was taken out, rubber membrane was removed and weight of the failed sample and its water content was determined. The test was repeated on two more identical specimens with increasing cell pressure.





5.2 LABORATORY TESTS ON ROCK CORE SAMPLES

Rock samples recovered from various depths of strata were tested for the following properties:

Description of Test	Specifications
Preparation of rock specimen	IS : 9179
Specific gravity, porosity and water absorption	IS : 13030
Unconfined Compressive Strength (UCS)	IS : 9143
Modulus of Elasticity	IS: 9221
Point Load Index (PLI)	IS : 8764

• The results of various laboratory tests conducted on selected rock core samples are shown vide **Appendix – B.**

The detailed procedure adopted for conducting various laboratory tests is described in the following paragraphs:

5.2.1 Preparation of Rock Specimen (IS: 9179)

The core cut-off machine was used for cross cutting of rock core. Rock core was clamped in a veeblock slotted to permit passage of wheel. Core was supported on both sides of the cut to avoid spalling. Edge grinding was done using lathe. Sample was held directly in the chuck and rotated and the grinding wheel was passed against it.

5.2.2 Water Absorption (WA) & Specific Gravity (SG) (IS: 13030)

Following procedure was adopted to determine water absorption and specific gravity of rock samples.

Approximately 500g of rock sample was thoroughly washed to remove finer particles and dust and then immersed in distilled water for a period of $24 \pm \frac{1}{2}$ hours. Mass of the basket submerged in the immersion bath was noted down. Sample was transferred under water to the basket in the immersion bath. Saturated submerged mass of the basket plus sample was noted. Massof the clean dry sample container and lid was noted. Sample was removed from the immersion bath and surface dried. Mass of the saturated surface dry sample plus container was noted. Sample and the container with lid was oven dried. Dried mass was noted.

5.2.3 Unconfined Compressive Strength (UCS) (IS: 9143)

For the determination of UCS of rock core, length to diameter ratio of the cylindrical specimen was kept between 2.0 to 3.0. The specimen ends were made flat. The specimen was kept on the lower disc of compression testing machine. The axis of the specimen was carefully aligned with the center of the thrust of the specime specimen was applied continuously at a constant stress rate such that failure takes there in about 5 to 15 minutes of loading. The maximum load on the specimen was eccolled. The unconfined compressive strength of the specimen was calculated



by dividing the max load carried by the specimen during the test by the average original crosssectional area.

5.2.4 Point Load Index (PLI) (IS:8764)

The diameter 'D' of the specimen measured in 'mm'. The core specimen was tested after soaking them. There are two methods to determine Point Load Index on rock cores.

a) Diametral Test

Core specimens with length/diameter ratio greater than 1.0 were used for diametral testing. The specimen was inserted in the test machine and the platens were closed to make contact along a core diameter, ensured the distance between contact point and the nearest free end was at least 0.50 times the core diameter.

Load was applied to the specimen such that failure occurs within 10-60s and the failure load 'P' is recorded.

b) Axial Test

Core specimens with length/diameter ratio of 0.3 to 1.0 are suitable for axial testing. The specimen was inserted in the test machine and the platens closed to make contact along a line perpendicular to the core end faces.

Load was then applied to the specimen such that failure occurs within 10-60s and the failure load 'P' was recorded.





CHAPTER 2 TEST RESULTS AND INTERPRETATION

6.0 STRATIFICATION

From the study of the borehole log of 07 BHs, it is revealed that the sub strata:-

At the location of BH-TNST-01

- a) From existing ground level to 3.00m depth, strata consist of filled up soil.
- b) From 3.00m to termination depth, strata consist of coarse grained soil i.e. Silty sand (SM).

At the location of BH-TNST-02

- a) From existing ground level to 3.00m depth, strata consist of filled up soil.
- b) From 3.00m to 27.50m depth, strata consist of coarse grained soil i.e. Silty sand (SM).
- c) From depth 27.50m to termination depth, strata consist of rocky strata i.e. Highly to completely weathered, medium grained, Sandstone/Quartzite.

At the location of BH-TN Alignment-01

- a) From existing ground level to 3.00m depths, strata consist of filled up soil.
- b) From depth 3.00m to 30.00m depth, strata consist of coarse grained soil i.e. Silty sand (SM)
- c) From depth 30.00m to termination depth, strata consist of rocky strata i.e. Highly weathered, very poor, medium grained Quartzite.

At the location of BH-TN-Alignment-02

- a) From existing ground level to 3.00m depths, strata consist of filled up soil.
- b) From depth 3.00m to 7.50m depth, strata consist of rocky strata i.e. Highly to completely weathered, medium grained, Sandstone/ Quartzite
- c) From depth 7.50m to 21.00m depth, strata consists of coarse grained soil i.e. Silty sand (SM).
- d) From 21.00m to 24.00m depth, strata consist of coarse grained soil i.e. Clayey sand (SC)
- e) From 24.00m to termination depth, strata consist of coarse grained soil i.e. Silty sand (SM)

At the location of BH-TN Alignment-03

- a) From existing ground level to 3.00m depth, strata consist of filled up soil.
- b) From 3.00m to 39.00m depth, strata consist of coarse grained soil i.e. Silty sand (SM)
- c) From depth 39.00m to termination depth, strata consist of coarse grained soil i.e. Clayey Silty Sand (SM-SC)

At the location of BH. Alignment-04



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- a) From existing ground level to 3.00m depth, strata consist of filled up soil.
- b) From depth 3.00m to termination depth, strata consist of coarse grained soil i.e. Silty Sand (SM)

At the location of BH-TN Alignment-05

- a) From Existing ground level to 3.00m depth, strata consist of filled up soil.
- b) From 3.00m to 24.00m depth, strata consist of coarse grained soil i.e. Silty sand (SM)
- c) From 24.00m to 28.50m depth, strata consist of coarse grained soil i.e. Clayey sand (SC)
- d) From depth 28.50m to termination depth, strata consist of coarse grained soil i.e. Silty Sand (SM)

6.1 GROUND WATER TABLE DEPTH

Water table is not met in the boreholes during investigation. However, for the analysis the water table has been considered to rise up to EGL.

6.2 **RESULTS OF CHEMICAL ANALYSIS**

Results of chemical analysis of soil samples (as per **Appendix** – **B2**) indicates that the soil sample falls under Class I for sulphates and chlorides concentration (As per IS 456-2000 and CIRIA Sp. Publication No. 31). The results are summarized here in below :-

Chemical Property	Findings	Remarks (Required limits as per IS 456-200)		
рН	8.14 to 8.24	> 6.0		
Sulphate as SO_4^{2-} (%)	0.0021 to 0.0029 (%)	< 0.2% (Class I)		
Chlorides as Cl ⁻ (%)	0.0031 to 0.0038 (%)	No limit specified in IS 456. However, a limit of 0.20% specified for class I in CIRIA Sp. Publication No. 31)		

Summary of chemical analysis of soil samples

6.3 COMPUTATION OF LIQUEFACTION POTENTIAL

Liquefaction is the sudden loss of shear strength of the sub soil strata due to earthquake-induced vibration under saturated conditions.

Assessment of liquefaction potential of foundation strata is made by simplified approach proposed as per IS: 1893 (Part-1)-2016, from the SPT data and peak ground acceleration likely to occur at the site. In this method, cyclic shear stress likely to be induced in the foundation strata by Design Basis Earthquake (DBE) is first evaluated.





Next threshold cyclic shear stress, which is good enough to cause liquefaction, is determined from SPT data and the empirical relations. Finally, comparison of these two stresses is used in the estimation of liquefaction susceptibility of the foundation strata.

Unsaturated soils are not subjected to liquefaction because vibratory forces from earthquakes do not cause any increase in pore water pressure in such soils.

The area of site from Badi Chouper to Transport Nagar and Mansarovar to Ajmer Road (Chauraha) in the State of Rajasthan falls in seismic zone – II of India as per IS: 1893. Further as per the provisions of IS: 1893 in soil deposits consisting of submerged loose sands & soils falling under classification of SP with standard penetration N value less than 15, the shaking caused by earthquake ground motion may cause liquefaction or excessive total and differential settlements. For the analysis of liquefaction potential, following constant parameters are considered:

EQ Zone	II
Earthquake Magnitude (Mw)	6.0
Peak Horizontal Ground Acceleration (amax /g)	0.10

For the cohesion less strata encountered in the borehole at site, the IS: 1893 (Part-1)-2016 is referred for the analysis of Liquefaction Potential and for the cohesive strata, RDSO BS-118 is referred.

As per IITK RDSO Guidelines- Appendix – (G) "Simplified Procedure for Evaluation of Liquefaction Potential (Clause 13.3):

- a. Cohesive soils should be considered liquefiable if wl≤ 37 %, Ip≤ 12 % and wn>0.80 wl is the liquid limit, where Ip is the Plasticity Index.
- b. Liquefaction susceptibility of soils should be considered marginal if wl ≤ 47 %, Ip≤ 20 % and wn≥ 0.85 wl, where Ip is the Plasticity Index.
- c. Cohesive soils should be considered non-liquefiable if wl>47 % or Ip>20 % or wn<0.85 wl, where Ip is the Plasticity Index.

As Ground water table was not encountered at the location of boreholes below EGL during investigation, it may rise up in rains/ rainy seasons. Therefore, for the liquefaction analysis of foundation, the water table has been considered to rise up to EGL. Further as per cl. C above liquefaction depth is given below:-





		Table 2.1: Results of	Liquefaction Anal	ysis	
S.No.	Ch. (km)/ Structure	BH No.	Water table depth met during field work (m)	Water table depth considered for analysis (m)	Liquefiable Depth below EGL (m)
1		TNST-01	Not Encountered	0	Non Liquefiable
2	ion	TNST-02	Not Encountered	0	Non Liquefiable
3	ject	TN Alignment-01	Not Encountered	0	Non Liquefiable
4	s pa	TN Alignment-02	Not Encountered	0	Non Liquefiable
5	Elevated Section	TN Alignment-03	Not Encountered	0	Non Liquefiable
6	Ele	TN Alignment-04	Not Encountered	0	Non Liquefiable
7		TN Alignment-05	Not Encountered	0	Non Liquefiable

Sample calculation for computation of liquefaction potential vide attached Appendix - C1





CHAPTER 3 TYPE AND DEPTH OF FOUNDATION WITH ANALYSIS

7.0 TYPE & DEPTH OF FOUNDATION:

Based on the nature & strength characteristics of the substrata, requirement of the project and discussions held with client, the following type of foundation have been analyzed as given below:

Chainage/Structure (km)	BH No.	Type of foundation	Depth of Foundation Below EGL (m)	Size of Foundation (m)
Elevated section	TN Alignement- 02, TN Alignment-03	Open Foundation	3 4 5	3 x 4 & 4 x 5

Chainage/ Structure (km)	BH No.	Type of foundation	Size of Foundation / Dia. of Pile (m)
	TNST-01, TNST-02, TN Alignment-01, TN Alignment-02,	Pile	1.00
Elevated section	TN Alignment-03, TN Alignment-04, TN Alignment-05	foundation	1.20

The details of foundation analysis are given in the subsequent paragraph.

7.1 ANALYSIS OF FOUNDATION

7.1.1 From Shear Failure Criteria

Net Safe Bearing capacity from Shear Failure consideration has been computed in accordance with IS: 6403-1981, which is based on, modified Terzaghi's classical approach. The weighted average of shear strength parameters for various strata upto depth equal to $0.5*B*Tan (45+\emptyset/2)$ (where B = Width of the Foundation, $\emptyset =$ Angle of internal friction) is used in the analysis. A factor of safety of 2.5 to estimate the net safe bearing capacity from ultimate net bearing capacity.

For soils, containing both coarse grained (gravels & sands) and fine grained (clays), c and Φ are used to determine the soil strength. In case of predominantly fine grained soils, c and Φ are determined by the Triaxial Compression test as per IS: 2720 pt XI. For predominantly coarse grained soils, c and Φ are determined by Direct Shear test as per IS: 2720 pt XIII. These c and Φ values were used for determining the SBC of soil as per shear failure criteria.

The ultimate net bearing capacity in case of general shear failure is given by following expression, $q_d = c N_c s_c d_c i_d + q (N_q i_q + (1/2) B \gamma N_\gamma s_\gamma d_\gamma i_\gamma W'$



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The ultimate net bearing capacity in case of local shear failure is given by following expression,

 $\begin{array}{l} q'_{d} = (2/3) \ c \ N'_{c} \ s_{c} \ d_{c} \ i_{c} + q \ (N'_{q} - 1) \ s_{q} \ d_{q} \ i_{q} + (1/2) \ B \ \gamma \ N'_{\gamma} \ s_{\gamma} \ d_{\gamma} \ i_{\gamma} \ W' \\ \\ Where, \\ d_{c} = 1 + 0.2 \ (D_{f} / B)^{*} SQRT(N_{\phi}) \\ d_{q} = d_{\gamma} = 1 \ for \ \phi < 10^{\circ} \\ d_{q} = d_{\gamma} = 1 + 0.1 \ (D_{f} / B)^{*} SQRT(N_{\phi}) \ for \ \phi > 10^{\circ} \\ \\ N_{\phi} = \tan^{2}(\pi/4 + \phi/2) \\ \phi' \ for \ local \ shear \ failure = \tan^{-1}(\ 0.67 \ tan\phi \) \end{array}$

The following soil parameter was assumed for calculations:

Chainage/Str ucture (km)	BH No.	Size of foundation (m)	Depth of foundation below EGL (m)	Cohesion 'C'(kg/cm2)	Angle of internal friction(ф)(Deg.)
	me 2		3	0	32
	TN Alignme nt-02		4	0	31
		3 x 4	5	0	31
ų	TN Mignme nt-03	5 X 4	3	0	32
ctic	TN Jignm nt-03	nt-0	4	0	32
Se	\checkmark		5	0	32
ted	nen		3	0	31
Elevated Section	TN Alignmen t-02		4	0	31
Ē		1 5	5	0	31
	TN Alignmen t-03	4 x 5	3	0	32
	TN gnm t-03		4	0	32
	Alig		5	0	32

7.1.2 From Settlement Failure Criteria

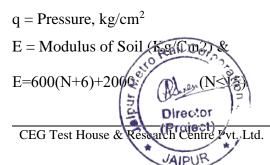
Allowable Bearing Pressure from Settlement Failure consideration has been computed in accordance with IS: 8009 (Part-I). The magnitude of settlement, when foundation loads are applied, depends upon the compressibility of the underlying strata and rigidity of the substructure.

The total permissible settlement in cohesion-less soil is estimated using clause **9.2.3.2** as per IS: 8009 (Part-I).

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Si =
$$(q B (1-\mu^2) / E)*I$$

Where,





E=600(N+6) (N>15)

(Reference: "Foundation Analysis and Design" by J.E.Bowles)

I = Influence Factor......Reference: Fig.11 IS:8009(Part I)

Further the immediate settlements in cohesionless soil are estimated using the elastic theory considering the effect of a rigid stratum underlying the foundation soils (Reference: "Foundation Analysis and Design" by J.E.Bowles) and for consolidation settlement in cohesive soil the following equation has been used:

 $S_t = \Delta P M_v H$

Where,

 M_v = Coefficient of volume compressibility, cm²/kg

 ΔP = Pressure increment, kg/cm²

H = Thickness of layers

Coefficient of Volume Compressibility derived from SPT N-Value

			1000000000000000000000000000000000000	,	alue: $m_v = 1/(1)$	f2N)
Plasticity Index (%)	Conversion Factor (f ₂)	N=10	N=20	N=30	N=40	N=50
10	800	0.12	0.06	0.04	0.03	0.02
20	525	0.19	0.09	0.06	0.05	0.04
30	475	0.21	0.10	0.07	0.05	0.04
40	450	0.22	0.11	0.07	0.06	0.04

(After Stroud and Butler, 1975)

 $Mv = 1/(f_2 N_{corr.})$

Where $f_2 =$ factor based on N_{corr.} Value & plasticity index of soil

 $N_{corr.} = corrected SPT 'N' value$

For the analysis of foundation the total permissible settlement has been considered as 50mm for open foundation and 75mm for raft foundation.

Zone of influence below foundation has been considered up to 1.5 times the width of the foundation.

Lower of the two values obtained from settlement and shear criteria is used in arriving at allowable bearing capacity of the soil.

Sample calculations for computation of allowable bearing capacity of sub-strata for open foundations resting op and ce attached vide Appendix C-1.

(A) Safe Load Carrying Capacity of Normal Bored Cast In-Situ RCC Pile In Soil Director CEG Test House & Kesearch Centre Vyt., Ltd.

The safe Load Carrying Capacity of normal bored cast in-situ RCC pile is determined in compression, uplift as per IRC: 78-2014 Appendix-5 (Clause 709.3.1) and lateral as per IS: 2911 (Part-1/Sec-2): 2010. The axial capacity of a pile depends upon the soil skin friction along the shaft and end bearing at it's tip.

Thus Axial load = Skin Friction + End-bearing

a) For piles in granular soils (using the static formula)

$$Q_u = (0.5*D*\gamma*N_\gamma + P_D*N_q)*A_p + (\Sigma K_i*P_{Di}*tan\delta_i)*A_{si}$$

Where,

Q_u = Ultimate load capacity of pile in KN

D = Dia. of pile shaft in m

 γ = Effective unit weight of the soil at pile tip in kN/m³

 N_{γ} & N_q = Bearing capacity factors depending upon the angle of internal friction Φ at pile tip

- P_D = Effective overburden pressure at pile tip in kN/m² limited to 15 times diameter of pile
 - Σ = Summation for layers (1 to n) in which pile is installed and which contribute to (+ve) skin friction

 K_i = Coefficient of earth pressure applicable for the ith layer

 P_{Di} = effective overburden pressure for the ith layer in kN/m² limited to 15 times diameter of pile

 δ_i = angle of wall friction between pile and soil for ith layer, and

 A_{si} = surface area of pile shaft in the ith layer in m²

b) For piles in cohesive soils (using the static formula)

$$\mathbf{Q}_{u} = \mathbf{c}\mathbf{p}^{*}\mathbf{N}\mathbf{c}^{*}\mathbf{A}_{p} + \boldsymbol{\Sigma}\boldsymbol{\alpha}_{i}^{*}\mathbf{c}_{i}^{*}\mathbf{A}_{si}$$

Where,

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 $Q_u = Ultimate load capacity of pile in KN$

 $A_p = cross-sectional$ area of pile tip in m^2

 N_c = bearing capacity factor (= 9)

Director

 Σ = Summation for layers (1 to n) in which pile is installed and which contribute to (+ve) skin friction

 α_i = adhesion factor for the i^{th} layer depending on the consistency of soil

 $c_i = average \ cohesion \ for \ i^{th} \ layer \ in \ kN/m^2$

 A_{si} = surface area for pile shaft in the ith layer in m²

c) For computation of lead carrying capacity of pile in lateral, the following equation has been used:



 $Q = (12 * E * I * Y) / (L_1 + L_f)^3$

Where,

Q = Lateral Load (in kg)

Y = Permissible lateral deflection taken as 5mm

E = Modulus of Elasticity of concrete

I = Moment of Inertia of the pile cross-section

 L_1 = Length of pile above cut-off level

 $L_f = Length of fixity$

The effective length of the pile has been considered below the cut-off level taken as 2.0 m below the EGL. Normal Bored cast in-situ RCC piles having stem diameter equal to 1.00 m & 1.20 m. For the analysis of the pile foundations the soil parameters used for computation of safe load carrying capacity of pile is tabulated below:-

Table 3.1: Design Soil Parameter

(M)		Layer depth	Delow EGL (m)	strata	ption		SPT N	gm/cc)	() ()	ernal) (°)
Chainage (KM)	BH Ref.	From	То	Thickness of strata (m)	Strata description	Observed	Corrected	Bulk Density (gm/cc)	Cohesion (C) (kg/cm2)	Angle of internal Friction (Φ) (°)
		0.0	7.0	7.0	Silty Sand	48	51	1.79	0	31
		7.0	10.0	3.0	Silty Sand	65	57	1.80	0	32
		10.0	13.5	3.5	Silty Sand	64	49	1.80	0	32
		13.5	16.5	3.0	Silty Sand	72	50	1.80	0	32
	TNST-01	16.5	21.0	4.5	Silty Sand	96	57	1.82	0	32
	SN	21.0	25.5	4.5	Silty Sand	94	50	1.83	0	32
	E	25.5	30.0	4.5	Silty Sand	98	46	1.84	0	32
ion		30.0	34.5	4.5	Silty Sand	98	44	1.84	0	32
lect		34.5	37.5	3.0	Silty Sand	100	-	1.88	0	33
s pa		37.5	40.0	2.5	Silty Sand	100	-	1.88	0	33
Elevated Section		0.0	7.0	7.0	Silty Sand	24	25	1.71	0	30
Ele		7.0	7.5	0.5	Silty Sand	24	-	1.75	0	31
	02	7.5	13.0	5.5	Silty Sand	50	41	1.80	0	32
	TNST-02	13.0	16.5	3.5	Silty Sand	70	48	1.80	0	32
	NL	16.5	24.0	7.5	Silty Sand	86	50	1.81	0	32
		24.0	28.5	4.5	Silty Sand	99	50	1.83	0	32
		28.8.ai		11.5	Silty Sand	98	44	1.84	0	34
	TN Align ment-	×9.0	7.0	7.0	Silty Sand	27	29	1.74	0	30
	TN Align ment-	37.0		3.0	Silty Sand	43	37	1.79	0	31
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Geo-technical Investigation work for Extension of underground and elevated section E-W Corridor from Badi Chouper to Transport Nagar (2.85Km) Phase-1C and Mansarovar to Ajmer Road (Chauraha) (1.35 km) Phase-1D of Jaipur Metro Rail Corporation at Jaipur

		evaipai						-		
		10.0	13.0	3.0	Silty Sand	56	43	1.81	0	31
		13.0	18.0	5.0	Silty Sand	69	46	1.81	0	32
		18.0	24.0	6.0	Silty Sand	83	47	1.82	0	32
		24.0	28.0	4.0	Silty Sand	95	47	1.82	0	32
		28.0	31.5	3.5	Silty Sand	100	-	1.86	0	34
		31.5	40.0	8.5	Silty Sand	100	-	1.84	0	34
		0.0	7.0	7.0	Silty Sand	48	51	1.79	0	32
		7.0	7.5	0.5	Silty Sand	35	28	1.80	0	32
	t-02	7.5	13.0	5.5	Silty Sand	35	28	1.76	0	31
	nen	13.0	16.5	3.5	Silty Sand	54	37	1.78	0	31
	gnn	16.5	21.0	4.5	Silty Sand	81	43	1.85	0	33
	Ali	21.0	24.0	3.0	Clayey Sand	66	36	1.85	0.11	29
	TN Alignment-02	24.0	31.5	7.5	Silty Sand	93	33	1.86	0	31
	Ľ	31.5	37.5	6.0	Silty Sand	100	-	1.87	0	33
		37.5	40.0	2.5	Silty Sand	100	-	1.87	0	33
		0.0	7.0	7.0	Silty Sand	46	48	1.74	0	31
	33	7.0	10.5	3.5	Silty Sand	65	24	1.77	0	32
	TN Alignment-03	10.5	16.5	6.0	Silty Sand	43	31	1.73	0	31
		16.5	22.5	6.0	Silty Sand	72	43	1.80	0	31
		22.5	27.0	4.5	Silty Sand	97	50	1.85	0	33
		27.0	31.5	4.5	Silty Sand	100	-	1.85	0	33
	IT	31.5	36.0	4.5	Silty Sand	100	-	1.86	0	33
		36.0	40.0	4.0	Silty Sand	100	-	1.93	0.07	31
		0.0	7.0	7.0	Silty Sand	33	36	1.76	0	29
	+	7.0	10.0	3.0	Silty Sand	43	38	1.77	0	30
	TN Alignment-04	10.0	13.0	3.0	Silty Sand	59	45	1.77	0	30
	nen	13.0	16.0	3.0	Silty Sand	55	38	1.78	0	31
	gnr	16.0	19.0	3.0	Silty Sand	65	41	1.80	0	31
	Ali	19.0	24.0	5.0	Silty Sand	78	44	1.80	0	31
	NT	24.0	30.0	6.0	Silty Sand	92	44	1.81	0	31
	-	30.0	34.5	4.5	Silty Sand	100	-	1.84	0	33
		34.5	40.0	5.5	Silty Sand	100	-	1.84	0	33
		0.0	7.0	7.0	Silty Sand	15	16	1.66	0	29
	05	7.0	10.0	3.0	Silty Sand	31	27	1.71	0	29
	TN Alignment-05	10.0	15.0	5.0	Silty Sand	49	37	1.79	0	31
		15.0	21.0	6.0	Silty Sand	61	38	1.79	0	31
		21.0	24.0	3.0	Silty Sand	81	44	1.79	0	32
	ΝA	24.0	28.5	4.5	Clayey Sand	46	23	1.81	0.07	28
	II	28.5	36.0	7.5	Silty Sand	100	-	1.84	0	33
		36.0	40.0	4.0	Silty Sand	100	-	1.85	0	33
		Rai	-00							



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The sample calculation for computation of safe load carrying capacity of normal bored cast-in-situ RCC pile in compression & uplift are attached vide **Appendix C2**.

The sample calculation for computation of safe load carrying capacity of normal bored cast-in-situ RCC pile in lateral are attached vide **Appendix C3**.





ANALYSIS OF FOUNDATION AND RECOMMENDATIONS CHAPTER 4

8.0 FOUNDATION RECOMMENDATIONS

- Based on the nature & strength characteristics of the substrata and requirement of the project, open foundations & pile foundations have been analysed mentioned in below Table 4.1 & 4.2.
- Based on design parameters and sample calculations attached, recommended allowable bearing capacities are tabulated as follows:-

Chainage (km)/Structure	BH [^] No.	Type of Foundation	Depth of Foundation below EGL (m)	Foundation Size (m)	Net Safe Bearing Capacity from Shear Failure (t/m ²)	Allowable Bearing Pressure from settlement failure (t/m ²)	Recommended Allowable Bearing Capacity (t/m ²)
	TN TN TN TN TN TN TN t-03 t-02 t-03		3		29.1	134.3	29.1
	TN gnm t-02		4		34.5	161.6	34.5
	Ali		5	3 x 4	41.1	201.0	41.1
ų	nen	uc	3	3 X 4	28.1	93.6	28.1
ctic	TN ignm t-03	latic	4		40.7	105.1	40.7
l Se	Ali	ound	5	-	46.4	111.0	46.4
Elevated Section	nen	Open Foundation	3		29.7	103.1	29.7
Jeva	TN Ignm t-02	pen	4		35.1	124.7	35.1
Щ	Ali	0	5	4 x 5	41.4	162.6	41.4
	nen		3	4 X J	30.6	66.6	30.6
	TN ignm t-03		4		39.8	71.3	39.8
	Ali		5		43.7	83.7	43.7

Table 4.1 : Recommended Net Allowable Bearing Capacity

Table 4.2: Safe Load Carrying Capacity of normal bored cast in-situ RCC Pile in Soil

			m)	(m) Delow		Safe load carrying capacity (T)		
SI. No.	Structure	BH. No.	Dia of piles (Cut-off level below EGL (m)	Length of piles below cut-off (m)	In compression	In uplift	Lateral
1	Elevated Section ()	TNSF	1	2	24 26	435 472	214 240	66
	131 02	rector			28	509	265	
CEG Test H	ouse & Kescarch		.td. 29 of 12	25				CEGTH TEST HOUSE



SR-837_23-24

Geo-technical Investigation work for Extension of underground and elevated section E-W Corridor from Badi Chouper to Transport Nagar (2.85Km) Phase-1C and Mansarovar to Ajmer Road (Chauraha) (1.35 km) Phase-1D of Jaipur Metro Rail Corporation at Jaipur

1							1
				30	546	290	
				32	583	316	-
				34	621	342	
				24	622	279	
				26	676	316	_
		1.2		28	729	353	107
		1.2		30	783	390	107
				32	836	427	
				34	892	465	
				24	418	207	
				26	454	232	
		1		28	492	258	
		1		30	591	284	51
				32	629	310	
	TNST-		_	34	668	337	-
2	02		2	24	599	270	
				26	651	306	-
		1.2		28	706	344	82
				30	868	382	
				32	924	421	
				32	981	459	-
				24	423	209	
				26	459	234	- 51
				28	560	260	
		1		30	599	287	
				30	638	314	
	TN			32	677	340	-
3	Alignme		- 2	24	606	272	
	nt-01					309	-
				26	659 716		
		1.2		28	716	348	82.5
				30	880	386	
				32	937	425	
				34	994	464	
				24	399	208	-
				26	434	232	-
		1		28	469	257	47
	TN			30	505	281	-
4	Alignme		2	32	594	307	-
	nt-02			34	632	333	
	Rail Cor			24	511	271	-
	en of the second	1.2		26	617	307	- 76
	entre and and a start			28	668	342	
				30	720	378	<u> </u>
CEG Test H	buse & Research Centre Pyt., I	Ltd. 30 of 12	25				CEGTH TEST HOU

SR-837_23-24

Geo-technical Investigation work for Extension of underground and elevated section E-W Corridor from Badi Chouper to Transport Nagar (2.85Km) Phase-1C and Mansarovar to Ajmer Road (Chauraha) (1.35 km) Phase-1D of Jaipur Metro Rail Corporation at Jaipur

							•
				32	866	416	
				34	922	454	
				24	434	202	
				26	470	227	57
		1		28	506	252	
			2	30	543	277	
				32	531	302	
5	TN			34	568	327	
5	Alignme nt-03		2	24	633	265	
	in 05			26	686	302	
		1.2		28	739	338	91
		1.2		30	792	375	
				32	761	411	
				34	814	448	
				24	386	202	
		1	2	26	421	226	- 56
				28	455	250	
				30	543	275	
				32	580	301	
6	TN Alignme			34	618	326	
0	nt-04	1.2		24	547	263	90.5
				26	597	298	
				28	646	333	
				30	700	370	
				32	843	407	
				34	897	444	
			2	24	324	192	- 38
				26	354	214	
		1		28	388	237	
		1		30	514	262	
				32	549	287	
7	TN Alignme			34	585	311	
/	nt-05		2	24	446	252	- 62
				26	489	283	
		1.2		28	539	317	
		1.4		30	749	353	02
				32	801	389	
				34	853	425	

<u>NOTE</u>:-1. Permissible lateral deflection has been taken as 1.0% of Pile dia. at Max. of cut-off level/ liquefaction denth. Director

> CEG TEST HOUSE AND RESEARCH CENTRE PVT. LTD.

CEG Test House & Kessarch Centre Vt. Ltd.

AIPUR

- 2. The self-weight of the pile has been taken into account while computing the Safe Load Carrying Capacity of Pile in uplift only and not considered for vertical load capacity in compression.
- 3. The safe load carrying capacity of piles have been worked out on the basis of IRC 78-2014 as per provisions / assumptions provided therein & are only an assessment based on characteristics of the substrata obtained at the locations of the above BHs. The safe load carrying capacities as tabulated above will further depend substantially on the piling technique adopted and equipment used for making the piles in the field. However, for the final designs & constructions, the safe/allowable load carrying capacities of these piles should be taken by conducting actual initial load tests on these piles by casting them in the respective areas.
- 4. While erecting normal bored cast in-situ pile, utmost care should be taken while flushing/cleaning the bottom of pile particularly prior to start of pouring of concrete so as o rest the pile in virgin soil only for obtaining full point bearing as while computing safe load carrying capacity of pile no bottom softening during erection of pile has been considered.
- 5. Further the pile should have necessary structural strength to transmit / sustain the design load.

All The above recommendations are based on the field and laboratory tests conducted on selected soil/ rock core samples and our experience in this regard. If the actual substrata conditions during excavation for the foundation differ from the observations reported here, the design experts/consultants should be referred for suggestion, further investigations.





Abbreviations

BH	Borehole
EGL	Existing Ground Level
GWT	Ground Water Table
IS	Indian Standards
SPT	Standard Penetration Test
UDS	Un-disturbed Soil
UDS*	UDS not recovered
DS	Disturbed Soil
R.L.	Reduced Level
m	Metre
%	Percentage
mg /l	Milligram per litre
mg /kg	Milligram per kilogram
DST	Direct shear test on UDS sample
DST+	Direct shear test on remoulded sample





APPENDIX – A (FIELD DATA RESULTS)

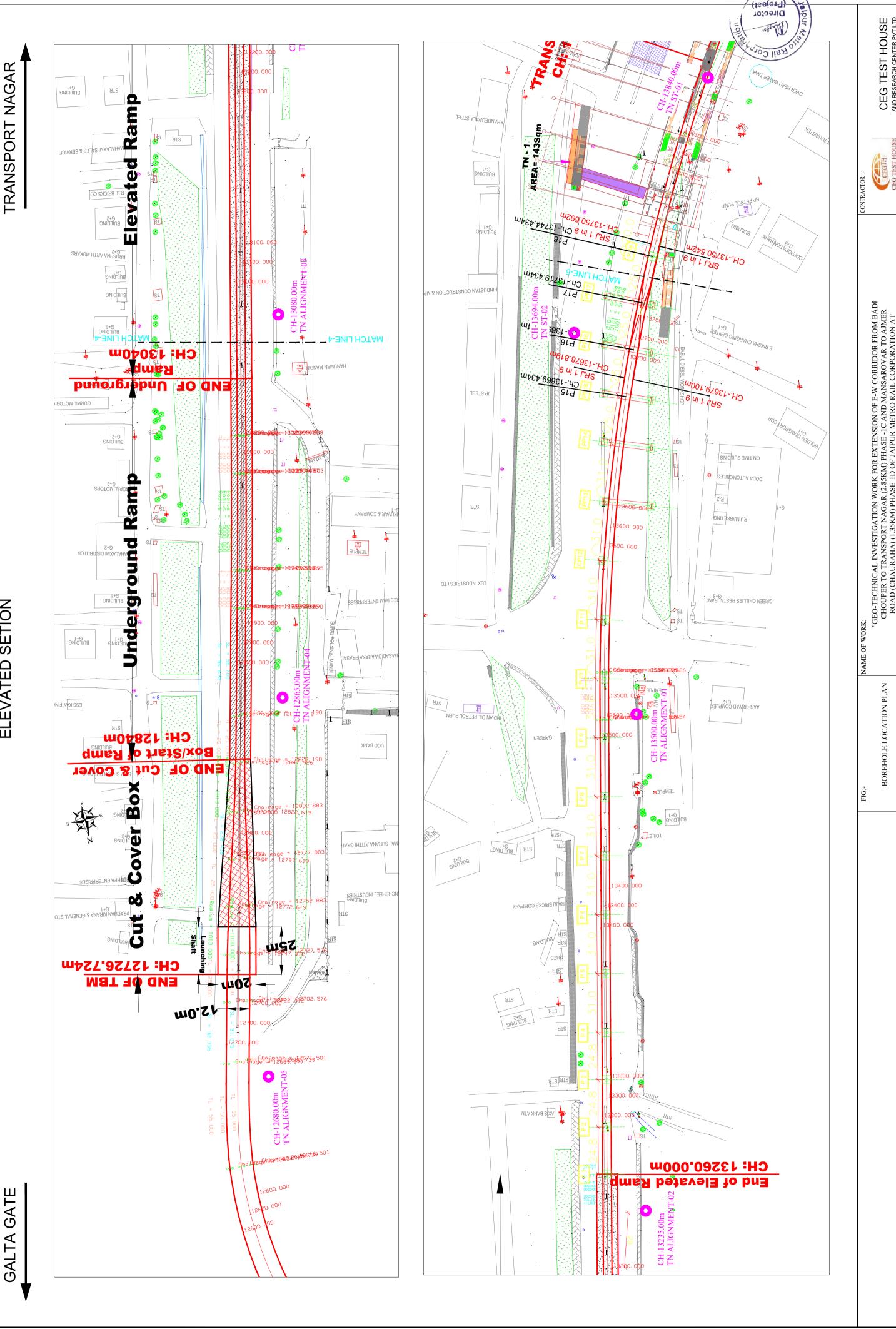
Appendix No.	ITEMS
A-1	LOCATION PLAN
A-2	FIELD BOREHOLE LOG
A-3	FIELD PERMEABILITY TEST RESULTS
A-4	COREBOX PHOTOGRAPH

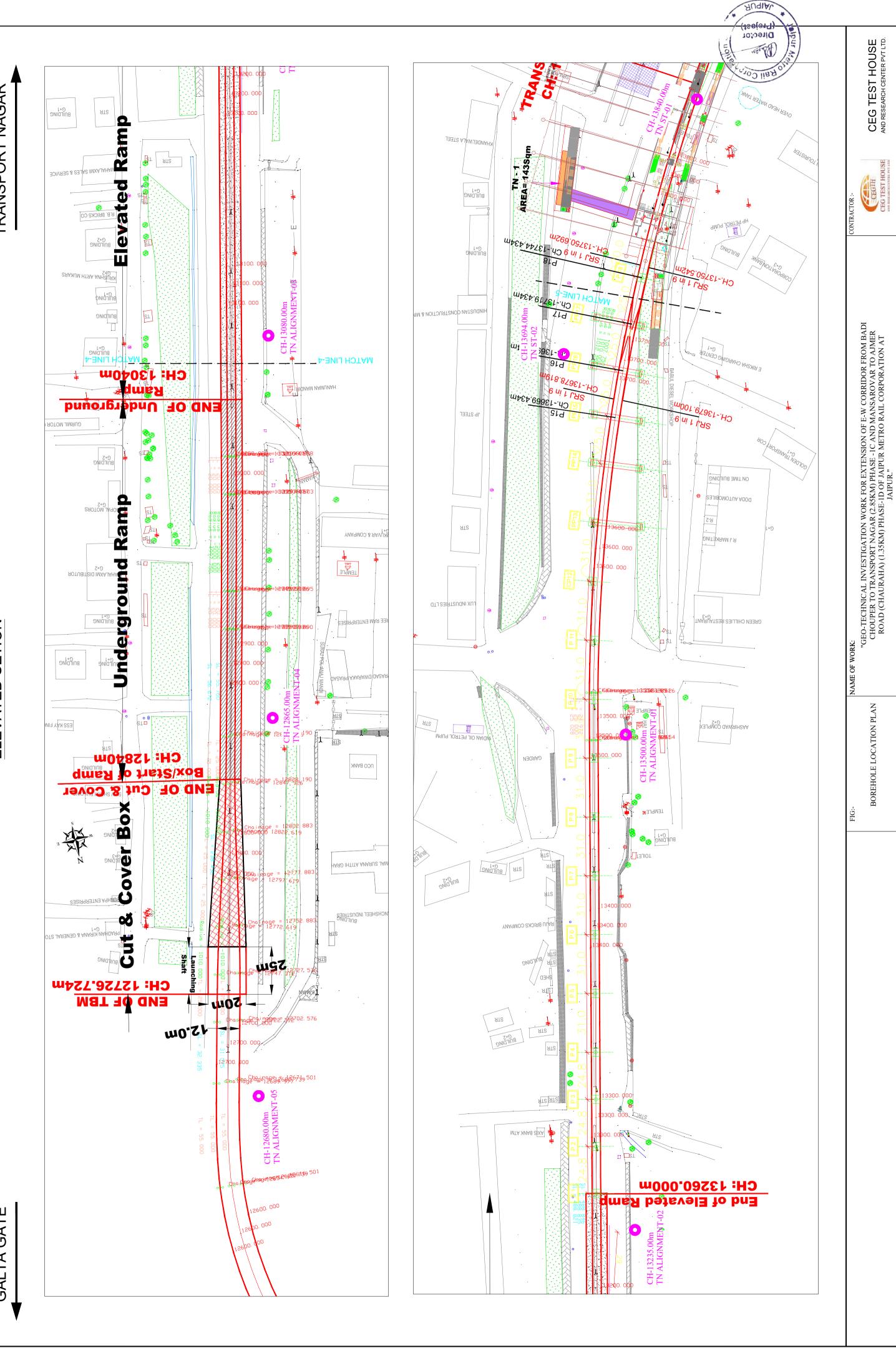












Project Name : Badi Chouper to Transport Nagar and Mansarova					ovar to A	jmer Road of .	JMRC at Jaipur.	Client :JMRCL			
BH Location/Chainage :Transport Nagar Reduced Level (m):(+)469.925				-	thing :297634		Easting :583984 m				
					No. :TNST-01						
	posed/Existing Structure :					Not Encountered	BH Depth (m):40 Inclination : Vertical				
		ell & Aug				of Boring :15		Depth of Casing			
		-04-2023	-				n :26-04-2023		(,		
Depth (m)	Sample & In-SituTest Depth (m)		ерт	Strata Description	IS Classification	Graphic Log	Core Recovery (%)	RQD (%)	SPT N value)	Special Observation	
_0.0		DS			U) 2,5 5,0 7,51000	2 ₅ 5507 <u>5</u> 100	0 10 20 30 40 50 60 70 80 9000		
0.5								-			
_1.5				Filled up soil	FILL			-			
_2.0											
_2.53.0	3	SPT-1	31								
_3.5								-			
_4.0	4	UDS-1						-			
_4.5	4.5	SPT-2	40					-			
_5.0								-			
_5.5	6	SPT-3	74								
_6.5				Dense to very dense, brownish, silty sand	SM						
_7.0	7	UDS-2									
_7.5	7.5	SPT-4	71								
_8.0											
_8.5	9	SPT-5	59	Director (Project)	220						
9.5	-			Director	in the			-			

CEG	THE ST HOUSE			FIELL) <i>B</i> (OREE	IOLE LO	G					
Project Name : Badi Chouper to Transport Nagar and Mansarov					ovar to Aj	mer Road of	JMRC at Jaipur.	Client : JMRCL					
BH Location/Chainage : Transport Nagar					Nort	hing :297634	9 m	<i>Easting</i> :583984 m					
Reduced Level (m):(+)469.925					No. :TNST-0		BH Depth (m):40						
Proposed/Existing Structure :					Not Encountered	Inclination : Vertical							
		ell & Aug				of Boring :1:		Depth of Casing	(m) :Not Used				
Date of	Start :21	-04-2023	3		Date	of Completio	n :26-04-2023						
Depth (m) _10.0_	Sample & In-SituTest Depth (m)	Sample Type	SPT N Value	Strata Description	IS Classification	Graphic Log	Core Recovery (%) 0 25 50 7,5100 0	RQD (%) 25 50 75100	(Depth v/s SPT N Value) 010 20 30 40 50 60 70 80 9000	Special Observations			
10.0													
10.5	10.5	SPT-6	62										
11.0													
11.5													
12.0	12	SPT-7	66										
12.5													
13.0	13	UDS*											
13.5	13.5	SPT-8	72										
14.0													
14.5													
15.0	15	SPT-9	71	Dense to very dense, brownish, silty sand	SM								
15.5													
16.0	16	UDS*											
16.5	16.5	SPT-10	89						+++++++++++++++++++++++++++++++++++++++				
17.0													
17.5													
18.0	18	SPT-11	100							•			
18.5				Rail Cor									
19.0	19	UDS*		and the second	nome								
19.5	19.5	SPT-12	98	Director (Project)									
20.0				JAIPUR	*/	37 of 1	25						

BH Location/Cha Reduced Level (m) Proposed/Existing Boring type :Shell Date of Start :21- Depth (m) of start :21- 20.0 21 _20.5 21 _21.5 22 _22.0 22 _22.5 22.5 _23.0 24 _24.5 24	ainage :T n):(+)469 g Structu II & Aug -04-2023 Sample	Transport 0.925 <i>ure :</i> er	t Nagar t Nagar Strata Description	North BH. N Wate Dia.	hing :297634 No. :TNST-0 r Table (m):1 of Boring :1: of Completio Graphic Log	19 m 1 Not Encountered	Client :JMRCL Easting :583984 BH Depth (m):40 Inclination : Vert Depth of Casing	tical (m) :Not Used (Depth	Special Observations
Reduced Level (m Proposed/Existing Boring type : Shel Date of Start : 21- Depth (m) * end to f to	n):(+)469 g Structu II & Aug -04-2023 Sample Type SPT-13 UDS*	9.925 are : er SPT N Value 95	Strata	BH. N Wate Dia. Date	No. :TNST-0 r Table (m):1 of Boring :1: of Completio Graphic Log	1 Not Encountered 51 mm on :26-04-2023 Core Recovery (%)	BH Depth (m):40 Inclination : Vert Depth of Casing RQD (%)	tical (m) :Not Used (Depth v/s SPT N Value)	Special Observations
Reduced Level (m Proposed/Existing Boring type : Shel Date of Start : 21- Depth (m) * end to f to	n):(+)469 g Structu II & Aug -04-2023 Sample Type SPT-13 UDS*	9.925 are : er SPT N Value 95	Strata	BH. N Wate Dia. Date	No. :TNST-0 r Table (m):1 of Boring :1: of Completio Graphic Log	1 Not Encountered 51 mm on :26-04-2023 Core Recovery (%)	BH Depth (m):40 Inclination : Vert Depth of Casing RQD (%)	tical (m) :Not Used (Depth v/s SPT N Value)	Special Observations
Boring type : Shel Date of Start : 21- Depth (m) of all start : 21- _20.0 20.5 _21.0 21 _22.0 22 _22.0 22 _22.0 22 _22.0 22 _22.0 22.5 _23.0 24 _24.0 24	II & Aug -04-2023 Sample Type SPT-13 UDS*	95		Dia. Date	of Boring : 15 of Completio Graphic Log	51 mm on :26-04-2023 Core Recovery (%)	Inclination : Vert Depth of Casing RQD (%)	tical (m) :Not Used (Depth v/s SPT N Value)	Special Observations
Date of Start :21- Depth (m) Start :21- _20.0 20.5 _21.0 21 _21.5 22 _22.0 22 _22.5 22.5 _22.5 22.5 _23.0 24 _24.0 24	-04-2023 Sample Type	SPT N Value		Date	of Completio Graphic Log	Core Recovery (%)	RQD (%)	(Depth v/s SPT N Value)	Special Observations
Depth (m) of all bit of all bit all bit of all bit all bit all bit of all bit all bit all bit of all bit all bit all bit of all bit of all bit of all bit of all bit of all bit of all bit of all bit of all bit all bit of all bit all bit of all bit all bit all bit of all bit of all bit of all bit of all bit of all bit of all bit of all bit all bit of all bit bit of all bit of all bit bit bit of all bit bit of	Sample Type SPT-13 UDS*	SPT N Value			Graphic Log	Core Recovery (%)	(%)	v/s SPT N Value)	Special Observations
20.0 _20.5_ _21.0_ 21 \$ _21.5_ _22.0_ 22 _22.5_ 22.5 \$ _23.0_ _23.5_ _23.5_ _24.0_ 24 \$ _24.5_	Type SPT-13 UDS*	N Value 95		IS Classification	Log	Recovery (%)	(%)	v/s SPT N Value)	Special Observations
20.5 _21.0_ 21 \$ _21.5_ _22.0_ 22 _22.5_ 22.5 \$ _23.0_ _23.5_ _24.0_ 24 \$ _24.5_	UDS*								
21.0 21 \$ _21.5_ _22.0_ 22 _22.5_ 22.5 \$ _23.0_ _23.5_ _24.0_ 24 \$ _24.5_	UDS*							• • • •	
21.5 _22.0_ 22 _22.5_ 22.5 \$ _23.0_ _23.5_ _24.0_ 24 \$ _24.5_	UDS*							•	
22.0 22 _22.5_ 22.5 \$ _23.0_ _23.5_ _24.0_ 24 \$ _24.5_		98						╶┼┼┼┼┼┼┼╢	
22.5 22.5 \$ _23.0_ _23.5_ _24.0_ 24 \$ _24.5_		98							
23.0 _23.5_ _24.0_ 24 \$ _24.5_	SPT-14	98			- 영화 문화 문화		-		
23.5 _24.0_ 24 5 _24.5_			1						
24.0 24 \$ _24.5_							-		
24.0 24 \$ _24.5_									
24.5	SPT-15	90							
	SF 1-15	90							
25.0 25									
	UDS*		Dense to very dense, brownish, silty sand	SM					
25.5 25.5	SPT-16	98							
26.0									
26.5									
27.0 27 \$	SPT-17	96					·	+	
27.5									
28.0 28	UDS*								
28.5 28.5	SPT-18	99							•
29.0			Rail Cor	2271211			·		
29.5			Director (Project						
_30.030\$	SPT-19	_95	JAIPUR	*/	38 of 12	25			

FIELD .	BOREH	OLE LO	G		
Project Name :Badi Chouper to Transport Nagar and Mansarovat	r to Ajmer Road of JN	MRC at Jaipur.	Client : JMRCL		
BH Location/Chainage : Transport Nagar	Northing :2976349	m	Easting :583984	m	
Reduced Level (m):(+)469.925	BH. No. :TNST-01		BH Depth (m):40)	
Proposed/Existing Structure :	Water Table (m):No	ot Encountered	Inclination : Vert	tical	
Boring type : Shell & Auger	Dia. of Boring :151	mm	Depth of Casing	(m) :Not Used	
Date of Start :21-04-2023	Date of Completion	:26-04-2023			
Depth (m)a to find a to f	Graphic Log	Core Recovery (%) 25 50 7,5100 0	RQD (%) 25 50 75100	(Depth v/s SPT N Value) ० 19 29 39 49 59 69 79 89 5900	Special Observations
				•	
30.5 31.0 31 UDS*	БМ				
31.5 31.5 SPT-20 100					•
32.0					
32.5					
33.0 33 SPT-21 100					•
33.5					
34.0 34 UDS*					
34.5 34.5 SPT-22 100					•
35.0					
35.5					
36.0 36 SPT-23 100 Very dense, brownish, silty sand	SM				•
36.5					
37.0 37 UDS*					
37.5 37.5 SPT-24 100					•
38.0					
38.5					
39.0 39 SPT-25 100					•
39.5 Director (Project)					
	39 of 125				

Car	atti st nousi			FIELL	BC	OREH	IOLE LC	\overline{OG}		
Project	Name :B	adi Cho	uper to T	ransport Nagar and Mansar	ovar to A	jmer Road of	JMRC at Jaipur.	Client :JMRCL		
BH Loc	ation/Ch	ainage :]	Near red	light police booth	Nort	hing :297667	0 m	Easting :584086	m	
	d Level (i			6 1		No. :TN Aligr		BH Depth (m):40		
	ed/Existir						Not Encountered	Inclination : Vert		
	<i>type</i> :She					of Boring :15		Depth of Casing	(m) :Not Used	
Date of	Start :25	-04-202	3			of Completio	n :02-05-2023			
Depth (m)	Sample & In-SituTest Depth (m)	Sample Type	SPT N Value	Strata Description	IS Classification	Graphic Log	Core Recovery (%) 0 25 50 751000	RQD (%) 2,5 5,0 7,5100	(Depth v/s SPT N Value) 010 20 30 40 50 60 70 80 5000	Special Observations
0.0		DS								
0.5 1.0	-									
1.5	-			Filled up soil	FILL					
2.0										
2.5										
2.5	-									
3.0	3	SPT-1	18							
3.5	-									
4.0	4	UDS-1								
4.5	4.5	SPT-2	29							
5.0	-									
5.5										
6.0	6	SPT-3	35							
6.5	-			Dense, brownish, Silty sand	SM					
7.0	7	UDS-2								
7.5	7.5	SPT-4	38					·		
8.0										
8.5	-									
9.0	9	SPT-5	47	Rail Cor	2nration					
9.5				Director (Project)	171					
10.0	10	UDS-3		VAIPUR	*/	40 of 12	5			

CHO THE	HU ST HOUSE			FIELL	$\mathcal{D}B$	OREE	IOLE LC	G		
Project	Name :E	adi Chou	uper to T	ransport Nagar and Mansar	rovar to	Ajmer Road of	JMRC at Jaipur.	Client :JMRCL		
BH Loca	ation/Ch	ainage :1	Near red	light police booth	No	rthing :297667	70 m	Easting :584086	m	
		n):(+)46				. No. :TN Alig		BH Depth (m):40		
		ng Structi					Not Encountered	Inclination : Vert		
		ell & Aug				a. of Boring :1		Depth of Casing	(m) :Not Used	
Date of	Start :25	-04-2023	3		Da	te of Completic	on :02-05-2023			
Depth (m) _10.0_	Sample & In-SituTest Depth (m)	Sample Type	SPT N Value	Strata Description	IS Classification	Graphic Log	Core Recovery (%) 0 25 50 75100	RQD (%) 0 25 50 75100	(Depth V/s SPT N Value)	Special Observation:
10.0										
10.5 11.0	10.5	SPT-6	55						+ + + + + + + + + + + + + + + + + + + +	
11.0										
11.5										
12.0	12	SPT-7	57							4
12.5										-
13.0	13	UDS-4								-
13.5	13.5	SPT-8	63							-
14.0										
_ 14.0_										
14.5										
15.0	15	SPT-9	68	Dense, brownish, Silty	SM					-
				sand						
15.5										-
16.0	16	UDS*								-
16.5	16.5	SPT-10	75						<u> </u>	-
17.0										-
17.5										
18.0	18	SPT-11	76							
18.5										1
				Director (Project)	2					
19.0	19	UDS*			je:				+++++++++++++++++++++++++++++++++++++++	
				E (Daren	- jei					
19.5	19.5	SPT-12	80	Director					┼┼┼┼┼╋┼	
				(Project)	1.	그는 것 같은 것 같				
20.0		ecovere		JAIPUR		41 of 1	25			

Proiect	Name :F	adi Chou	per to T	ransport Nagar and Mansaro	var to A	imer Road of	JMRC at Jaipur.	Client :JMRCL		
-			-	light police booth		thing :297667	_	<i>Easting</i> :584086	m	
		m):(+)46		nght police booth		No. :TN Alig		BH Depth (m):40		
		ng Structi					Not Encountered	Inclination : Vert	ical	
		ell & Aug				of Boring :1		Depth of Casing		
		-04-2023					on :02-05-2023	Depin of Cusing	(<i>m</i>) . Not Osca	
Duie of			,			of complete				
Depth (m) _20.0_	Sample & In-SituTest Depth (m)	Sample Type	SPT N Value	Strata Description	IS Classification	Graphic Log	Core Recovery (%) 0 25 50 75100 (RQD (%) 25 50 75100	(Depth v/s SPT N Value) 0 10 20 30 40 50 60 70 80 9000	Special Observation
20.0										
20.5								-		
21.0	21	SPT-13	88					-		-
21.5								-		-
22.0	22	UDS*						-		
22.5	22.5	SPT-14	89					-	+++++++++++++++++++++++++++++++++++++++	-
23.0								-		-
23.5								-		-
24.0	24	SPT-15	92	Dense, brownish, Silty sand	SM			-	++++++	-
24.5										-
25.0	25	UDS*						-		-
25.5	25.5	SPT-16	96					-		-
26.0								-		-
26.5								-		-
27.0	27	SPT-17	97					-		
27.5								-		
28.0	28	UDS*						-		
28.5	28.5	SPT-18						-	<u> </u>	ł
29.0				Hard, brownish, Clayey silt with inw posticity	N.S.			-		-
29.5				Director (Project)				-		
			100		*/	42 of 1				

Project	Name :B	adi Choi	uper to T	ransport Nagar and Mansaro	var to Aj	mer Road of	JMRC at Jaipur.	Client :JMRCL						
				light police booth		hing :297667		Easting :584086	m					
	l Level (1			light police booti		No. :TN Alig		BH Depth (m):40						
	d/Existin						Not Encountered	Inclination : Ver		[
	<i>type</i> :She					of Boring :1:		Depth of Casing			ot U	Jsed		
	Start :25						n :02-05-2023	1 7 8	()					
Depth (m)	Sample & In-SituTest Depth (m)	Sample Type	SPT N Value	Strata Description	IS Classification	Graphic Log	Core Recovery (%) 0 25 50 75100	RQD (%) 0 25 50 75100		SPT	v/ 「 N	Val	ue)	Special Observatior
30.0	30.02	RC-1							010.		-10 3.		0.00.3	
_30.5														
_31.0	04.5	50.0												
_31.5	31.5	RC-2					66	J		\parallel				H
_32.0														
32.5														
_33.0	33	RC-3					3)						
33.5														
_34.0														
_34.5	34.5	RC-4					5.33)						
_35.0				Highly weathered, very poor, brownish, medium G grained Quartzite	RADE-V									
_35.5				granied Quarzite										
_36.0	36	RC-5					7.33)						
_36.5														
_37.0														
_37.5	37.5	RC-6					10.33)						
_38.0														
_38.5				a sil Col										
_39.0	39	RC-7		Director (Project)	otter		10 8	3.66						
_39.5				Director (Project)	171									
40.0_	40				*/	43 of 1								

Ducient	Nama i D	adi Cha	mor to T	ransport Nagar and Mansarc	wanto A	mar Dood of	N/DC at Jaimum	Client :JMRCL		
					1					
				of Khandelwal stoel shop		hing :297646		Easting :584079		
		n):(+)46				No. :TNST-02		BH Depth (m):40		
		ng Struct					Not Encountered	Inclination : Vert		
		ell & Aug				of Boring :15		Depth of Casing	(m) :Not Used	
		-04-2023	3			of Completio	n :03-05-2023			
Depth (m)	Sample & In-SituTest Depth (m)	Sample Type	SPT N Value	Strata Description	IS Classification	Graphic Log	Core Recovery (%) D 25 50 7,5100 (RQD (%) 2,5 5,0 7,5100	(Depth v/s SPT N Value) ٥ 1ρ 2ρ 3ρ 4ρ 5ρ 6ρ 7ρ 8ρ 3600	Special Observation
0.0		DS								
0.5										
1.0				Filled up es il	511					
2.0				Filled up soil	FILL					
2.5										
3.0	3	SPT-1	16						$- \mathbf{e} + \mathbf{e} $	
3.5										
4.0	4	UDS-1								
4.5	4.5	SPT-2	26							
5.0				Medium dense, brownish, Silty sand	SM					
5.5	6	SPT-3	30							
6.5	U									
7.0	7	UDS-2								
7.5	7.5	SPT-4	41							
_8.0										
_8.5				Dense, brownish Sov	SM					
9.0 9.5	9	SPT-5	54	Director (Project)	nailon.					
				(Project)	1.					

Clus	THE ST HOUSE			FIELI	OBC	OREI	HOLE LO	\overline{OG}		
Project	Name :B	adi Chou	uper to T	ransport Nagar and Mansar	rovar to A	jmer Road o	f JMRC at Jaipur.	Client : JMRCL		
BH Loca	ation/Ch	ainage :]	In front o	of Khandelwal stoel shop	Nort	hing :29764	67 m	Easting :584079	m	
Reduced	l Level (i	n):(+)46	9.254			No. :TNST-		BH Depth (m):40		
Propose	d/Existir	ng Struct	ure :		Wate	er Table (m)	Not Encountered	Inclination : Vert		
Boring t	ype :She	ell & Aug	ger		Dia.	of Boring :	150 mm	Depth of Casing	(m) :Not Used	
Date of L	Start :28	-04-2023	3			of Complet	ion :03-05-2023			
Depth (m)	Sample & In-SituTest Depth (m)	Sample Type	SPT N Value	Strata Description	IS Classification	Graphic Log	Core Recovery (%) 0 25 50 7,5100	RQD (%) 0 25 50 75100	(Depth V/s SPT N Value) 0 10 20 30 40 50 60 70 80 9000	Special Observations
_ 10.0_										
10.5 11.0	10.5	SPT-6	53							-
11.0							· · ·	·		
11.5										
12.0	12	SPT-7	52				· · ·			
12.5										-
13.0	13	UDS-4					- - - -			
_ 10.0_	10	0201		Dense, brownish, Silty	SM					
13.5	13.5	SPT-8	68	sand			· · ·			-
							· · ·			
14.0							- - - -			
14.5										4
15.0	15	SPT-9	72							-
1E E							- - - -			
15.5										
16.0	16	UDS*					- - -			
							- - -			
16.5	16.5	SPT-10	79						┼┼┼┼┼╋┼	-
17.0										_
17.5										
18.0	18	SPT-11	82						┼┼┼┼┼╋┼	
10 5				Very dense, brownish, Silty sand	SM					
18.5				anil Ca						
19.0	19	UDS*		Palien	22.02					-
19.5	19.5	SPT-12	87	Director (Project)						
20.0				VAIPUR	*/	45 of 1	25			

D	st nouse	L Class					IOLE LC			
-			-	ransport Nagar and Mansarc	-			Client :JMRCL		
		0		of Khandelwal stoel shop		hing :297646		Easting :584079		
		n):(+)46				No. :TNST-02		BH Depth (m):40		
		ng Struct					Not Encountered	Inclination : Vert		
		ell & Aug				of Boring :15		Depth of Casing	(m) :Not Used	
Date of	Start :28	-04-2023	3			of Completio	n :03-05-2023			1
Depth (m) _20.0_	Sample & In-SituTest Depth (m)	Sample Type	SPT N Value	Strata Description	IS Classification	Graphic Log	Core Recovery (%) 0 25 50 75100 0	RQD (%) 25 50 75100	(Depth v/s SPT N Value) 0 10 20 30 40 50 60 70 80 900	Special Observatior
20.5	21	SPT-13	92							
21.5										
22.0	22	UDS*						ŀ		_
22.5	22.5	SPT-14	89							-
23.0								-		-
23.5				Very dense, brownish,	SM			-		
	~	007.45	~~	Silty sand						
24.0	24	SPT-15	98							•
24.5										
24.0										
25.0	25	UDS*								
	20	020						-		
25.5	25.5	SPT-16	99							
26.0										_
26.5								·	+++++++++++++++++++++++++++++++++++++++	-
27.0		SPT-17	100					·	+++++++++++++++++++++++++++++++++++++++	+
	27.23	RC-1								
27.5										-
0 0 -						\searrow				
28.0										1
28.5	28.5	RC-2		Highly to completely			I.33 0			
20.3	20.0	110-2		weathered, whitish to brownish, meaning grain staticor	RADE-V	1 1	r.00 U			1
29.0				grain Sands or Quartzite	2					
				He Maren	ration					
29.5				Director	171					
				(Project)	/ .					
30.0	20	_RC-3_			*/	46 of 1	0			

Project	Name :B	adi Chou	per to T	ransport Nagar and Mansar	ovar to A	mer Road of	JMRC at Jaipur.	Client : JMRCL					
-			-	f Khandelwal stoel shop	-	hing :297646		Easting :584079 :	m				
	l Level (1	0		in Khanderwar stoer snop		No. :TNST-02		BH Depth (m):40					
	d/Existin						Not Encountered	Inclination : Vert					
	<i>type</i> :She	-				of Boring :15		Depth of Casing		Not	Llee	d	
	Start :28	-					n :03-05-2023	Depin of Casing	(m).	ΙΝΟΙ	Use	20	
Dule of			5				n .03-03-2023						<u> </u>
Depth (m) 30.0	Sample & In-SituTest Depth (m)	Sample Type	SPT N Value	Strata Description	IS Classification	Graphic Log	Core Recovery (%) 0 25 50 7,5100	RQD (%) 0 25 50 75100		PTN		alue	Special Observation
30.5 _31.0_				Highly to completely weathered, whitish to brownish, medium grained Sandstone/Quartzite	GRADE-V			-					-
31.5	31.5	RC-4					3.66	0					_
32.0													
32.5													
33.0	33	RC-5					1.66	0					
33.5				Highly to completely weathered, whitish to				-					-
34.0				brownish, medium grained Sandstone/Quartzite	GRADE-IN			-					-
34.5	34.5	RC-6					20	18.66					-
35.0								-					_
35.5								-					-
36.0	36	RC-7					0.66	0					-
36.5					GRADE-V			-					
37.0				grained Sandstone/Quartzite									-
37.5	37.5	RC-8		Highly to completely weathered, whitish to brownish, medium	GRADE-IN	\sim	5.33	0					-
38.0	38			grained Sandstone/Quartzite			6	0					-
38.5				Rail Cor				-		+			-
39.0				Rail Co	noiter								-
39.5				Director (Project)				-					_

Project	Name :B	adi Chou	uper to Tr	ransport Nagar and Mansard	ovar to Aj	mer Road of	JMRC at Jaipur.	Client :JMRCL		
			Near Jain			hing :297748		Easting :584247	m	
		n):(+)46				No. :TN Aligr		BH Depth (m):40		
		ng Struct					lot Encountered	Inclination : Vert		
		ell & Aug				of Boring :15		Depth of Casing		
		-05-2023					n :12-05-2023			
Depth (m)	m) est		PDT	Strata Description	IS Classification	Graphic Log	Core Recovery (%) 0 25 50 75100 0	RQD (%) 25 50 75100	(Depth v/s SPT N Value) o 1p 2p 3p 4p 5p ep 7p ep spoo	Special Observatio
_0.0		DS						20 00 70100		
0.5 1.0										
_1.5				Filled up soil	FILL					
_2.0										
_2.03.0	3	SPT-1	8						•	
_3.5										
_4.0	4	UDS-1								
_4.5	4.5	SPT-2	16						-++	
_5.0 _5.5										
6.0	6	SPT-3	20							
_6.5				Medium dense, brownish, Silty sand	SM					
_7.0	7	UDS-2								
_7.5	7.5	SPT-4	28							
_8.0										
_9.0	9	SPT-5	33	Director (Project)	21011					
_9.5				Director (Project)						

CHG TE	ITH ST HOUSE			FIELL) B(JKEE	<i>HOLE LO</i>	G		
Project .	Name :B	adi Chou	uper to T	ransport Nagar and Mansard	ovar to Aj	mer Road of	JMRC at Jaipur.	Client : JMRCL		
BH Loca	ation/Ch	ainage :1	Near Jair	n temple	North	hing :297748	33 m	Easting :584247	m	
		n):(+)46		-		No. :TN Alig		BH Depth (m):40	1	
Propose	d/Existir	ng Structi	ure :				Not Encountered	Inclination : Vert		
		- ll & Aug			Dia.	of Boring :1:	50 mm	Depth of Casing	(m) :Not Used	
Date of	Start :11	-05-2023	3		Date	of Completio	on :12-05-2023			
Depth (m)	Sample & In-SituTest Depth (m)	Sample Type	SPT N Value	Strata Description	IS Classification	Graphic Log	Core Recovery (%) 0 25 50 7,5100 0	RQD (%) 25 50 75100	(Depth v/s SPT N Value) 0 10 20 30 40 50 60 70 80 9000	Special Observation
10.0				Medium dense,	SM					
10.5	10.5	SPT-6	44	brownish, Silty sand	5101					
11.0										
11.5										
12.0	12	SPT-7	54							
12.5										
13.0	13	UDS*								
13.5	13.5	SPT-8	48						+ +	
14.0										
14.5										
15.0	15	SPT-9	52	Dense, brownish, Silty						
15.5				sand	SM			-		
16.0	16	UDS*								
16.5	16.5	SPT-10	56							
17.0										
17.5										
18.0	18	SPT-11	64							
18.5								·		
19.0	19	UDS*		AND RAIL CON	ratil			·		
19.5	19.5	SPT-12	73	Director (Project)				·		
20.0					*/	49 of 10	-			

CUS	TH FT HOUSE			FIELI	D B c	OREF	IOLE LC	\overline{OG}		
Project	Name :B	adi Chou	uper to T	ransport Nagar and Mansa	arovar to A	jmer Road of	JMRC at Jaipur.	Client :JMRCL		
BH Loca	tion/Ch	ainage :1	Near Jair	n temple	Nor	thing :297748	33 m	Easting :584247	m	
		n):(+)46		-		No. :TN Alig		BH Depth (m):40		
Propose	d/Existir	ig Structi	ure :				Not Encountered	Inclination : Vert		
Boring t	ype :She	ell & Aug	ger		Dia	. of Boring :1:	50 mm	Depth of Casing	(m) :Not Used	
Date of L	Start :11	-05-2023	3			e of Completic	on :12-05-2023			
Depth (m)	Sample & In-SituTest Depth (m)	Sample Type	SPT N Value	Strata Description	IS Classification	Graphic Log	Core Recovery (%) 0 25 50 7,5100 (RQD (%) 0 2,5 5,0 7,5100	(Depth V/s SPT N Value) 0 10 20 30 40 50 60 70 80 9000	Special Observations
20.0										
20.5 _21.0_	21	SPT-13	77							
21.5										-
22.0	22	UDS*		Dense, brownish, Silty sand	SM					-
22.5	22.5	SPT-14	84						_	
23.0										
23.5 _24.0_	24	SPT-15	30							
24.5	27		00							-
25.0	25	UDS*								-
25.5	25.5	SPT-16	46							
26.0										
26.5				Medium dense to dense, brownish, Clayey sand	SC					
27.0	27	SPT-17	93							-
27.5										
28.0	28	UDS*								
28.5	28.5	SPT-18	100	Rail Col						
29.0				Verydense, plownen Sity sand	27781108					
29.5				Directo (Project						
30.0		SPT-19		JAIPUR	<u> </u>	50 of 1	25			<u> </u>

CER	THE CT HOUSE			FIELD) B(JREE	<i>HOLE LC</i>	<i>JG</i>		
Project	Name :E	Badi Chou	uper to T	ransport Nagar and Mansaro	ovar to Aj	mer Road of	JMRC at Jaipur.	Client :JMRCL		
BH Loca	ation/Ch	ainage :]	Near Jair	n temple	North	hing :297748	33 m	Easting :584247	m	
Reducea	l Level (i	<i>m):</i> (+)46	4.947		BH. 1	No. :TN Aligi	nment-05	BH Depth (m):40		
Propose	d/Existir	ng Struct	ure :		Wate	r Table (m):1	Not Encountered	Inclination : Vert	ical	
Boring t	ype :She	ell & Aug	ger		Dia.	of Boring :15	50 mm	Depth of Casing	(m) :Not Used	
Date of L	Start :11	-05-2023	3		Date	of Completio	on :12-05-2023			
Depth (m) 30.0	Sample & In-SituTest Depth (m)	Sample Type	SPT N Value	Strata Description	IS Classification	Graphic Log	Core Recovery (%) 0 25 50 7,5100 (RQD (%) 0 2,5 5,0 7,5100	(Depth v/s SPT N Value) ٥ 1ρ 2p 3p 4p 5p 6p 7p 8p 5pc0	Special Observations
00.0										
30.5	24									
31.0	31	UDS*								
31.5	31.5	SPT-20	100							
32.0										
32.5										
33.0	33	SPT-21	100							•
33.5										
34.0	34	UDS*						-		
34.5	34.5	SPT-22	100					-		•
35.0				Very dense, brownish, Silty sand	SM					
35.5								-		
36.0	36	SPT-23	100							•
36.5								·		
37.0	37	UDS*								
37.5	37.5	SPT-24	100					·		•
38.0										
38.5										
39.0	39	SPT-25	100	ello Rail Coro	ratio					
39.5				Director (Project)						
		SPT-26		(Project)	*1	51 of 10	-			

Project	Name :B	adi Chou	uper to T	ransport Nagar and Mansa	rovar to A	mer Road of	JMRC at Jaipur.	Client : JMRCL		
				ffic police chauki (RAC he				Easting :584132	m	
	d Level (1			ine ponee enwan (rure n		No. :TN Aligi		BH Depth (m):40		
	ed/Existin						Not Encountered	Inclination : Vert		
	<i>type</i> :She					of Boring :15		Depth of Casing		
_	Start :05		-				n :09-05-2023			
Depth (m)	m) est	Sample Type	ерт	Strata Description	IS Classification	Graphic Log	Core Recovery (%)	RQD (%)	(Depth v/s SPT N Value)	Special Observation
0.0		DS			0		0 2,5 5,0 7,5100	0 2,5 5,0 7,5100	0 10 20 30 40 50 60 70 80 9000	
0.5 1.0 1.5 2.0				Filled up soil	FILL					
_2.5										
3.0 3.5	3 3.02	SPT-1 RC-1	100	Highly to completely weathered, whitish to brownish, medium / grained Sandstone/Quartzite	GRADE-V					•
4.0 4.5	4.5	RC-2		Highly to completely weathered, whitish to brownish, medium grained Sandstone/Quartzite	GRADE-V).75 ()		
5.0 5.5										
6.0	6	WS-1		Highly to completely			3.66 () .		
7.0				weathered, whitish to	GRADE-V					
7.5 8.0	7.5	SPT-2	30							
8.5 9.0 9.5	9	SPT-3	35	Medium dense to dense, brownentismo sender Director (Project	nation					

CERT	THI ST HOUSE			FIELI	DÌ	BC	DREF	<i>HOLE LO</i>	OG		
Project	<i>Name</i> :E	Badi Cho	uper to T	ransport Nagar and Mansa	rovar	to Ajı	ner Road of	JMRC at Jaipur.	Client : JMRCL		
BH Loce	ation/Ch	ainage :]	Near Tra	ffic police chauki (RAC he	eadqua	North	ing :297692	27 m	Easting :584132	m	
Reduced	l Level (i	m):(+)46	3.950]	BH. N	lo. :TN Alig	nment-02	BH Depth (m):40)	
Propose	d/Existir	ng Struct	ure :			Water	r Table (m):	Not Encountered	Inclination : Ver	tical	
Boring	<i>type</i> :She	ell & Aug	ger			Dia. o	of Boring :1	50 mm	Depth of Casing	(m) :Not Used	
Date of	Start :05	5-05-202	3				of Completie	on :09-05-2023			
Depth (m)	Sample & In-SituTest Depth (m)	Sample Type	SPT N Value	Strata Description	SI	Classification	Graphic Log	Core Recovery (%) 0 25 50 75100	RQD (%) 0 25 50 75100	(Depth v/s SPT N Value) 0 10 20 30 40 50 60 70 80 9000	Special Dbservations
10.5	10.5	SPT-4	37							•	
11.0											
12.0	12	SPT-5	38								
12.5											
13.0	13	UDS-1									
13.5	13.5	SPT-6	45								
14.0											
14.5											
15.0	15	SPT-7	63	Medium dense to dense, brownish, Silty sand	SI	Μ					
15.5											
16.0	16	UDS*									
16.5	16.5	SPT-8	100								
17.0											
17.5											
18.0	18	SPT-9	77								
18.5				RailCor	0						
19.0	19	UDS*		Palien	aller	, ibn					
19.5	19.5	SPT-10	67	Director (Project)		, ! ,					
20.0				AIPUR		,	53 of 1	25			

Project .	Name :B	adi Chou	uper to T	ransport Nagar and Mansar	ovar to A	jmer Road of	JMRC at Jaipur.	Client :JMRCL		
				ffic police chauki (RAC hea				Easting :584132	m	
		n):(+)46		1 (No. :TN Aligi		BH Depth (m):40		
		ng Struct					Not Encountered	Inclination : Vert		
		ell & Aug				of Boring :15		Depth of Casing		
_	-	-05-2023					n :09-05-2023	1 0 0		
Depth (m) _20.0_	Sample & In-SituTest Depth (m)		SPT N Value	Strata Description	IS Classification	Graphic Log	Core Recovery (%) 0 25 50 751000	RQD (%) 2,5 5,0 7,5100	(Depth v/s SPT N Value) 0 10 20 30 40 50 60 70 80 91	Special Observation
20.0										
20.5				Medium dense to dense, brownish, Silty sand	SM			-		_
_21.0	21	SPT-11	68					-		
21.5								-		_
22.0	22	UDS-2						-		_
22.5	22.5	SPT-12	63	Dense, brownish, Clayey sand	SC					
23.0								-		
_23.5								-		_
_24.0	24	SPT-13	64					-	•	
24.5										
_25.0	25	UDS-3						-		
_25.5	25.5	SPT-14	100					-		
_26.0								-		
_26.5								-		_
_27.0	27	SPT-15	100	Very dense, brownish, Silty sand	SM			-		-
_27.5								-		
_28.0								-		_
_28.5	28.5	SPT-16	100	anil Co				-		_ •
_29.0				W Rail Cor	2 allo					
_29.5				Director (Project)				-		_

Clight	atu st uousi			FIELD) B(DREE	IOLE LC	\overline{OG}		
Project	Name :E	Badi Chou	uper to T	ransport Nagar and Mansaro	ovar to Aj	mer Road of	JMRC at Jaipur.	Client :JMRCL		
BH Loc	ation/Ch	ainage :1	Near Tra	ffic police chauki (RAC hea	dqu:Nort	hing :297692	7 m	Easting :584132	m	
		m):(+)46		1		No. :TN Alig		BH Depth (m):40		
Propose	ed/Existi	ng Struct	ure :				Not Encountered	Inclination : Vert		
Boring	<i>type</i> :Sh	ell & Aug	ger		Dia.	of Boring :1:	50 mm	Depth of Casing	(m) :Not Used	
Date of	Start :05	5-05-2023	3		Date	of Completio	on :09-05-2023			
Depth (m) 30.0	Sample & In-SituTest Depth (m)	Sample Type	SPT N Value	Strata Description	IS Classification	Graphic Log	Core Recovery (%) 0 25 50 7,5100 (RQD (%) 0 2,5 5,0 7,5100	(Depth v/s SPT N Value) ગ 1ρ 2p 3p 4p 5p 6p 7p 4p 3p00	Special Observations
										•
30.5	31	UDS*								
31.5	31.5	SPT-18	100							
32.0										
32.5										
33.0	33	SPT-19	100							•
33.5										
34.0	. 34	UDS*								
34.5	34.5	SPT-20	100							
35.0				Very dense, brownish, Silty sand	SM					
35.5	36	SPT-21	100							
36.5										
37.0	. 37	UDS*								
37.5	37.5	SPT-22	100						+++++++++++++++++++++++++++++++++++++++	•
38.0										
38.5				Rail Cor						
39.0	. 39	SPT-23	100	Director (Project)	ration.					
40.0	40	SPT-24		Director (Project)	*/	55 of 10	25			

CER	ITH ST HOUSE			FIELD) B(JREH	IOLE LC	<i>G</i>		
Project	<i>Name</i> :B	adi Chou	uper to T	ransport Nagar and Mansard	ovar to A	jmer Road of .	JMRC at Jaipur.	Client :JMRCL		
BH Loca	ation/Ch	ainage :]	Near Hai	numan Temple	Nort	hing :297709	1 m	Easting :584164	m	
Reduced	l Level (r	n):(+)46	3.910		BH. I	No. :TN Align	iment-03	BH Depth (m):40		
Propose	d/Existin	ng Struct	ure :		Wate	er Table (m):N	lot Encountered	Inclination : Vert	ical	
Boring i	<i>type</i> :She	ell & Aug	ger		Dia.	of Boring :15	0 mm	Depth of Casing	(m) :Not Used	
Date of	Start :07	-05-2023	3			of Completion	n :09-05-2023			
Depth (m)	Sample & In-SituTest Depth (m)	Sample Type	SPT N Value	Strata Description	IS Classification	Graphic Log	Core Recovery (%) 25 50 75100 0	RQD (%) 25 50 75100	(Depth v/s SPT N Value) 0 10 20 30 40 50 60 70 80 5000	Special Observation
0.0		DS								
0.5								-		
1.5				Filled up soil	FILL			-		
2.0								-		
2.5								-		
3.0	3	SPT-1	29					-	+++++++++++++++++++++++++++++++++++++++	
3.5										
4.0	4	UDS-1						-		
4.5	4.5	SPT-2	35					-		
5.0								-		
5.5	6	SPT-3	73					-		
6.5	Ť			Dense, brownish, Silty sand	SM					
7.0	7	UDS-2						-		
7.5	7.5	SPT-4	100					-		•
8.0										
8.5				o Rail Cor	2					
9.0 9.5	9	SPT-5	29	Director	(allion					
10.0	10	_UDS*_		(Project)	*	56 of 12	5			

CHG TR	HU ST HOUSE			FIELL	$\mathcal{D}B$	OREF	<i>IOLE LC</i>	OG		
Project .	Name :E	adi Chou	uper to T	ransport Nagar and Mansar	rovar to	Ajmer Road of	JMRC at Jaipur.	Client : JMRCL		
BH Loca	ation/Ch	ainage :1	Near Hai	numan Temple	No	orthing :297709	91 m	Easting :584164	m	
		n):(+)46		-		I. No. :TN Alig		BH Depth (m):40	1	
Propose	d/Existir	ng Struct	ure :		W	ater Table (m):1	Not Encountered	Inclination : Vert	ical	
Boring t	<i>type</i> :She	ell & Aug	ger		Di	a. of Boring :1	50 mm	Depth of Casing	(m) :Not Used	
Date of	Start :07	-05-2023	3				on :09-05-2023			
Depth (m)	Sample & In-SituTest Depth (m)	Sample Type	SPT N Value	Strata Description	IS Classification	Graphic Log	Core Recovery (%) 0 25 50 75100	RQD (%) 0 25 50 75100	(Depth V/s SPT N Value) 0 10 20 30 40 50 60 70 80 9000	Special Observation:
10.0										
10.5	10.5	SPT-6	33							
11.0										1
11.5										
12.0	12	SPT-7	40							
12.5										
13.0	13	UDS*								
13.5	13.5	SPT-8	45						+++++	
14.0										
_ 14.0_										
14.5										
15.0	15	SPT-9	52	Dense, brownish, Silty	SM					-
				sand						
15.5										
16.0	16	UDS*								
16.5	16.5	SPT-10	62						┼┼┼┼╋┼┼┼	
17.0										-
17.5										-
18.0	18	SPT-11	71						┼┼┼┼┼╋┼┼	-
18.5										-
19.0	19	UDS*		Director (Project)	2010II					-
				E (Manen	10					
19.5	19.5	SPT-12	74	Director	$\sim P$				┼┼┼┼┝┝┼┼	-
				(Project)	/*/	A set of the set of	-			
20.0		ecovere		JAIPUR		57 of 1	/5			1

	N	. 1. C1					IOLE LC			
-			-	ransport Nagar and Mansar				Client :JMRCL		
		-		numan Temple		thing :297709		Easting :584164		
		n):(+)46				No. :TN Alig		BH Depth (m):40		
		ng Structi					Not Encountered	Inclination : Vert		
		ell & Aug	-			. of Boring :1:		Depth of Casing	(m) :Not Used	
Date of		-05-2023	3			e of Completic	on :09-05-2023			
Depth (m) _20.0_	Sample & In-SituTest Depth (m)	Sample Type	SPT N Value	Strata Description	IS Classification	Graphic Log	Core Recovery (%) 0 25 50 751000	RQD (%) 2,5 5,0 7,5100	(Depth v/s SPT N Value) 0 10 20 30 40 50 60 70 80 9000	Special Observatior
_20.5	21	SPT-13	82							
			-							
21.5										
22.0	22	UDS*		Dense, brownish, Silty	SM					-
				sand						
22.5	22.5	SPT-14	91						+	-
23.0										-
23.5										-
	~	007.45								
_24.0	24	SPT-15	99							
24.5										
27.0										
25.0	25	UDS*								
		•								
25.5	25.5	SPT-16	100							
26.0										-
26.5										-
27.0	27	SPT-17	100	Very dense, brownish, Silty sand	SM					ł
07 5										
27.5										1
28.0	28	UDS*								
20.0	20	503								1
28.5	28.5	SPT-18	100							
				No Rail Co						T
29.0				110 hu 00	22					
				E Paren	間					
29.5				Director	-					-
				(Project))/ ,					
30.0	30	SPT-19	_100_	AIPUR	*/	58 of 1	25			1

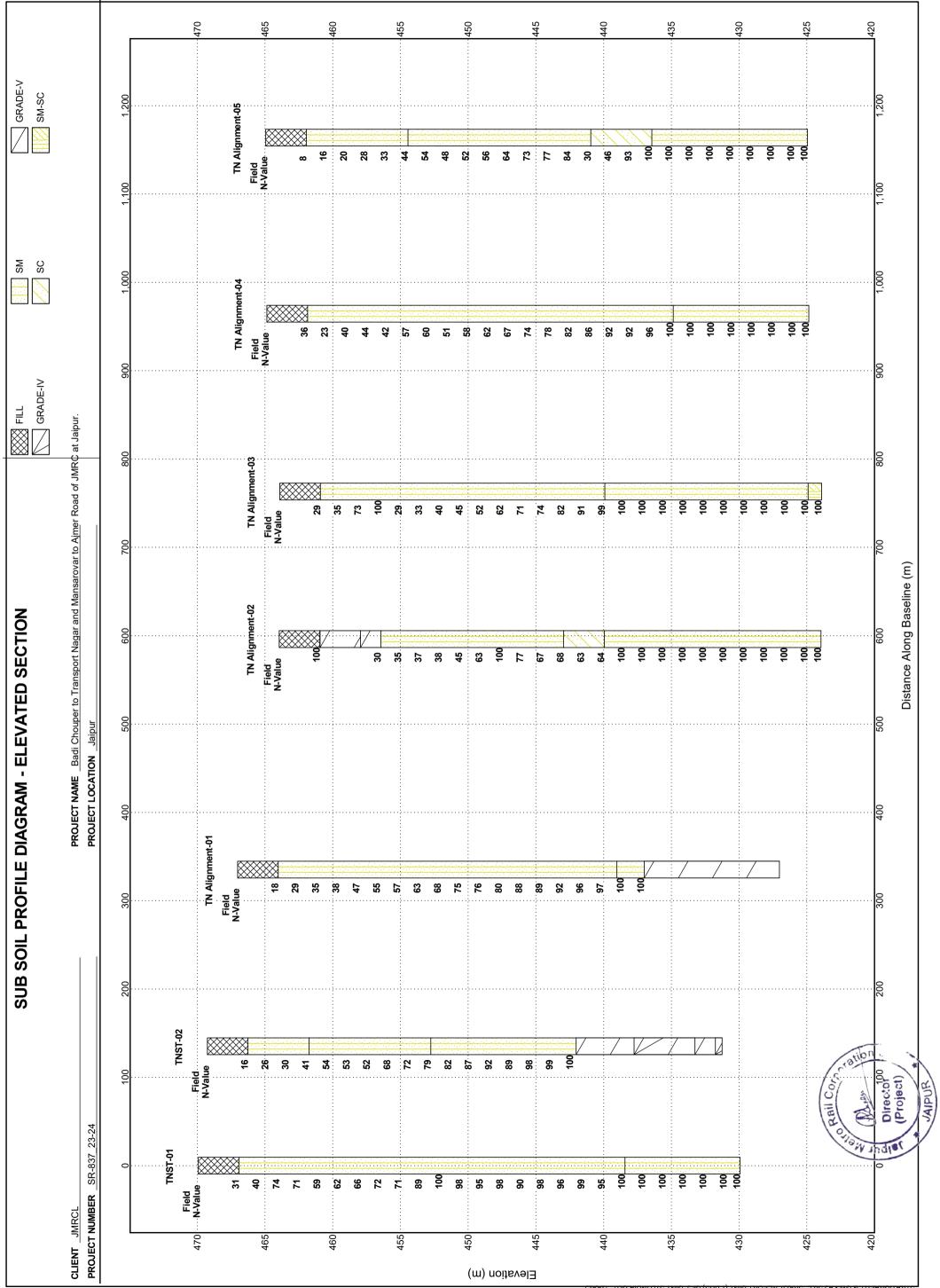
Project l	Name :B	adi Chou	uper to T	ransport Nagar and Mansaro	var to Aj	mer Road of	JMRC at Jaipur.	Client : JMRCL		
				numan Temple	-	hing :297709		Easting :584164	m	
		n):(+)46			-	No. :TN Alig		BH Depth (m):40		
		ng Struct					Not Encountered	Inclination : Vert		
		ell & Aug				of Boring :1		Depth of Casing		
		-05-2023					on :09-05-2023		(,	
Depth (m)	est m)		ODT	Strata Description	IS Classification	Graphic Log	Core Recovery (%) 0 25 50 7,5100 0	RQD (%) 25 50 75100	(Depth v/s SPT N Value) 0 10 20 30 40 50 60 70 80 91	Special Observation
30.0					0			2,0 0,0 7,0100	0 10 20 30 40 50 60 70 80 91	
30.5 _31.0_	31	UDS*						-		-
31.5	31.5	SPT-20	100					·		•
32.0										
32.5										
33.0	33	SPT-21	100					-		-•
33.5								-		
_34.0	34	UDS*						-		
_34.5	34.5	SPT-22	100	Very dense, brownish, Silty sand	SM			-		-
_35.0								-		_
_35.5								-		_
_36.0	36	SPT-23	100					-		-
_36.5										_
_37.0	37	UDS*						-		_
_37.5	37.5	SPT-24	100					-		-
_38.0										_
_38.5	~~~		105	No Rail Cor	2					
_39.0 _39.5	39	SPT-25		Very cause, brownishor Clave, Silty sand (Project)	151			-		→

CRUTER	ITH ST HOUSE			FIELL) B(OREH	IOLE LC	OG		
Project	Name :B	adi Chou	uper to T	ransport Nagar and Mansar	ovar to A	jmer Road of	JMRC at Jaipur.	Client :JMRCL		
BH Loca	ation/Ch	ainage :]	Near Kri	shi Mandi	Nor	thing :297728	9 m	Easting :584201	m	
		n):(+)46				No. :TN Aligr		BH Depth (m):40		
Propose	d/Existin	ng Struct	ure :				lot Encountered	Inclination : Vert		
		ell & Aug				of Boring :15		Depth of Casing	(m) :Not Used	
Date of L	Start :11	-05-2023	3		Date	e of Completio	n :15-05-2023			
Depth (m)	Sample & In-SituTest Depth (m)	Sample Type	SPT N Value	Strata Description	IS Classification	Graphic Log	Core Recovery (%) 0 25 50 75100 0	RQD (%) 25 50 75100	(Depth v/s SPT N Value) 0 10 20 30 40 50 60 70 80 5000	Special Observation:
0.0		DS								
0.5 1.0										
1.5				Filled up soil	FILL					
2.0										
2.5										
3.0	3	SPT-1	36						•	
3.5										
4.0	4	UDS-1								
4.5	4.5	SPT-2	23							
5.0										
5.5										
6.0	6	SPT-3	40							
6.5				Dense, brownish, Silty sand	SM			·		
7.0	7	UDS-2								
7.5	7.5	SPT-4	44							
8.0										
8.5				Rail Col						
_9.0	9	SPT-5	42	Rail Cor	ratio					
9.5				Director (Project)	171					
10.0	10	UDS-3		JAIPUR	*/	60 of 12	5			

CEG	ITH ST HOUSE			FIELD) BC	DREE	IOLE LO	G		
Project	Name :E	adi Chou	per to T	ransport Nagar and Mansarc	ovar to Aj	mer Road of	JMRC at Jaipur.	Client : JMRCL		
BH Loca	ation/Ch	ainage :1	Near Kri	shi Mandi	Nort	hing :297728	9 m	Easting :584201	m	
		n):(+)464				No. :TN Aligi		BH Depth (m):40		
Propose	d/Existir	ng Structi	ure :				Not Encountered	Inclination : Vert		
		ell & Aug			Dia.	of Boring :15	51 mm	Depth of Casing	(m) :Not Used	
Date of	Start :11	-05-2023	3			of Completio	n :15-05-2023			
Depth (m) _10.0_	Sample & In-SituTest Depth (m)	Sample Type	SPT N Value	Strata Description	IS Classification	Graphic Log	Core Recovery (%) 0 25 50 7,5100 0	RQD (%) 25 50 75100	(Depth v/s SPT N Value) 0 10 20 30 40 50 60 70 80 5000	Special Observations
10.0										
10.5	10.5	SPT-6	57							
11.0										
11.5										
12.0	12	SPT-7	60							
12.5										
13.0	13	UDS-4								
13.5	13.5	SPT-8	51							
14.0										
14.5										
15.0	15	SPT-9	58	Dense, brownish, Silty sand	SM					
15.5								-		
16.0	16	UDS-5								
16.5	16.5	SPT-10	62							
17.0										
17.5										
18.0	18	SPT-11	67							
18.5				Director (Project)	2					
19.0	19	UDS-6		A Bluen	nolite					
19.5	19.5	SPT-12	74	Director (Project)	1					
20.0				JAIPUR	<u>/</u>	61 of 1	25			

CES	THOUSE			FIELL	$\mathcal{D}B$	OREE	IOLE LC	OG		
Project 1	Vame :B	adi Chou	per to T	ransport Nagar and Mansar	ovar to	Ajmer Road of	JMRC at Jaipur.	Client :JMRCL		
BH Loca	tion/Ch	ainage :1	Near Kri	shi Mandi	Ne	orthing :297728	9 m	Easting :584201	m	
Reduced						I. No. :TN Alig		BH Depth (m):40		
Propose							Not Encountered	Inclination : Vert		
Boring t					D	ia. of Boring :15	51 mm	Depth of Casing	(m) :Not Used	
Date of S	Start :11	-05-2023	3			ite of Completio	n :15-05-2023			
Depth (m) _20.0_	Sample & In-SituTest Depth (m)	Sample Type	SPT N Value	Strata Description	IS Classification	Graphic Log	Core Recovery (%) 0 25 50 7,5100 (RQD (%) 0 25 50 75100	(Depth V/s SPT N Value) 0 10 20 30 40 50 60 70 80 9000	Special Observations
20.0										
20.5	21	SPT-13	78							
21.5										
22.0	22	UDS*								
22.5	22.5	SPT-14	82							
23.0										
23.5										
24.0	24	SPT-15	86							
25.0	25	UDS*		Dense, brownish, Silty sand	SM					
25.5	25.5	SPT-16	92						++++++	
26.0										
26.5										
27.0	27	SPT-17	92							
27.5	28	UDS*								
28.5		SPT-18	96							
29.0				Rail Cor	22101					
29.5				Director (Project)						
		SPT-19		JAIPUR	*/	62 of 12	25			

CER	THE ST HOUSE			FIELL	$\mathcal{D}B$	OREE	IOLE LC	∂G			
Project I	Name :E	adi Chou	uper to T	ransport Nagar and Mansar				Client :JMRCL			
BH Location/Chainage :Near Krishi Mandi				N	Northing :2977289 m		<i>Easting</i> :584201 m				
Reduced Level (m):(+)464.859					BH. No. :TN Alignment-04		BH Depth (m):40				
Proposed/Existing Structure :					Water Table (m):Not Encountered		Inclination : Vert				
Boring t						a. of Boring :1:		Depth of Casing (m) :Not Used			
Date of S	Start :11	-05-2023	3			te of Completio	on :15-05-2023				
Depth (m) _30.0_	Sample & In-SituTest Depth (m)	Sample Type	SPT N Value	Strata Description	IS Classification	Graphic Log	Core Recovery (%) 0 25 50 7,5100 (RQD (%) 0 2,5 5,0 7,5100	(Depth v/s SPT N Value) 0 10 20 30 40 50 60 70 80 5000	Special Observations	
30.0										•	
30.5 _31.0_	31	UDS*									
31.5	31.5	SPT-20	100							•	
32.0											
32.5								·			
33.0	33	SPT-21	100							•	
33.5											
34.0	34	UDS*									
34.5	34.5	SPT-22	100							•	
35.0				Very dense, brownish, Silty sand	SM						
35.5	36	SPT-23	100							-	
36.5	- •										
37.0	37	UDS*						·			
37.5	37.5	SPT-24	100								
38.0											
38.5				Rail Col.							
39.0	39	SPT-25	100	Director (Project)	nation					•	
39.5				Director (Project)							
40.0 UDS*-UI		SPT-26		JAIPUR	/	63 of 1	25			<u> </u>	



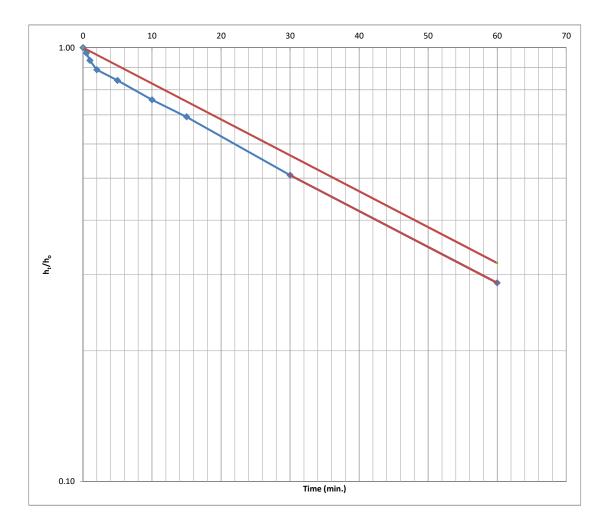
<u>STRATIGRAPHY & GW - A3 SIZE SR.837 REPORT GINT (7 RHS) GP1 GINT STD INDIA GDT 12.6.23</u>

64 of 125

Borehole N	0.:-	TN STN-01				
Depth From	m:-	30.25 m	Depth To:-	31.00 m		
Diameter o	of Intake pipe	e (d) 150.0 mm	Co-ordinates:- (m)	E 583984.000	N 2976349.000	
Length of t	test section (I	L) 0.75 m				1
Water leve	l at time t ₀ =	H ₀ 2.44 m		ł	-	1
Coefficient	t of Permeabi	ility, $\mathbf{K} = (\mathbf{d}^2/\mathbf{8L})\ln[(\mathbf{L}/\mathbf{r})(\ln(\mathbf{h}_1))]$	/h ₂)/((t ₂ -t ₁)]			
_			Where,	d = diameter of i	* *	
l ² /8L	=	3.7500E-03		L = length of tes		
n (L/r)	=	2.303		$h_1 = head of wate$		
$n(h_2/h_1)$	=	0.419		$h_2 = head of wate$	=	
2 -t 1	=	22		r = radius of hole	e	
c Calculation	= s:	1.65E-04	2.74E-04 cm/sec			
S.No.		H = Water level in the intake pipe at time (t) in metre	Height of Water Level (m) at time t, H ₁ = H ₀ -H	H _t /H ₀	From Graph	
1	0	0.00	2.44	1.00	h ₁ /h _o	1
2	0.5	0.07	2.37	0.97	h_2/h_o	0.6
3	1	0.16	2.28	0.93	t ₁	0
4	2	0.27	2.17	0.89	t ₂	22
5	5	0.39	2.05	0.84	1	
6	10	0.59	1.85	0.76	1	
7	15	0.75	1.69	0.69	1	
8	30	1.20	1.24	0.51	1	
9	60	1.74	0.70	0.29		











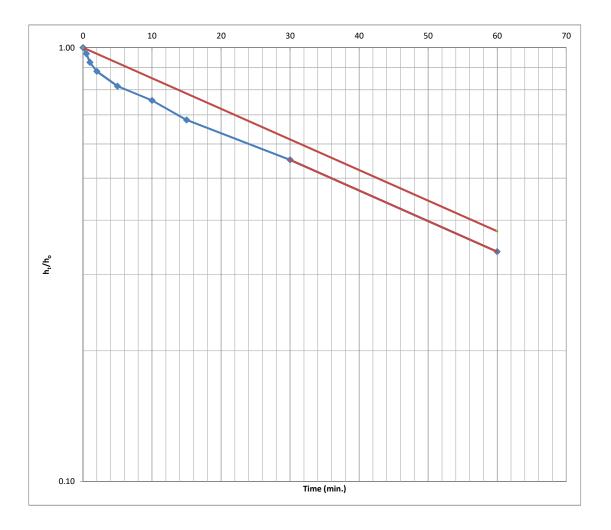


Borehole N	No.:-	TN STN-0	1			
Depth Fro	m:-	20.25 m	Depth To:-	21.00 m		
Diameter o	of Intake pipe	e (d) 150.0 mm	Co-ordinates:-	Е	Ν]
Length of	test section (I	L) 0.75 m	(m)	583984.000	2976349.000	1
Water leve	el at time $t_0 =$	H ₀ 2.54 m		4	-	4
Coefficien	t of Permeabi	ility, K = (d ² /8L)ln[(L/r)(ln(h ₁ /h ₂)/((t ₂ -t ₁)]			
			Where,	d = diameter of	* *	
1²/8L	=	3.7500E-03		L = length of tes		
ln (L/r)	=	2.303		$h_1 =$ head of wat	-	
$\ln \left(h_2 / h_1 \right)$	=	0.357		$h_2 = head of wat$	=	
t ₂ -t ₁	=	22		r = radius of hol	le	
k Calculation	=	1.40E-04	2.34E-04 cm/sec			
S.No.		H = Water level in the inta pipe at time (t) in metre		H _t /H ₀	From Graph	
1	0	0.00	2.54	1.00	h ₁ /h _o	1
2	0.5	0.08	2.46	0.97	h ₂ /h _o	0.7
3	1	0.19	2.35	0.93	t ₁	0
4	2	0.30	2.24	0.88	t ₂	22
5	5	0.47	2.07	0.81		
6	10	0.62	1.92	0.76		
7	15	0.81	1.73	0.68		
8	30	1.14	1.40	0.55		
9	60	1.68	0.86	0.34		









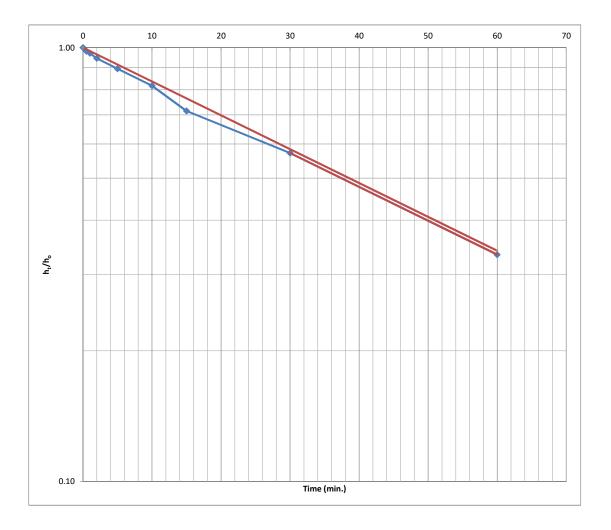




Borehole N	No.:-	TN STN-02				
Depth Fro	m:-	12.00 m	Depth To:-	12.75 m		
Diameter o	of Intake pipe	e (d) 150.0 mm	Co-ordinates:- (m)	Е	Ν]
Length of	test section (I	L) 0.75 m		584079.000	2976467.000	1
Water leve	el at time $t_0 = 1$	H ₀ 2.73 m		4	-	4
Coefficien	t of Permeabi	ility, $\mathbf{K} = (\mathbf{d}^2/8\mathbf{L})\ln[(\mathbf{L}/\mathbf{r})(\ln(\mathbf{h}_1)]]$				
-			Where,	d = diameter of		
1 ² /8L	=	3.7500E-03		L = length of tes		
n (L/r)	=	2.303		$h_1 =$ head of wat	-	
$n(h_2/h_1)$	=	0.395		$h_2 = head of wat$	=	
t ₂ -t ₁	=	22 1.55E-04	2.59E-04 cm/sec	r = radius of hol	e	
k Calculation		1.33E-04	2.59E-04 cm/sec			
S.No.		H = Water level in the intake pipe at time (t) in metre	Height of Water Level (m) at time t, H ₁ = H ₀ -H	H _t /H ₀	From Graph	
1	0	0.00	2.73	1.00	h ₁ /h _o	1
2	0.5	0.05	2.68	0.98	h ₂ /h _o	0.6
3	1	0.08	2.65	0.97	t ₁	0
4	2	0.15	2.58	0.95	t ₂	22
5	5	0.29	2.44	0.89		
6	10	0.50	2.23	0.82	7	
7	15	0.78	1.95	0.71		
8	30	1.17	1.56	0.57		
9	60	1.82	0.91	0.33		











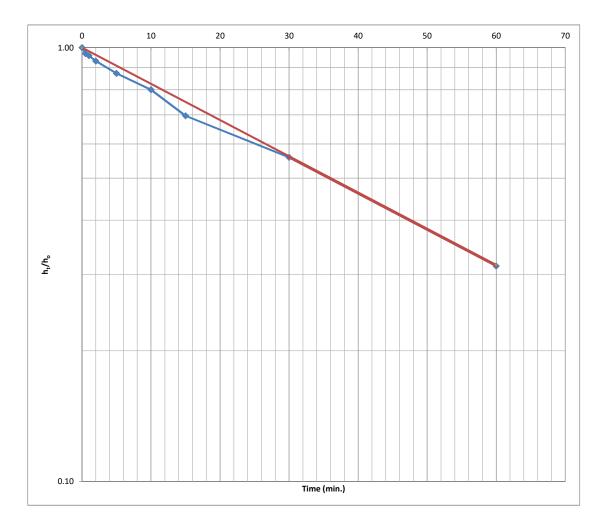


Borehole N	(0.:-	TN STN-02	2			
Depth From	m:-	20.00 m	Depth To:-	20.75 m		
Diameter o	of Intake pipe	e (d) 150.0 mm	Co-ordinates:-	Е	Ν	1
Length of t	test section (L	L) 0.75 m	(m)	584079.000	2976467.000	
Water leve	el at time $t_0 = 1$	H ₀ 2.90 m		4	-	4
Coefficient	t of Permeabi	ility, $K = (d^2/8L)ln[(L/r)(ln(l))]$	h ₁ /h ₂)/((t ₂ -t ₁)]			
			Where,	d = diameter of		
1²/8L	=	3.7500E-03		L = length of tes		
n (L/r)	=	2.303		$h_1 = head of wat$	-	
$n(h_2/h_1)$	=	0.423		$h_2 = head of wat$	=	
t ₂ -t ₁	=	22		r = radius of hol	e	
k Calculation	=	1.66E-04	2.77E-04 cm/sec			
S.No.		H = Water level in the intal pipe at time (t) in metre	ke Height of Water Level (m) at time t, H ₁ = H ₀ -H	H _t / H ₀	From Graph	
1	0	0.00	2.90	1.00	h ₁ /h _o	1
2	0.5	0.09	2.81	0.97	h ₂ /h _o	0.6
3	1	0.12	2.78	0.96	t ₁	0
4	2	0.20	2.70	0.93	t ₂	22
5	5	0.37	2.53	0.87		
6	10	0.58	2.32	0.80	-	
7	15	0.88	2.02	0.70	7	
8	30	1.28	1.62	0.56	7	
9	60	1.99	0.91	0.31		









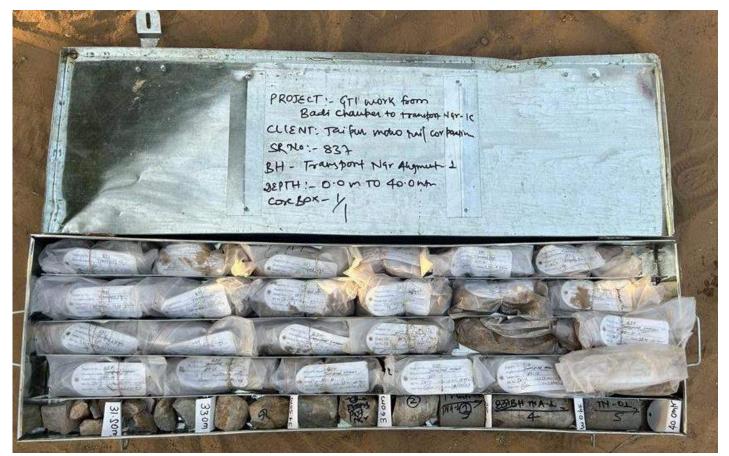




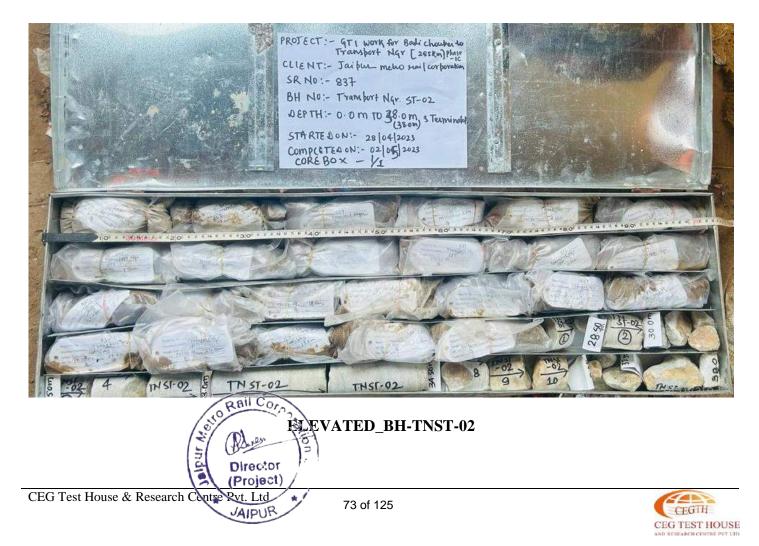


Geo-technical Investigation work for Extension of underground and elevated section E-W Corridor from Badi Chouper to Transport Nagar (2.85Km) Phase-1C and Mansarovar to Ajmer Road (Chauraha) (1.35 km) Phase-1D of Jaipur Metro Rail Corporation at Jaipur.

COREBOX PHOTOGRAPHS



ELEVATED_BH-TN Alignment-01



Geo-technical Investigation work for Extension of underground and elevated section E-W Corridor from Badi Chouper to Transport Nagar (2.85Km) Phase-1C and Mansarovar to Ajmer Road (Chauraha) (1.35 km) Phase-1D of Jaipur Metro Rail Corporation at Jaipur

APPENDIX – B (LAB TEST RESULTS)

Appendix No.	ITEMS
B-1	SOIL CHARACTERISTICS SHEETS
B-2	GSD CURVE
B-3	RESULTS OF CHEMICAL ANALYSIS OF SOIL SAMPLE
B-4	SHEAR CURVE





roie		- Dal	Director (Project) /	Pd	SPT-1	UDS-1	SPT-2	SPT-3	UDS-2	SPT-4	SPT-5	UDS-3	SPT-6	SPT-7	NDS*	SPT-8	6-TqS	UDS*	SPT-10	SPT-11	*SUU
"Geo.	(1.35	≺/	Rati Co Ta uo.j usdan	01	-1 3.00	5-1 4.00	-2 4.50	-3 6.00	5-2 7.00	.4 7.50		3-3 10.00	-6 10.50	7 12.00	S* 13.00	-8 13.50	-9 15.00	S* 16.00	-10 16.50	-11 18.00	S* 19.00
-technical menort N	km) Phas	ənisV	(N)		0 31	- 0	0 40	0 74	- 0	0 71	0 59	- 00	50 62	99 00	- 00	50 72	00 71	- 00	60 89	0 >100	0
Investig:	e-1D of J		Corrected SI Value (N _c)	,	37		43	72		64	50	1	49	49	'	51	48		57	'	,
"Geo-technical Investigation work for Extension of E-W corridor from Badi Chouper Droisor to Transnort Nagor (7 83km) Phase -1C and Mansarovar to Aimer Road (Chameleo)	DALID F HARSE - I.C. and MAILSAUCHAR IN 701. aipur Metro Rail Corporation at Jaipur.		Soil Description	Filled up soil									Dense to very dense, brownish, silty sand								·
lor from Badi		uoi	IS Classificat	ı	I	SM	ı	ı	SM	ı		SM	ı	ı		SM	ı	ı	SM	ı	ı
i Chouper	liaul alla)		lodmy2 21																		
L			Clay		1	0			0		'	0		,	'	0	1		0	1	,
Dat	21-04-2023	Grain (IIS	,	1	18	1	1	16		1	16		,	1	17	1		18	,	,
Date of Boring	to	Grain Size Distribution % wt retained	əniA			64			89			72				70			99	1	
<u>ല</u>	26-04-2023	bution %	Sand muib9M			13			Ξ			6				9			12		
-		o wt retai	Coarse			с С			4			2				S			4		,
Chainage/Location	ansport Na of water h	ned	Fine Grave Crave Coarse	'		2 0			1 0			1 0		'		2 0			0 0	' '	
/Location	Transport Nagar in front of water head tank		Liquid Limit	, ,		· ·	'		· ·		'	'			'	·	, ,	·	· 	· ·	
		Atterbe	Plastic Limit	'	1	Nil			Nil		'	Nil		'	'	Nil			Nil	,	
B.H. No.	TNST-01	Atterberg Limits %	Plasticity Vadicity	1		đN	'	1	ď			ND				ŊŊ	1		đN	1	
Depth (Not	%	Shrinkage Limit	,	ı	1		1				ı		1			1				
Depth of Water Table	Not Encountered		g) yiiznəC Alu&			1.79		I	1.80		1	1.80			1	1.80	ı	ı	1.82	ı	
	pa	(isioM IsrutsN %) tnotnoD			8.90			9.20			9.25				9.30	,		9.55		
Depth	40.00 m		Dry Density (g/			1.64 2			1.65 2			1.65 2				1.65 2			1.66 2		
		الزلا	verð sflissq2 tærð fræði			2.62 DS			2.62 DS			2.62 DS				2.62 DS			2.62 DS		
	583984.000 m	Shear Strength	Type of Test Cohesion C			DST 0.00			DST 0.00			DST 0.00		'		DST+ 0.00			DST+ 0.00		
Cordin)00 m	rength	(kg/cm ²) fo signA Friction (o°)			00 31			00 32			00 32				00 32			00 32		
Cordinates (E,N)	297	хәр	Free Swell Inc (%)	,	ı	ı	ı	1				ı		,			1			1	
	2976349.000 m		Swelling Press (kg/cm ²)		ı		1					ı					1		ı	1	
	m	Â	Permeabilit (cm/sec)			ı	ı	1				ı									
R.L.	+469.925	Cons	Void Ratio (e_) Pressure														1				
		Consolidation Parameters	С ^{^ х} 10 _{-t} (қб\сш ₅₎																	, ,	
Ref. Code	SR-837_22-23	Paramete	(500 ₇ /Kg) 2-01 x M (5095/2m2)	'	1		1				'	1		'	'		1			,	
ode	22-23	srs	Compression	'	'	'	1	'	1	1	1	ı	1	'	1	1	'	'	'	'	1



Abbreviations:-DS-Disturbed Sample, SPT-Standard Penetration Test, UDS-Undisturbed Sample, UDS*-UDS not recovered, DST-Direct Shear Test, UUT-Unconsolidated Undrained Triaxial Shear Test, DST+ - Direct Shear Test on Remoulded Sample, UUT+ - Unconsolidated Undrained Tri-axial Test on Remoulded Sample.

	Proje	"Geo Sct to Tr	o-technical ransport N	l Investigat lagar (2.851	Project to Transport Nagar (2.85km) Phase -1C and Mansarovar to Ajmer Road (Chauraha)	lor from Badi (ner Road (Cha "	Chouper uraha)		Date of	Date of Boring		Chair	Chainage/Location	ion	B.H. No.	Dep	Depth of Wate	ter Table	Term De	Termination Depth		C01	Cordinates (E,N)	(E,N)			R.L.		Ref. Code	9
Matrix sectors and sec	1	(1.35	5km) Phas	se-1D of Ja	ipur Metro Rail Corporation at Jaipur."	=.		21-04-2(04-2023	Transpo of we	rt Nagar In tter head tai		TNST-01	~	Not Encour	ntered	40.1	00 m	583	984.000 m		29763	49.000 m		+469.925	SF	R-837_22	-23
Matrix	► I ~	∖</th <th>ənie A</th> <th></th> <th></th> <th>uoi</th> <th></th> <th>)</th> <th>Grain Size</th> <th>Distributi</th> <th></th> <th>etained.</th> <th></th> <th>Atter</th> <th>berg Limi</th> <th>its %</th> <th>(_ewə/</th> <th>ə.n.;</th> <th>(_ewə</th> <th>ŢţŢ.</th> <th>Shea</th> <th>r Strengtl</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>dation Pa</th> <th>rameters</th> <th></th>	ənie A			uoi)	Grain Size	Distributi		etained.		Atter	berg Limi	its %	(_e wə/	ə.n.;	(_e wə	ŢţŢ.	Shea	r Strengtl						dation Pa	rameters	
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Ľ	SR	tion Par		(cm ² /Sec) C ^v x 10 ⁻⁴	ı	ı	ı
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	m (л		Permeabi Des/mo)			ı
	2976349.000 m	nre		ord gnillow2 mo/ga)			ı
(E,N)	2976	хәр	u	Eree Swell (%)	-	-	-
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Cor	583984.000 m	Shear Strength		Cohesion C (kg/cm ²)	0.00		ı
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th th	m (ţţ	AB.	1D sifisedS	2.63	-	
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r Table	ntered			oM læruræl) fnofnoð	11.30		1
Depth of Water Table	Not Encount	(_e wə/	B)	Bulk Density	1.88	ı	ı
Depth	Not	0		Shrinkage Jimit	1		ı
B.H. No.	TNST-01	Atterberg Limits %		Plasticity Index	dN	'	ı
B.H	TNS	Atterberg	1	imiJ sitsel¶	Nil		
cation	in front l tank	7	1	imiJ biupiJ	·	'	ı
Chainage/Location	Transport Nagar in front of water head tank		Gravel	Coarse	0	1	ı
Chai	Transpo of w	retained	Gr	əniA	1	'	ı
	26-04-2023	Grain Size Distribution % wt retained		Serse	1	ı	ı
oring	26-0	stributio	Sand	muibəM	2	1	ı
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_	21-0			VrIJ	0	'	1
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W corridor from Badi Choupe ar to Aimer Road (Chauraha)		uoj	ite	Jiiserl') SI	SM	ı	ı
"Geo-technical Investigation work for Extension of E-W corridor from Badi Chouper to Transnort Nacor O 85(m) Phase -IC and Manearover to Aimar Road (Channaha)	(1.35km) Phase-1D of Jaipur Metro Rail Corporation at Jaipur."			Soil Description		ownish, silty sand	
"Geo-technical Investigation work for Extension of E- Protiont to Transnort Navar (2 S5km) Phase -1C and Manearov	Jaipur Metro Rail (Very dense, brownish, silty	
cal Investig	hase-1D of .	Lo	IS	(N) Corrected Dalue (I	- >100	>100 -	- >100
o-techni ransnort	5km) Pł	auls V	2	Diserved SP		39.00 >1	
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	Proiect	"Geo-technical Investigs Chonner to Transnort Ns	ation work for Extension of E-W corride la or (7 85km) Phase - I C and Manserov	or from Badi ar to Aimer R	per	Da	Date of Boring		Chainag	Chainage/Location	B.F	B.H. No.	Depth of `	of Water Table		Termination Depth		Ŭ	Cordinates (E,N)	(E,N)		-	R.L.	Ť.	Ref. Code
A sector of the sector		(Chauraha) (1.35km) Ph	agar (2.12) of Jaipur Metro Rail Corporatio	n at Jaipur."		28-04-2023		-05-2024	In front of stoe	î Khandelwai 1 shop		'NST-02	Not Er	ncountered		38.00 m	5	84079.000 i	u	297646	2976467.000 m	+46	+469.254	SR	SR-837_23-24
(1) (2) <th></th> <th>مT /alue / (m)</th> <th></th> <th>uo</th> <th></th> <th>Grain</th> <th>Size Distribu</th> <th>tion % wt r</th> <th>etained</th> <th></th> <th>Atterber</th> <th>g Limits %</th> <th></th> <th></th> <th>(</th> <th></th> <th></th> <th>tear Streng</th> <th></th> <th></th> <th></th> <th></th> <th>Consolid</th> <th>Consolidation Parameters</th> <th>ameters</th>		مT /alue / (m)		uo		Grain	Size Distribu	tion % wt r	etained		Atterber	g Limits %			(tear Streng					Consolid	Consolidation Parameters	ameters
Matrix Indivinition Individition	Pluen	Depth from G.L Observed SPT V (V) Corrected SP	Soil Description	ifsofficati	lodmy2 21				G S S S	Coarse	Plastic Limit		timiJ		(%) tnotnoD			-	Friction (¢°)	Free Swell Ind (%) Swelling Press	(kg/cm²) Permeability	(cm/sec) Void Ratio (e_)	(k&\cw ₃₎ Lessence	(cm ² /Sec) C ^a x 10-4	(By/zmo) 7-01 x M
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700 1 1 1 0 1	SPT-3	6.00 30									,	1							,		1	1	,	1	1
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Abbreviations:-DS-Disturbed Sample, SPT-Standard Penetration Test, UDS-Undisturbed Sample, UDS*-UDS not recovered, DST-Direct Shear Test, UUT-Unconsolidated Undrained Triaxial Shear Test, DST+ - Direct Shear Test on Remoulded Sample, UUT+ - Unconsolidated Undrained Tri-axial Test on Remoulded Sample.



Abbreviations:-DS-Disturbed Sample, SPT-Standard Penetration Test, UDS-Undisturbed Sample, UDS*-UDS not recovered, DST-Direct Shear Test, UUT-Unconsolidated Undrained Triaxial Shear Test, DST+ - Direct Shear Test on Remoulded Sample, UUT+ - Unconsolidated Undrained Tri-axial Test on Remoulded Sample.



	"Geo-technic	cal Investigat	ion work for Extension of E-W corr	idor from Badi		ü	Date of Boring	ing		Challagy Lucauu							Depth									NUL COUC
Projec	Chouper to (Chauraha) (1 ransport Νε (1.35km) Ρhε	Project Chouper to Transport Nagar (2,85km) Phase -IC and Manastovar to Ajmer Koad (Chauraha) (1.35km) Phase-1D of Jaipur Metro Rail Corporation at Jaipur."	ovar to Ajmer K tion at Jaipur."		25-04-2023	to	02-05-2023		Near red light police booth	it police	BH-TN Alignment-01	IN nt-01	Not Enc	Encountered		40.00 m	<u>с</u>	584086.000 m	н	29766	2976670.000 m	т 	+467.024	S	SR-837_23-24
Jelpur Alera	(w) "	Lo		uoj		Grain	Size Dist	Grain Size Distribution % wt retained	wt retaind	p	V	Atterberg Limits %	imits %			(S	Shear Strength	gth				Consoli	Consolidation Parameters	ameter
Director	Depth from G.L Observed SPT V	(N) Corrected SF Value (N,)	Soil Description	IS Classificati	lodmy2 21	Clay	əniA	Sand muib9M	Coarse Fine	Coarse Coarse	timi.I biupi.I	Plastic Limit	Plasticity x9bn1	Shrinkage Limit	Bulk Density (g, Natural Moist	%) tnstnoD	Dry Density (g/ Specific Grav	tesT to sqvT) noisəhd Cohesion C	Angle of Friction (φ°)	Free Swell Inc (%)	Swelling Press (kg/cm ²) Permeabilit	(cm/sec) Void Ratio (e_)	(kg/cm ²⁾ Pressure	(cw ₅ /26c) C [^] x 10 ₄	(cm ² /Kg) M _v x 10 ⁻²
*Sol tion	9.00																									I
SPT-12	19.50	80 46					ı			1									ı	1				ı		I
SPT-13	21.00	88 49				,					'			,												ı
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UDS*	25.00			1			,		'	1								ı	1	1				ı	,	ı
SPT-16	25.50	96 47		1			1		' '	ı								ı	,	1		,		1	,	I
SPT-17	7 27.00 97	7 46												,				ı								I
*SQU	28.00													,												I
SPT-18	8 28.50 >100	- 00	Very dense, brownish, Silty sand	SM		0 26	63	s	5 1	0		Nil	ď	-	1.86 10	10.11 1.0	1.69 2.63	DST+	0.00	33						I
SPT-19	30.00	>100 -				•								,				ı								I
RC-1	30.02			GRADE-V	//	C. R. = 6.66 %	R.Q.D. = 0 %	•% 0 =				'														
RC-2	31.50			GRADE-V	//	C. R. = 8 %	R.Q.D. = 0 %	•% 0 =				1		'												
RC-3	33.00			GRADE-V	//	C. R. = 5.33 %	R.Q.D. = 0 %	•% 0 =				'		'										'		
RC-4	34.50		Highly weathered, very poor, brownish, medium grained Ouartzite	GRADE-V	//	C. R. = 7.33 %	R.Q.D. = 0 %	•% 0 =				I		'												
RC-5	36.00			GRADE-IV		C. R. = 10.33 %	R.Q.D. = 0 %	•% 0 =	Sp.Gr. = 2.65	W.A.	= 1.56 %			Porosity = 4.1	4.13 %											
RC-6	37.50			GRADE-V	//	C. R. = 10 %	R.Q.D. = 8.66 %		Sp.Gr. = 2.66	W.A.	= 1.47 %			Porosity $= 3.9$	3.91 %									P.L.I. = 115.67 (t/m ²)	57 (t/m²)	
RC-7	39.00			GRADF-V	/	C D = 0 %) o o																		



Abbreviations:-DS-Disturbed Sample, SPT-Standard Penetration Test, UDS-Undisturbed Sample, UDS*-UDS not recovered, DST-Direct Shear Test, UUT-Unconsolidated Undrained Triaxial Shear Test, DST+ - Direct Shear Test on Remoulded Sample, UUT+ - Unconsolidated Undrained Tri-axial Test on Remoulded Sample.

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Ref. Code	SR-837_22-23	neters		Compression	1	ı			,					1				,		,	1
Ref	SR-8.	Consolidation Parameters		W ^A X 10 ₋₅ (cu ₅ /2ec)	1	ı				ı				ı			1		ı		1
	0	isolidatio		C ^A x 10 ₄ (қ&\сш ₅₎		1			1		,			1	,		1	,	,		1
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	, T		(:	oəs/wə)		1				-				1					1		1
	2976927.000 m		(,	r9 gnilləw2 mɔ/gメ) Permeabi	1	1				ı	,			1	,						1
(E,N)	29769			Free Swell (%)	ı	I			1	ı	1			I	1				ı		1
Cordinates (E,N)			1	fo slgnA Φ) noitsirA	ı	ı	I	I		ı	31	,		ı	31				33		1
C01	584132.000 m	Shear Strength		Cohesion C (kg/cm²)		ı				ı	0.00			ı	0.00				0.00		1
	5841.	Shear	-	rs9T to 9qvT	1	1				1	DST+			1	DST			,	DST+		
ttion h	m	ity	IVB.	1D office Gr		I				ı	2.63 1			I	2.63				2.63		
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R.L.	+463.910	Consol	(kg/cm ²⁾ Pressure	'	1	'	1	1	'	'	'	'	'	'	'	'	'	ı	'	1
	+4		(09) oits R bio	\		'	ı			'	'		'	'	'		,	ı		ı
	00 m	Â	Permeability (cm/sec)			'	ı		'	'	'	'	'	'	'	'	'	1	,	
(2977091.000 m	nre	Swelling Press (kg/cm²)		1	'		ı	'	'	'	'	'	'		'		ı	'	
Cordinates (E,N)	25	xəp	Free Swell Inc (%)		1	'	'		'	'	1	'	1	ı	1	'	'		,	'
Cordina	0 m	ngth	(moven) Angle of Friction (9°)	'	1	31	'	1	32	'	'	'	31	'	'	'	'	1	31	,
	584164.000 m	Shear Strength	O noisənO (kg/cm²)		1	00.0	'		0.00	'	1	'	0.00	ı	1	'	'		00.0	'
	28	ЧS	tsəT to əqYT		,	DST	ı	ı	DST				+LSQ	-	-		ı	ı	DST+	ı
ation th	ш	ţţ	vrað sifisgel			2.62		ı	2.62				2.62					ı	2.63	1
Termination Depth	40.00 m	(₂ mə	(g) (g/	E '		1.59			1.62				1.58						1.64	1
Table	red		tsioM IsrutsV %) tnэtnoO			9.17			9.29				9.44						9.46	1
Depth of Water Table	Not Encountered	(_e mə/	(g) (jisnəd Alu	1 '		1.74			1.77	,			1.73	ı	1				1.80	1
Depth o	Not	` 0	Shrinkage Limit		1	-	ı	ı					-	-	-		ı	ı		ı
B.H. No.	BH-TN Alignment-03	Atterberg Limits %	Plasticity Index		1	dΝ	ı	I	NP	'			dN		-		ı	I	AN	I
B.H	BH Alignn	Atterberg	Plastic Limit			lίΝ		ı	ΪΝ				lίΝ	-	-			ı	liN	I.
cation	Temple	V	timi.I biupi.I			-							-	-			,			ı
Chainage/Location	Near Hanuman Temple		Gravel Coarse	ı	1	0	ı	ı	0	'			0	ı		ı	ı	I	0	ı
Chai	Near H	etained	9niA	ı	ı	1	ı	ı	-	'	'		1	·		ı	ı	I	0	ı
	09-05-2023	1 % wt r	Coarse	ı	1	3	ı	ı	s	'			1	ı		ı	ı	I	7	ı
ring	;0-60	tributio	Mand Mand Mand Mand Mand Mand Mand Mand			3	,		4	'		'	4	'	'	'	'	ı	я	
Date of Boring	to	Grain Size Distribution % wt retained	9niA			72	,		73	'	,	,	78	1		,	,	ı	70	ı
D	07-05-2023	Grain	JUS	,	1	21			17	'	'	'	16	'	'	,			25	ı
	00		Clay		'	0		1	0	1	,	1	0	,		,	ı	ı	0	
ii * Dood			lodmy2 21																	
lor from Ba	var to Ajure on at Jaipur	uo	IS Classificati	,	,	SM			SM		,		SM	ı	ı				SM	
"Geo-technical Investigation work for Extension of E-W corridor from Badi	gar (z. 0.21km) r trasse - 1.C anu mansaro se-1D of Jaipur Metro Rail Corporati		Soil Description	Filled up soil											Dense, brownish, Silty sand					
Investigat	isport va Skm) Pha		AS Corrected SP Value (N,)		35	'	38	71			24		26	30		32	35	ı	40	4
technical ar to Tra	raha) (1.3	ənls/	N) V TAS bəvrəsd		29	'	35	73		>100	29	,) 33) 40	- () 45) 52	') 62	71
"Geo-t	Chau			0	1 3.00	.1 4.00	2 4.50	3 6.00	.2 7.00	4 7.50	5 9.00	* 10.00	6 10.50	7 12.00	* 13.00	8 13.50	9 15.00	* 16.00	10 16.50	1 18.00
Dioior	LIOJE	1	are stilled	2 2 2 2 3 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3	SPT-1	UDS-1	SPT-2	SPT-3	UDS-2	SPT-4	SPT-5	*SQU	SPT-6	SPT-7	*SQU	SPT-8	6-TqS	*SQU	SPT-10	SPT-11
		Julpur A.	Director (Project	The second second						84	of 12	5								



ode	23-24	SJ(pression ex (C _c)	lmoD											,							
Ref. Code	SR-837_23-24	Consolidation Parameters	^v , Kg) x 10 ⁻²	'W	ı	ı	ı	ı	ı	ı	ı	ı	ı	ı	'	ı	1	ı	ı	1	1	ı
	01	dation P	(əəs/ _z u +01 x	°D	,		,		,	'	,	,	'		'		,	'	,	'	,	'
R.L.	+463.910	Consolic	d,cm ^{z)} essnre				,		1		,		1		,			1	,			,
	+		(09) (09) Batio (60)			ı			ı	1			1	ı	'			ı				·
	000 m	Á	(kg/cm) ermeabilit (cm/sec)	Ъ		ı	ı	ı	ı	1	ı		I	ı	'	ı		ı	ı	'		ı
(1	2977091.000 m	nre	(kg/cm ²) lling Press		ı	ı	1	1	1	1	1	ı	1	ı	'	1	1	1	1	1	1	1
Cordinates (E,N)	5	xəj	(°¢) noii e Swell Ine (%)		1	1	1	1	1	1	1	1	1	1	'	1	1	1	1	'	1	1
Cordin	00 m	ength	Jo algi gle of	u¥	1	1	'	'	32	'	'	1) 33	1	'	'	1	33	'	'	1	33
	584164.000 m	Shear Strength	O noisə		'	1	1	1	0.00	1	1	'	0.00	1	'	1	'	0.00	1	'	'	0.00
	S.	N	tsəT to s	ədYT	'	,	,	,	DST+	'	,	'	DST+	,	'	,	'	DST+	,	'	'	DST+
Termination Depth	40.00 m	ity	vrrd offic	əds	'				2.63	'		'	2.64		'		'	2.64		'	'	2.63
	40		(g) (g/		,				1.64	'		,	1.69				'	1.69		'	'	1.70
Depth of Water Table	ntered	nre	tsioM Isru %) tnotno	uteN					9.57	,			9.66		'			9.78		'		9.86
th of Wa	Not Encountered	(_e wə,	Density (g		1	1	,		1.80	1	,	1	1.85	1	'		1	1.86	,	'	1	1.87
Dep		ts %	xəbn inkage imit	зчs	1	1	•	1	'	1	•	1	'	1	'	1	1	'	•	'	1	'
B.H. No.	BH-TN Alignment-03	Atterberg Limits %	Viicity			•		•	đ	1			đ	•	'	•		đ		'		đ
		Atterb	timi.I si		1	1	'	1	IIN	'	'	1	Nil	1	'	1	1	Nil	'	'	1	Nil
/Location	nan Temp		arse id Limit			-	· ·	-	- 0	-	· ·		0	-	'	-		- 0		'		0
Chainage/Location	Near Hanuman Temple	ned	Gravel ne					-	0	1			2			-	1	-			1	2
		Grain Size Distribution % wt retained	arse	:0D					9	,			5					4				Э
<u>ള</u>	09-05-2023	ibution %	Sand muit	bəM					9	,			5				,	5		,	,	∞
Date of Boring	to	ize Distri	əuj	ĿЛ					71	,			67				,	68			,	65
Dat	07-05-2023	Grain S	His	1					17				21					22				22
	07-05	Clay	I	ı	ı		0	ı	ı	1	0	ı	'		ı	0	ı		ı	0		
i Pood	" NOau		I																			
ridor from Bad	ation at Jaipur.						SM			·	SM				ı	SM		ı	ı	SM		
ttion work for Extension of E-W cor	roject Cuouper to Hansport vaget (2.03km) Phase-1C and Mansatova to Ajnict Noad (Chauraha) (1.35km) Phase-1D of Jaipur Metro Rail Corporation at Jaipur."		Soil Description														Very dense, brownish, Silty sand					
.l Investiga	.35km) Ph		(N) rrected SI Value (V _e)		ı	43	46	ı	49	51		- 0	- 0	ı	- 0	- 0	ı	- 0	- 0	1	- 0	- 0
-technica	uper to 1. turaha) (1		V TQ2 b9v			50 74	00 82	- 00	50 91	66 00	- 00	50 >100	00 >100	- 00	50 >100	00 >100	- 00	50 >100	00 >100	- 00	50 >100	00 >100
"Geo	(Cha		AVE All		PDS* 19.00	SPT-12 19.50	SPT-13 21.00	UDS* 22.00	SPT-14 22.50	SPT-15 24.00	UDS* 25.00	SPT-16 25.50	SPT-17 27.00	UDS* 28.00	SPT-18 28.50	SPT-19 30.00	UDS* 31.00	SPT-20 31.50	SPT-21 33.00	UDS* 34.00	SPT-22 34.50	SPT-23 36.00
	<u> </u>	Jelpur Ar	(m)	ctor ect)		LdS	LdS		LdS	LdS	1	5 of 12			SP1	LdS		LdS	LdS		LdS	SP1



a)	-24		ι	10issərqmoD Index (C.)	ı	ı	ı	ı
Ref. Code	SR-837_23-24	rameters		(53/ ₇ w2) 7. ^{01 x ^} W	1	ı	ı	I
	SF	tion Pa		(cm ² /Sec)	-	-	-	I.
j	910	Consolidation Parameters		Pressure Pressure	ı	I	ı	ı
R.L.	+463.910	U	(0	9) oita Ratio (e	ı	ı	ı	ı
	Е	Â		idrəmrə¶ 998\mɔ)	-	-	-	ı
	2977091.000 m	nı.ç		Swelling Pro ⁷ m3/2d		T		I
(E,N)	2977	xəp	ouj	Free Swell] (%)	1	1	ı	1
Cordinates (E,N)		4	(Angle of (°q) noitoirT	ı	1	31	ı
Col	584164.000 m	Shear Strength		Cohesion C (kg/cm²)	ı	ı	0.07	I
	58416	Shear		rs9T to 9qvT			DST+	,
ion		ity	vb	1D office Gr	ı	1	2.65 I	ı
Termination Depth	40.00 m	(ູພວ	/ 8)	Dry Density (1.70	
		(%) tnstnoJ		-	13.34 1.	
of Water Table	Encountered			Bulk Density Matural Mo			1.93 13	
Depth of V	Not Enc	`£ ′	,	timiJ			- 1.	
		its %		xəbnl Shrinkage				
B.H. No.	BH-TN Alignment-03	Atterberg Limits %		Plasticity		1	L	'
B		Atterbe	1	himi. Line and a starte Line and a starte a star	1	ı	22	1
ocation	Near Hanuman Temple		1	imiJ biupiJ	I	I	29	I
Chainage/Location	Hanuma		Gravel	Coarse	ı	ı	0	ı
Ch	Near	retained	9	AniT	ı	I	1	1
	09-05-2023	n % wt		Coarse	I	I	3	I
ring	0-60	stributio	Sand	muibəM	1	1	9	1
Date of Boring	to	Grain Size Distribution % wt retained		9ni'T		1	55	1
ũ	07-05-2023	Grair		11!S	'	ı	30	'
	07-0;			Clay		ı	5	'
bood	L'NOAU		ю	dmy2 21				
r from Badi	a w Ajmer n at Jaipur.'	uoj	ite	IS Classific	I	ı	SM-SC	
"Geo-technical Investigation work for Extension of E-W corridor from Badi	спочрет ю дтальрон мадац (ж.о.м.п) глаже -1.С ани мальатома ю длист. (Chauraha) (1.35km) Phase-1D of Jaipur Metro Rail Corporation at Jaipur."			Soil Description			Very dense, brownish, Clayey silty	sand
Investig:	(5km) PE			Corrected Value (V	ı	I	ı	ı
schnical .	er to 11a aha) (1.3	ənlaV	L ۱	(N) Observed SP7	ı	>100	>100	>100
"Geo-te	(Chaur	(w) "	1.3	Depth from C	37.00	4 37.50	39.00	SPT-26 40.00
Ducion	rrojec	1	ax V	Rallacora	*SOA	SPT-24	SPT-25	SPT-26
		Julpur M		Director (Project)	inon.			





Ref. Code	SR-837_22-23	ameters	M _{v x} 10 ⁻² Compression Compression (Co		1		•		1	1	1		1	1	1	1	•	1	1	1	,
×	SR-	tion Par	(cm ² /Sec) C ^x x 104											-							
Ŀ	59	Consolidation Parameters	(kg/cm ²⁾ Pressure	ı																	
R.L.	+464.859		(₀ 9) oitsA bioV	. 1	ı	ı		ı	I	ı	ı	ı	ı	-	-	I	ı	ı	ı	I	ı
	.000 m	Â	Permeabilit (cm/sec)	,																	,
0	2977289.000 m	n.e	(kg/cm ²)	ı	1	1		1	1	1	'	1	1	1		1	ı	1	1	1	'
Cordinates (E,N)		xəp	Friction (q°) Free Swell In (%)	ı	'	'	'	'	'	'	'	'	'	'		'		'	'	'	'
Cordin	00 m	ength	ु,	1	'	0 29	'	1	0 30	'	'	0 30	'	'	0 31	'	1	0 31	'	'	0 31
	584201.000 m	Shear Strength	O noisentoO	1	'	Г 0.00	'	1	Г 0.00	'	'	Г 0.00	'	'	r 0.00	'	1	Г 0.00	'	'	r 0.00
		•2	ts9T to 9qVT	ı	1	DST	1	1	DST	'	'	DST	1	'	DST	1	ı	DST	'	1	DST
Termination Depth	40.00 m	ţţ	vraD offio9q2	ı	1	2.62		1	2.62	'	'	2.63	1	'	2.63	1		2.63	'	1	2.63
	4(Dry Density (g/	·	'	1.62	'	' 	1.63	'	'	1.63	'	,	1.64	'	'	1.65	,	'	1.65
ter Table	ntered		tsioM IsrutsN %) tnotnoO	ı	'	8.69			8.71	'	'	8.72	'	'	8.73	'		8.81	'	'	8.82
Depth of Water Table	Not Encountered	(_e mə/	Bulk Density (g	· ·	'	1.76	'	'	1.77	'	'	1.77	'	'	1.78	'	'	1.80	'	'	1.80
Dept	Ż	\$ %	Shrinkage Shrinkage Limit	ı	,		,	,	'	'	,	,	,			,		'	,	,	•
B.H. No.	TN-04	Atterberg Limits %	Plasticity Index	1	'	ď	'	'	ďN	'	'	đ	'	,	ΑN	'	'	ďN	,	'	đ
B.	L	Atterbe	Plastic Limit	'	'	Nil	'	'	Nil	'	•	Nil	'	'	Nil	'		Nil	'	'	Nil
ocation	i Mandi		Liquid Limit	1					,	,	,			1	1	,		,	,	,	'
Chainage/Location	Near Krishi Mandi	ğ	Coarse Coarse	,	'	0	'	'	0	'		0	'		0	'	'	0		'	C
C		Grain Size Distribution % wt retained	aniN	'	·	0	'	'	0		•	0	·		0 /	'	'	0		'	0
	15-05-2023	tion % w	Coarse	-	'	19 6	'	'	15 8	'	'	1 5	'	'	7 7	'	'	10 2	'	'	1 2
Date of Boring	to 15	Distribu	əniA MuibəM	· ·		60 15	'		61 15			66 11			68 7			70 10			71 11
Date of		rain Size	nis	, , , , , , , , , , , , , , , , , , ,		15 6			16 6			18 6			18 6			18 7			16 7
	11-05-2023	0	Clay	1		0			0			0			0			0			0
ad			lodmy2 21																		
idor from Badi ovar to Aimer Ro	ition at Jaipur."	uoj	IS Classificat		1	SM	1	1	SM	1	1	SM	1	1	SM		1	SM	1		SM
"Geo-technical Investigation work for Extension of E-W corridor from Badi Project Chouser to Transport Nazar 2, 85km) Phase - JC and Mansarovar to Aimer Road	se-1D of Jaipur Metro Rail Corpor.		Soil Description	Filled up soil														Dense, brownish, Silty sand			
Investigati nsport Nag	Skm) Pha		Corrected SI (₀ N) sulue (N ₀)	ı	43	ı	25	39	ı	40	35	ı	45	45		36	39	1	40	41	,
-technical per to Trai	uraha) (1.5		VD56176d SPT V (N)	-	0 36	- 0	0 23	0 40	- 0	0 44	0 42	- 0	0 57	09 00	- 0	0 51	0 58	- 0	0 62	0 67	- 0
"Geo-	(Chai		L.Ə morî diye	0	T-1 3.00	S-1 4.00	T-2 4.50	SPT-3 6.00	S-2 7.00	T-4 7.50	T-5 9.00	S-3 10.00	SPT-6 10.50	T-7 12.00	S-4 13.00	T-8 13.50	T-9 15.00	S-5 16.00	C-10 16.50	C-11 18.00	S-6 19.00
Proi		Jelpur Areco	Director	-iion	SPT-1	UDS-1	SPT-2	LdS	UDS-2	SPT-4	SPT-5	UDS-3	LdS	SPT-7	UDS-4	SPT-8	6-TqS	UDS-5	SPT-10	SPT-11	UDS-6
		121	(Project) JAIPUR	*						87	' of 12	5									



Project	"Geo-te t Choupe (Chanra	technical Investig ter to Transport N raha) (1.35km) Ph	"Geo-technical Investigation work for Extension of E-W corridor from Badi "Geo-technical Investigation work for Extension of E-W corridor from Badi Project Chouper to Transport Nagar (2.85km) Phase -1C and Mansarovar to Ajmer Road (Channeha) (1.35km) Phase-1D of Jainnr Merro Rail Cornoration at Jainnr "	or from Badi 'ar to Ajmer Road m at Taimur "		Date of	Date of Boring		Chains	Chainage/Location		B.H. No.	Depth o	Depth of Water Table		Termination Depth			Cordina	Cordinates (E,N)			R.L.	-	Ref. Code
	Cullaur	л (шисст) (впви	liase-11) of Jaipur Micu o Kall Corporate	on at Jaipur.	11-05-2023		to 15-	15-05-2023	Near F	Near Krishi Mandi		TN-04	Not F	ot Encountered	pe	40.00 m		584201.000 m	0 m	29	2977289.000 m		+464.859	SR	SR-837_22-23
	(w) "	Τq				Grain Size	Distribut	Grain Size Distribution % wt retained	etained.		Atterb	Atterberg Limits %	%		(Shear Strength	ngth				Consoli	Consolidation Parameters	ameters.
ARAIL Cor	Depth from G.L	V TYS US (N) (V) Corrected SI Corrected SI (V,)	Soil Description	IS Classificati	Clay	nis	Sad Medium	Coarse	Fine Gravel	Coarse	Liquid Limit Plastic Limit	Plasticity Index	Shrinkage Limit	g) ytiensd Mua	tsioM lautaN %) tn9tn0D	Dry Density (g/	Specific Grav Type of Test) noisəho Cohesion (Kg/cm ²)	Angle of Friction (φ°)	Free Swell Inc (%)	Swelling Press (kg/cm²) Permeabilit	(cm/sec) Void Ratio (e ₀)	(k&\cm ³⁾ Pressure	(cw ₅ /26c) C ^A X 10 ₄	Compression (cm ² /Kg)
SeT-12 19	19.50				1			ı	1	,	1	,	ı				, ,	'		,			,		
SPT-13 2	21.00	0 78 44			T		1	I	1			,	1		1	I		1	ı	1		ı	ı	1	1
23	22.00				ı			ı	,			,	1			1	'	,		,		1	ı	,	
SPT-14 22	22.50	0 82 44					-									1		'	'			ı		ı	
SPT-15 24	24.00	98 6 44		SM	0	19 7.	73 4	4	0	0	- Nil	dv I	,	1.81	8.85 1	1.66 2	2.64 DST+	+ 0.00	31						
5	25.00	-	T				· ·						,		1	1	'	1	,			ı		ı	1
SPT-16 25	25.50	0 92 45	T				· ·				•				1		· ·	'	,			ı	1	ı	1
SPT-17 27	27.00	92 44					•	,			•		,				'	'			•		1		
28	28.00	-		1 - 1 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 -	1	, ,		1	1		,	'	1					'					,		
SPT-18 28	28.50	96 44		101020100000 001000000 001000000	1			1	1		,	'	1				·	'					,		
SPT-19 30	30.00	0 >100 -		SM	0	13 7.	75 11	1	0	0	- Nil	I NP	1	1.84	8.86 1	1.69 2	2.64 DST+	+ 0.00	33	,	•	,	'	1	
3]	31.00	-			1			1			•		1					'						1	
SPT-20 3	31.50	0 >100 -		10102400000 0020000000 0000000000 000000000				1				'	1				'	1							
SPT-21 3	33.00	0 >100 -	T								•				1	1		'	'	1	•		1	ı	1
ň	34.00	-		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1		•	1	'		•	'	1				'	'			•		'	,	
SPT-22 3.	34.50	0 >100 -	Very dense, brownish, Silty sand	SM	0	13 7.	75 9	n	0	0	- Nil	I NP	,	1.84	9.12 1	1.69 2	2.64 DST+	+ 0.00	33		•	,	'		
SPT-23 3	36.00	0 >100 -			1	,		,	1		,	'	,					'	'	,			'	ı	
	37.00	-						,			,		,				·	'	'	,	•	,	'	,	
4			-			-									-	-	-		-			_			-



	23		ι	Compression Index (C,)	ı	ı	ı
Ref. Code	SR-837_22-23	meters		(cm ² /Kg) M ^{2 x} 10 ⁻²			,
Rc	SR-8	on Para		(cm ² /Sec) C ^A x 10 ⁴	,		,
		Consolidation Parameters		Pressure			ı
R.L.	+464.859	C	(0	9) oita Ratio (e			
			(oəs/wə)			
	2977289.000 m		(Swelling Pro mo/gy) Permeabi			
(E,N)	2973			Free Swell (%)			
Cordinates (E,N)				fo slgnA (°\$) noitsirA		1	ı
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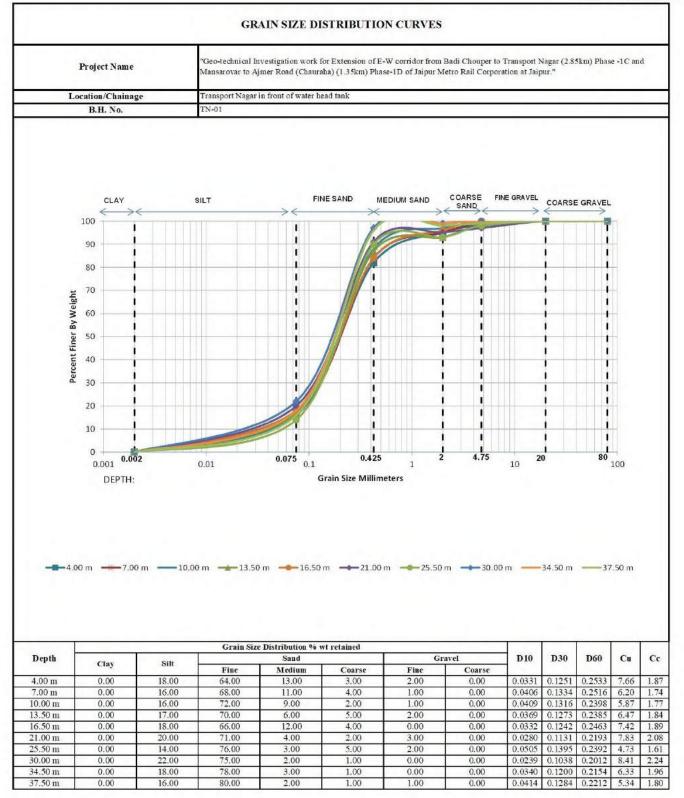
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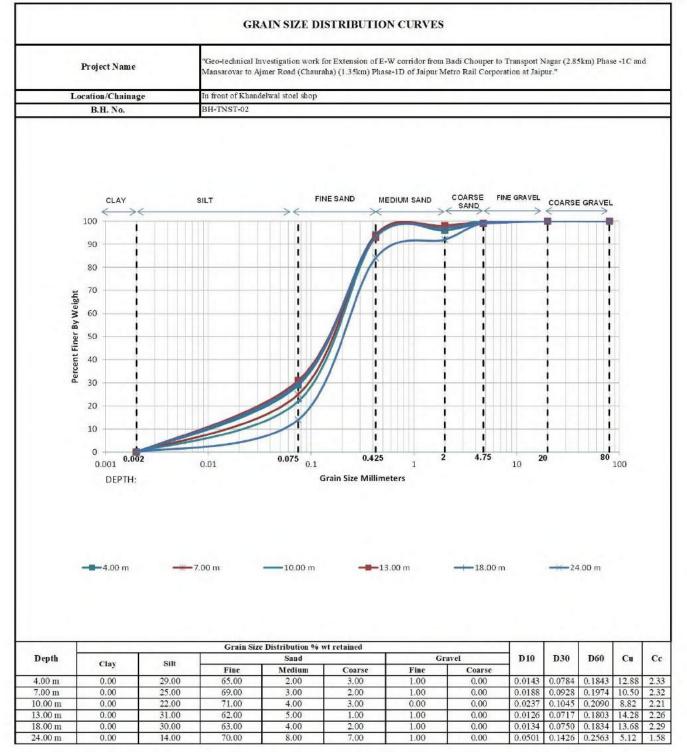






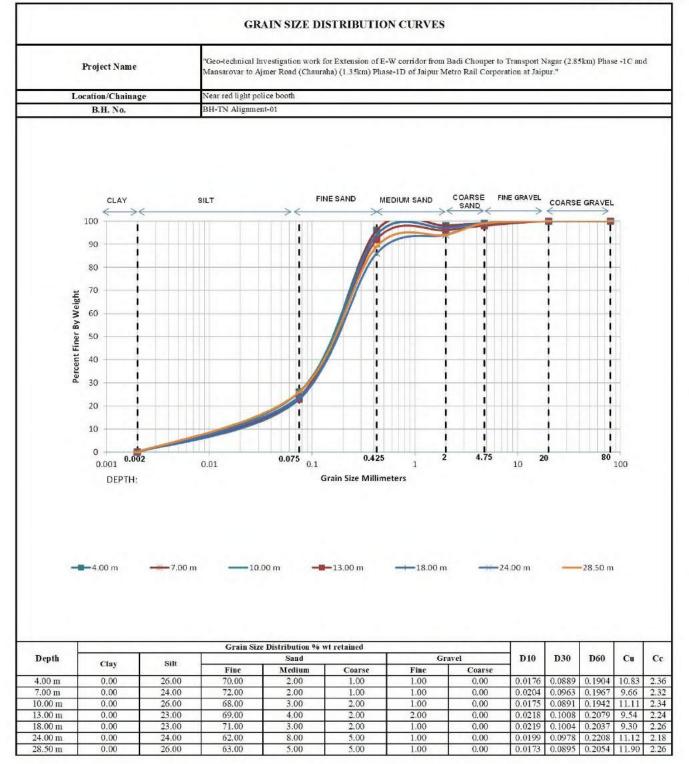






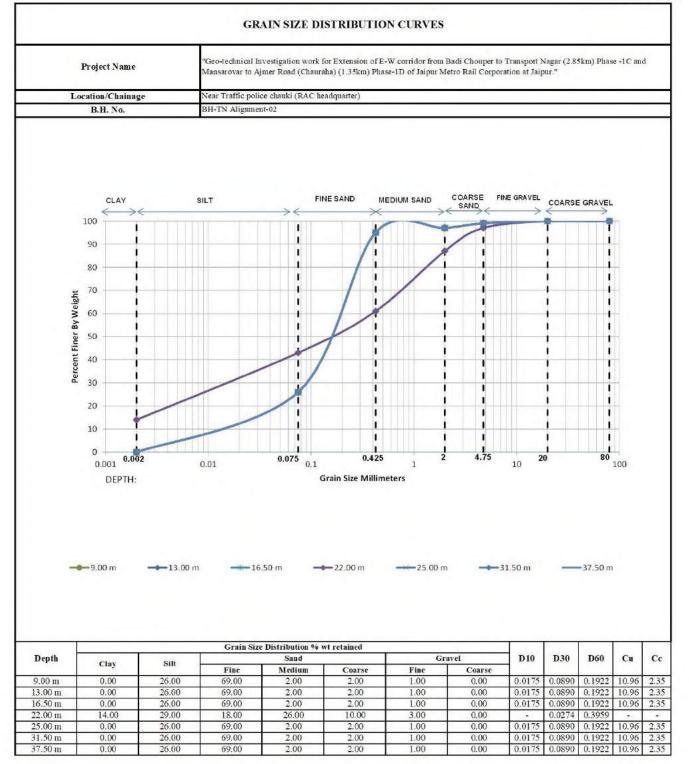






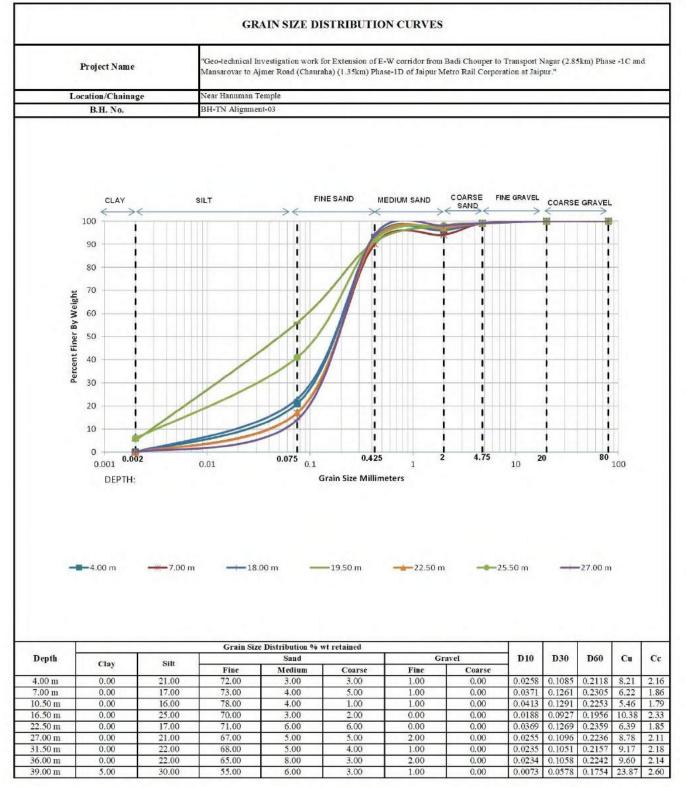






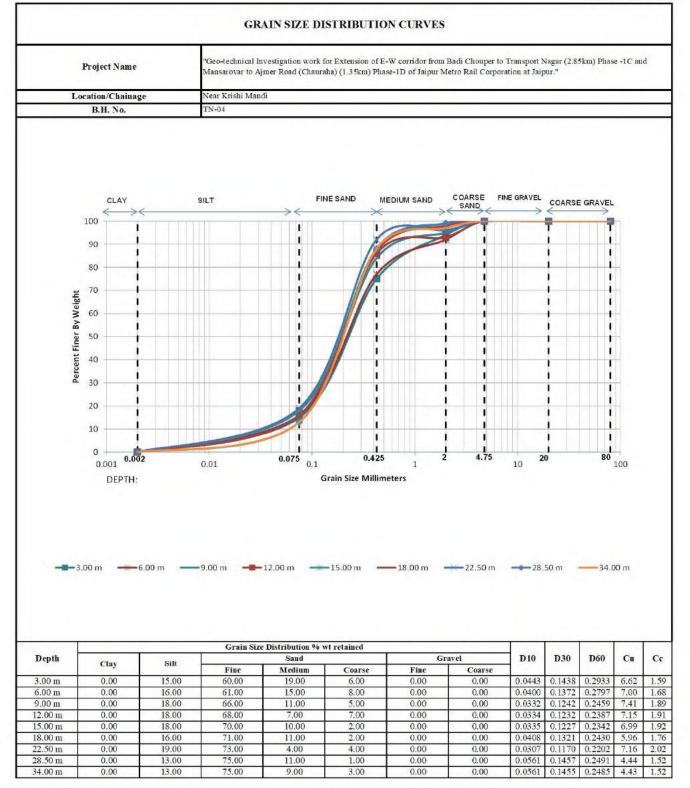








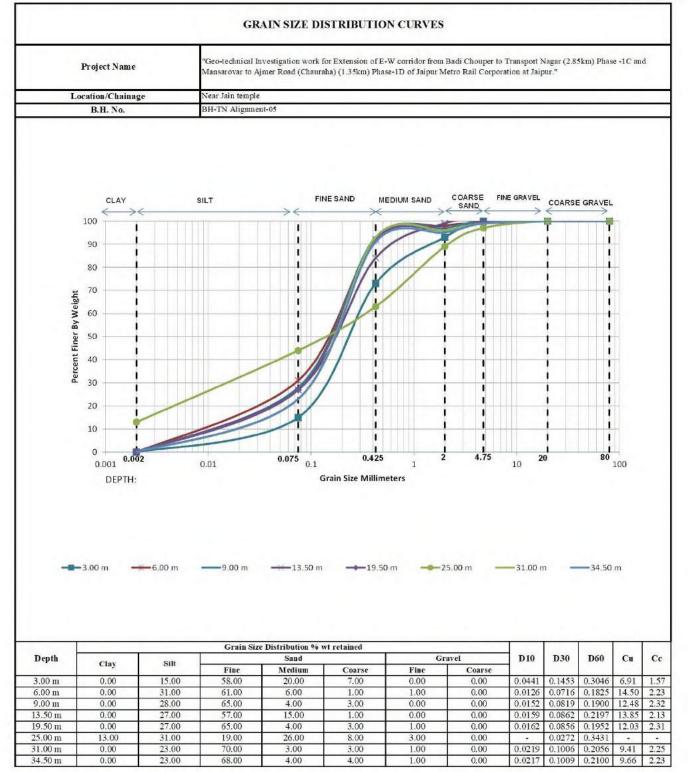








Rail Corp







Geo-technical Investigation work for Extension of underground and elevated section E-W Corridor from Badi Chouper to Transport Nagar (2.85Km) Phase-1C and Mansarovar to Ajmer Road (Chauraha) (1.35 km) Phase-1D of Jaipur Metro Rail Corporation at Jaipur.

APPENDIX B-3

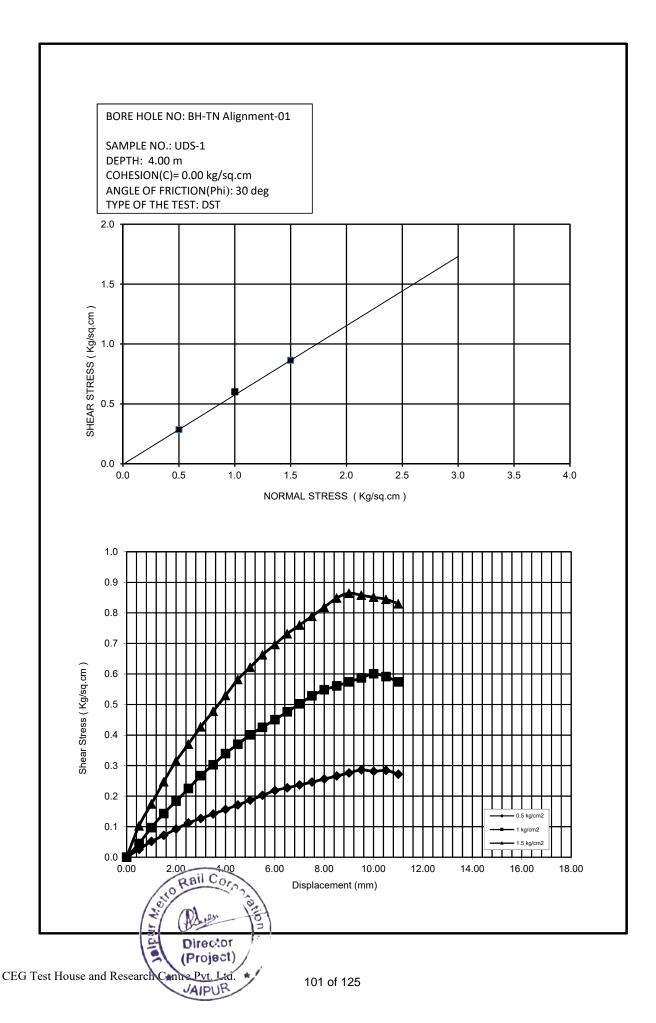
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2	TN Alignment- 04	4.50	8.24	31.27	0.0031	24.69	0.0025
3	TN Alignment- 05	3.00	8.21	38.22	0.0038	28.81	0.0029

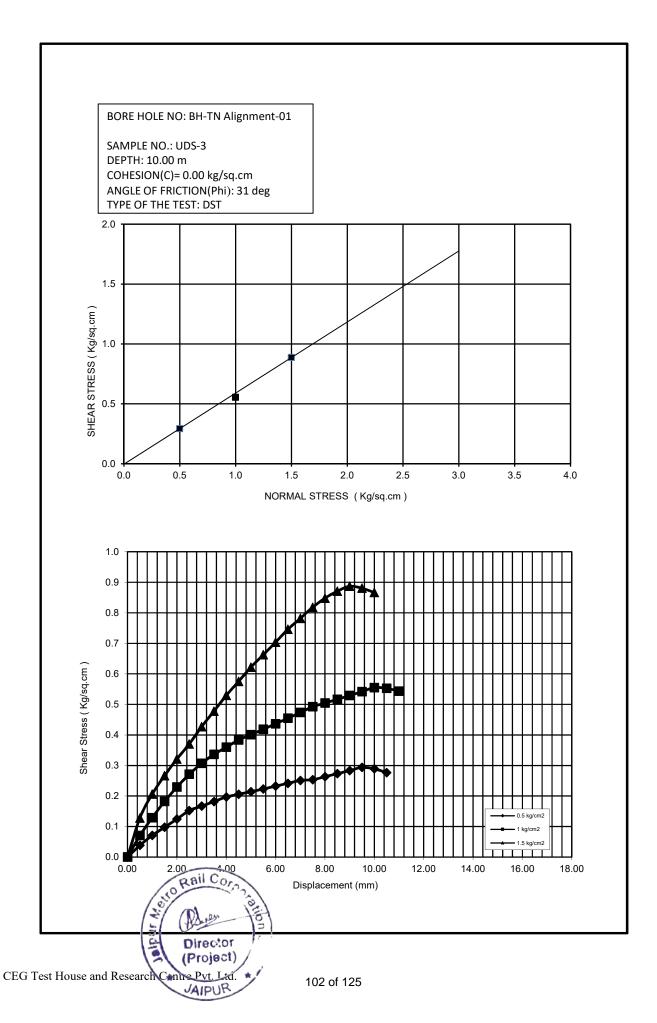
RESULTS OF CHEMICAL ANALYSIS OF SOIL SAMPLES











Geo-technical Investigation work for Extension of underground and elevated section E-W Corridor from Badi Chouper to Transport Nagar (2.85Km) Phase-1C and Mansarovar to Ajmer Road (Chauraha) (1.35 km) Phase-1D of Jaipur Metro Rail Corporation at Jaipur

APPENDIX – C (ANALYSIS & RECOMENDATION)

Appendix No.	ITEMS
C-1	CALCULATION FOR COMPUTATION OF LIQUEFACTION POTENTIAL
C-2	SAMPLE CALCULATION FOR COMPUTATION OF ALLOWABLE BEARING CAPACITY OF SUB-STRATA FOR SHALLOW FOUNDATION RESTING ON SOIL
C-3	SAMPLE CALCULATION FOR COMPUTATION OF SAFE LOAD CARRYING CAPACITY OF NORMAL BORED CAST-IN-SITU RCC PILE IN COMPRESSION & UPLIFT
C-4	SAMPLE CALCULATION FOR COMPUTATION OF SAFE LOAD CARRYING CAPACITY OF NORMAL BORED CAST-IN-SITU RCC PILE IN LATERAL





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INPUT DAT	TA		Elevated
			BH-TNAL-02
Type of foo	ting		
1 C	Continuous Strip		
2 R	Rectangular	Rectangular	2
3 S	Square		
4 C	Circular		
Angle of int	ternal friction (ϕ°)		31.4
Cohesion (c in t/m²)		0.0
√oid ratio (e	e), e = (G.γ _w /γ _d)-1		0.6
Direction of	f load with vertical (°)		0.0
Density of f	foundation soil (t/m³) γ _{bulk}		1.7
Depth of wa	ater table(m)		0.0
Factor of sa	afety		2.5
S.no.	Depth (m) of footing (D_f) below EGL	Width (m)	Length (m)
1	3.00	4.00	5.00
		0.00	0.00
		0.00	0.00
		0.00	0.00
		0.00	0.00
Assumption	NILURE CRITERIA Ins and formula used in calculation as per IS: a type of failure used for bearing capacity an	-	oid ratio (see IS
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Assumption NOTE: The 5403 : 1981 The ultimate 3) The ultimate (Mhere, d d d Mhere, d d d Mhere, d d d d Mhere, d d d d Mhere, d d d d d d d d d d d d d d d d d d d	The sand formula used in calculation as per IS: a type of failure used for bearing capacity and 1, Page No. 9, Table No. 3). The net bearing capacity in case of general shall $d_d = c N_c s_c d_c i_c + q (N_q-1) s_q d_q i_q + (1/2) B \gamma I$ the net bearing capacity in case of local shear $d_d = (2/3) c N'_c s_c d_c i_c + q (N'_q-1) s_q d_q i_q + (1/2) I_q = (1/3) c N'_c s_c d_c i_c + q (N'_q-1) s_q d_q i_q + (1/2) I_q = (1/3) c N'_c s_c d_q + (1/2) I_q + (1/2) I_q = (1/3) c N'_c s_c d_q + (1/2) I_q + (1/$	alysis depends upon the value of vo ear failure is given by (from IS 6403 $N_{\gamma}s_{\gamma}d_{\gamma}i_{\gamma}W'$ r failure is given by (from IS 6403 : 1 2) B γ N' $_{\gamma}s_{\gamma}d_{\gamma}i_{\gamma}W'$ (from IS 6403 : 1 1 (0.67 tan ϕ)	: 1981, page No 981, page No. 8
Assumption NOTE: The 5403 : 1981 The ultimate 3) q The ultimate Q Where, d d d M b CUTPUT The compu nterpolated	The sand formula used in calculation as per IS: a type of failure used for bearing capacity and 1, Page No. 9, Table No. 3). The net bearing capacity in case of general shall $d_d = c N_c s_c d_c i_c + q (N_q-1) s_q d_q i_q + (1/2) B \gamma I$ the net bearing capacity in case of local shear $d_d = (2/3) c N'_c s_c d_c i_c + q (N'_q-1) s_q d_q i_q + (1/2) I_c = 1 + 0.2 (D_f/B)*SQRT(N_\phi)$ $d_q = d_\gamma = 1 \text{ for } \phi < 10^\circ$ $d_q = t_q = 1 + 0.1 (D_f/B)*SQRT(N_\phi) \text{ for } \phi > 10^\circ$ $d_q = tan^2(\pi/4 + \phi/2)$ T is friction angle for local shear failure = tan	alysis depends upon the value of volue ear failure is given by (from IS 6403 $N_{\gamma}s_{\gamma}d_{\gamma}i_{\gamma}W'$ failure is given by (from IS 6403 : 1 2) B γ N' $_{\gamma}s_{\gamma}d_{\gamma}i_{\gamma}W'$ (from IS 6403 : 1 1 (0.67 tan ϕ)	: 1981, page No 981, page No. 8
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Assumption NOTE: The 5403 : 1981 The ultimate 3) q The ultimate Q Where, d d d M b CUTPUT The compu nterpolated	The sand formula used in calculation as per IS: a type of failure used for bearing capacity and 1, Page No. 9, Table No. 3). The net bearing capacity in case of general shall $d_d = c N_c s_c d_c i_c + q (N_q-1) s_q d_q i_q + (1/2) B \gamma I$ the net bearing capacity in case of local shear $d_d = (2/3) c N'_c s_c d_c i_c + q (N'_q-1) s_q d_q i_q + (1/2) I_q = (1/3) c N'_c s_c d_c i_c + q (N'_q-1) s_q d_q i_q + (1/2) I_q = (1/3) c N'_c s_c d_q + (1/2) I_q + (1/2) I_q = (1/3) c N'_c s_c d_q + (1/2) I_q + (1/$	alysis depends upon the value of volue ear failure is given by (from IS 6403 $N_{\gamma}s_{\gamma}d_{\gamma}i_{\gamma}W'$ failure is given by (from IS 6403 : 1 2) B γ N' $_{\gamma}s_{\gamma}d_{\gamma}i_{\gamma}W'$ (from IS 6403 : 1 1 (0.67 tan ϕ)	: 1981, page No 981, page No. 8
Assumption NOTE: The 5403 : 1981 The ultimate 3) q The ultimate Q Where, d d d M b CUTPUT The compu nterpolated	The sand formula used in calculation as per IS: a type of failure used for bearing capacity and 1, Page No. 9, Table No. 3). The net bearing capacity in case of general shall $d_d = c N_c s_c d_c i_c + q (N_q-1) s_q d_q i_q + (1/2) B \gamma I$ the net bearing capacity in case of local shear $d_d = (2/3) c N'_c s_c d_c i_c + q (N'_q-1) s_q d_q i_q + (1/2) I_q = (1/3) c N'_c s_c d_c i_c + q (N'_q-1) s_q d_q i_q + (1/2) I_q = (1/3) c N'_c s_c d_q + (1/2) I_q + (1/2) I_q = (1/3) c N'_c s_c d_q + (1/2) I_q + (1/$	alysis depends upon the value of volue ear failure is given by (from IS 6403 $N_{\gamma}s_{\gamma}d_{\gamma}i_{\gamma}W'$ failure is given by (from IS 6403 : 1 2) B γ N' $_{\gamma}s_{\gamma}d_{\gamma}i_{\gamma}W'$ (from IS 6403 : 1 1 (0.67 tan ϕ)	: 1981, page No 1981, page No. 8



Director (Project) TRE PVT. LTD

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¢		31.42		φ'		22.26
N _c		33.81		N' _c		17.17
N _q		21.65		N' _q		8.03
Νγ		27.67		Ν' _γ		7.39
hape fa	ctors : (from IS	<u> 6403 : 1981, j</u>	page No. 8, Tab	ole No. 2)		
S.no.	Width(m)	Length (m)		Sc	Sq	Sγ
1	4.00	5.00		1.16	1.16	0.68
	0.00	0.00				
	0.00	0.00				
	0.00	0.00				
	0.00	0.00				
epth fa	ctors : (from IS	6403 : 1981, p	oage No. 9)			
S no	Donth(m)	Width(m)		da	d	d
S.no. 1	Depth(m) 3.00	Width(m) 4.00		dc 1.27	<i>d</i> _q 1.13	<i>d</i> _γ 1.13
		0.00				
		0.00				
		0.00				
	$i_c = (1 - \alpha / 90)^2$		$i_q = (1 - \alpha / 90)^2$			$i_{\gamma} = (1 - \alpha / \phi)^2$
		om IS 6403 : 19	-			$i_{\gamma} = (1 - \alpha / \phi)^2$ 1.00
	$\frac{i_c = (1 - \alpha / 90)^2}{1.00}$	om IS 6403 : 19	$i_q = (1 - \alpha / 90)^2$			
ater tal	$\frac{i_c = (1 - \alpha / 90)^2}{1.00}$	om IS 6403 : 19	$i_q = (1 - \alpha / 90)^2$ 1.00			
ater tal	$\frac{i_c = (1 - \alpha / 90)^2}{1.00}$	m IS 6403 : 19	$i_q = (1 - \alpha / 90)^2$ 1.00	· · · · · · · · · · · · · · · · · · ·		1.00
ater tal	i _c = (1-α / 90) ² 1.00 Dele factor : (fro Depth(m)	m IS 6403 : 19 m IS 6403 : 19 Width(m)	$i_q = (1 - \alpha / 90)^2$ 1.00	Z _w /B		1.00 W'
ater tal	i _c = (1-α / 90) ² 1.00 Dele factor : (fro Depth(m)	m IS 6403 : 19 m IS 6403 : 19 Width(m) 4.00	$i_q = (1 - \alpha / 90)^2$ 1.00	Z _w /B		1.00 W'
ater tal	i _c = (1-α / 90) ² 1.00 Dele factor : (fro Depth(m)	m IS 6403 : 19 m IS 6403 : 19 Width(m) 4.00 0.00	$i_q = (1 - \alpha / 90)^2$ 1.00	Z _w /B		1.00 W'
ater tal	i _c = (1-α / 90) ² 1.00 Dele factor : (fro Depth(m)	m IS 6403 : 19 m IS 6403 : 19 Width(m) 4.00 0.00 0.00	$i_q = (1 - \alpha / 90)^2$ 1.00	Z _w /B		1.00 W'
<mark>ater tal</mark> S.no. 1	i _c = (1-α / 90) ² 1.00 Dele factor : (fro Depth(m)	m IS 6403 : 19 m IS 6403 : 19 Width(m) 4.00 0.00 0.00 0.00 0.00	$i_q = (1 - \alpha / 90)^2$ 1.00	Z _w /B		1.00 W'
[/] ater tal S.no. 1 afe Bea	i _c = (1-α / 90) ² 1.00 ble factor : (fro Depth(m) 3.00	m IS 6403 : 19 m IS 6403 : 19 Width(m) 4.00 0.00 0.00 0.00 0.00	i _q = (1-α / 90) ² 1.00 81, page No. 9)	Z _w /B	SBC in (t/m ²)	1.00 <u>W</u> " 0.50
[/] ater tal S.no. 1 afe Bea	i _c = (1-α / 90) ² 1.00 De factor : (fro Depth(m) 3.00 ring Capacity	m IS 6403 : 19 m IS 6403 : 19 Width(m) 4.00 0.00 0.00 0.00 0.00	$i_q = (1 - \alpha / 90)^2$ 1.00	Z _w /B	SBC in (t/m²) Local shear	1.00 <u>W'</u> 0.50
[/] ater tal S.no. 1 afe Bea	i _c = (1-α / 90) ² 1.00 De factor : (fro Depth(m) 3.00 ring Capacity	m IS 6403 : 19 m IS 6403 : 19 Width(m) 4.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	<u>i_q = (1-α / 90) ²</u> 1.00 81, page No. 9) Length (m) 5.00	Z _w /B -0.75	. ,	1.00 <u>W</u> " 0.50
ater tal S.no. 1 afe Bea S.no.	i _c = (1-α / 90) ² 1.00 ble factor : (fro Depth(m) 3.00 ring Capacity Depth(m)	m IS 6403 : 19 m IS 6403 : 19 Width(m) 4.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	i _q = (1-α / 90) ² 1.00 81, page No. 9) 81, page No. 9 81, page No. 10 81, page No. 10 10, 	Z _w /B -0.75 General shear	Local shear	1.00 W' 0.50
ater tal S.no. 1 afe Bea S.no.	i _c = (1-α / 90) ² 1.00 ble factor : (fro Depth(m) 3.00 ring Capacity Depth(m)	m IS 6403 : 19 m IS 6403 : 19 Width(m) 4.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	<u>i_q = (1-α / 90) ²</u> 1.00 81, page No. 9) 81, page No. 9) 81, page No. 9 81, page No. 	Z _w /B -0.75 General shear	Local shear	1.00 W' 0.50
<u>ater tal</u> S.no. 1 afe Bea S.no.	i _c = (1-α / 90) ² 1.00 ble factor : (fro Depth(m) 3.00 ring Capacity Depth(m)	m IS 6403 : 19 m IS 6403 : 19 Width(m) 4.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	<u>i_q = (1-α / 90) ²</u> 1.00 81, page No. 9) 81, page No. 9) 81, page No. 9 81, page No. 10 81, page No. 10 10, page No. 10, page 	Z _w /B -0.75 General shear	Local shear	1.00 W' 0.50
<u>ater tal</u> S.no. 1 afe Bea S.no.	i _c = (1-α / 90) ² 1.00 ble factor : (fro Depth(m) 3.00 ring Capacity Depth(m)	m IS 6403 : 19 m IS 6403 : 19 Width(m) 4.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	<u>i_q = (1-α / 90) ²</u> 1.00 81, page No. 9) 81, page No. 9) 81, page No. 9 81, page No. 	Z _w /B -0.75 General shear	Local shear	1.00 W' 0.50 Recommended
Arr tal S.no. 1 afe Bea S.no. 1 0TE: 1/	<u>i_c = (1-α / 90)²</u> 1.00 ble factor : (fro <u>Depth(m)</u> 3.00 ring Capacity Depth(m) 3.00	m IS 6403 : 19 m IS 6403 : 19 Width(m) 4.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	<u>i_q = (1-α / 90) ²</u> 1.00 81, page No. 9) 81, page No. 9) 81, page No. 9) 81, page No. 9 81, page No. 10, page No. 10, 	Z _w /B -0.75 General shear	Local shear 12.89	1.00 W' 0.50 Recommended 29.71





NPUT DA	<u>TA</u>		Elevated	
			BH-TNAL-02	
Type of foo	oting			
1 C	Continuous Strip			
2 F	Rectangular	Rectangular	2	
3 S	Square			
4 C	Circular			
Angle of int	ternal friction (ϕ°)		31.1	
Cohesion (0.0	
/oid ratio ((e), $e = (G.\gamma_w/\gamma_d)-1$		0.6	
Direction of	f load with vertical (°)		0.0	
Density of f	foundation soil (t/m³) γ _{bulk}		1.7	
-	ater table(m)		0.0	
Factor of sa	afety		2.5	
S.no.	Depth (m) of footing (D_f) below EGL	Width (m)	Length (m)	
1	4.00	4.00	5.00	
		0.00	0.00	
		0.00	0.00	
		0.00	0.00	
		0.00	0.00	
Assumptior	AILURE CRITERIA ns and formula used in calculation as per IS		oid ratio (see IS	
Assumptior NOTE: The 5403 : 198 ⁻ The ultimat		alysis depends upon the value of vo		
Assumptior NOTE: The 6403 : 198′ The ultimat 3)	ns and formula used in calculation as per IS e type of failure used for bearing capacity an 1, Page No. 9, Table No. 3).	alysis depends upon the value of vo		
Assumptior NOTE: The 6403 : 198 ⁷ The ultimat 3) q	ns and formula used in calculation as per IS e type of failure used for bearing capacity an 1, Page No. 9, Table No. 3). te net bearing capacity in case of general sh $q_d = c N_c s_c d_c i_c + q (N_q-1) s_q d_q i_q + (1/2) B \gamma$	alysis depends upon the value of voluear failure is given by (from IS 6403 $N_{\gamma}s_{\gamma}d_{\gamma}i_{\gamma}W'$	3 : 1981, page No	
Assumptior NOTE: The 6403 : 1987 The ultimat 3) q The ultimat	ns and formula used in calculation as per IS e type of failure used for bearing capacity an 1, Page No. 9, Table No. 3). te net bearing capacity in case of general sh	alysis depends upon the value of voluear failure is given by (from IS 6403 $N_{\gamma}s_{\gamma}d_{\gamma}i_{\gamma}W'$ r failure is given by (from IS 6403 : ·	3 : 1981, page No	
Assumptior NOTE: The 5403 : 198' The ultimat 3) The ultimat q Where,	Ins and formula used in calculation as per IS e type of failure used for bearing capacity an 1, Page No. 9, Table No. 3). te net bearing capacity in case of general sh $a_d = c N_c s_c d_c i_c + q (N_q-1) s_q d_q i_q + (1/2) B \gamma$ te net bearing capacity in case of local shea $a_d = (2/3) c N'_c s_c d_c i_c + q (N'_q-1) s_q d_q i_q + (1/2)$	alysis depends upon the value of voluear failure is given by (from IS 6403 $N_{\gamma}s_{\gamma}d_{\gamma}i_{\gamma}W'$ r failure is given by (from IS 6403 : ·	3 : 1981, page No	
Assumptior NOTE: The 5403 : 198' The ultimat 3) The ultimat Q Where, d	Ins and formula used in calculation as per IS a type of failure used for bearing capacity an 1, Page No. 9, Table No. 3). te net bearing capacity in case of general sh $q_d = c N_c s_c d_c i_c + q (N_q-1) s_q d_q i_q + (1/2) B \gamma$ te net bearing capacity in case of local shea $q'_d = (2/3) c N'_c s_c d_c i_c + q (N'_q-1) s_q d_q i_q + (1/2) M_c$ $d_c = 1+ 0.2 (D_f/B)^*SQRT(N_{\phi})$	alysis depends upon the value of volue lear failure is given by (from IS 6403 $N_{\gamma}s_{\gamma}d_{\gamma}i_{\gamma}W'$ r failure is given by (from IS 6403 : - /2) B γ N' $_{\gamma}s_{\gamma}d_{\gamma}i_{\gamma}W'$	3 : 1981, page No 1981, page No. 8	
Assumption NOTE: The 5403 : 198 ³ The ultimat 3) The ultimat q Where, d	Ins and formula used in calculation as per IS a type of failure used for bearing capacity and 1, Page No. 9, Table No. 3). te net bearing capacity in case of general shad $q_d = c N_c s_c d_c i_c + q (N_q-1) s_q d_q i_q + (1/2) B \gamma$ te net bearing capacity in case of local shear $q'_d = (2/3) c N'_c s_c d_c i_c + q (N'_q-1) s_q d_q i_q + (1/2) d_c = 1 + 0.2 (D_f/B)*SQRT(N_\phi)$ $d_q = d_\gamma = 1$ for $\phi < 10^\circ$	alysis depends upon the value of volue lear failure is given by (from IS 6403 $N_{\gamma}s_{\gamma}d_{\gamma}i_{\gamma}W'$ r failure is given by (from IS 6403 : - /2) B γ N' $_{\gamma}s_{\gamma}d_{\gamma}i_{\gamma}W'$ (from IS 6403 : -	3 : 1981, page No	
Assumptior NOTE: The 5403 : 1987 The ultimat 3) The ultimat q Where, d d d	Ins and formula used in calculation as per IS a type of failure used for bearing capacity an 1, Page No. 9, Table No. 3). te net bearing capacity in case of general sh $q_d = c N_c s_c d_c i_c + q (N_q-1) s_q d_q i_q + (1/2) B \gamma$ te net bearing capacity in case of local shea $q'_d = (2/3) c N'_c s_c d_c i_c + q (N'_q-1) s_q d_q i_q + (1/2) M_q$ $d_c = 1 + 0.2 (D_f/B)^*SQRT(N_{\phi})$ $d_q = d_{\gamma} = 1$ for $\phi < 10^{\circ}$ $d_q = d_{\gamma} = 1 + 0.1 (D_f/B)^*SQRT(N_{\phi})$ for $\phi > 10^{\circ}$	alysis depends upon the value of volue lear failure is given by (from IS 6403 $N_{\gamma}s_{\gamma}d_{\gamma}i_{\gamma}W'$ r failure is given by (from IS 6403 : - /2) B γ N' $_{\gamma}s_{\gamma}d_{\gamma}i_{\gamma}W'$ (from IS 6403 : -	3 : 1981, page No 1981, page No. 8	
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Assumption NOTE: The 5403 : 198 ⁻⁷ The ultimat 3) The ultimat q Where, d d Mhere, d k here, d	Ins and formula used in calculation as per IS e type of failure used for bearing capacity and 1, Page No. 9, Table No. 3). te net bearing capacity in case of general sheat $d_d = c N_c s_c d_c i_c + q (N_q-1) s_q d_q i_q + (1/2) B \gamma$ te net bearing capacity in case of local sheat $d_d = (2/3) c N'_c s_c d_c i_c + q (N'_q-1) s_q d_q i_q + (1/2) d_c = 1 + 0.2 (D_f/B)*SQRT(N_{\phi})$ $d_q = d_{\gamma} = 1$ for $\phi < 10^{\circ}$ $d_q = d_{\gamma} = 1 + 0.1 (D_f/B)*SQRT(N_{\phi})$ for $\phi > 10^{\circ}$ $N_{\phi} = tan^2(\pi/4 + \phi/2)$	alysis depends upon the value of volue lear failure is given by (from IS 6403 $N_{\gamma} s_{\gamma} d_{\gamma} i_{\gamma} W'$ r failure is given by (from IS 6403 : - (2) B $\gamma N'_{\gamma} s_{\gamma} d_{\gamma} i_{\gamma} W'$ (from IS 6403 :	3 : 1981, page No 1981, page No. 8	
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Assumption NOTE: The 5403 : 198' The ultimat 3) The ultimat Where, d d Where, d d DUTPUT The compu	Ins and formula used in calculation as per IS a type of failure used for bearing capacity and 1, Page No. 9, Table No. 3). the net bearing capacity in case of general shaddle are N _c s _c d _c i _c + q (N _q -1) s _q d _q i _q + (1/2) B γ the net bearing capacity in case of local sheat $d_d = (2/3) c N'_c s_c d_c i_c + q (N'_q-1) s_q d_q i_q + (1/2)$ $d_d = (2/3) c N'_c s_c d_c i_c + q (N'_q-1) s_q d_q i_q + (1/2)$ $d_d = (2/3) c N'_c s_c d_c i_c + q (N'_q-1) s_q d_q i_q + (1/2)$ $d_d = d_{\gamma} = 1 + 0.2 (D_f/B)^*SQRT(N_{\phi})$ $d_q = d_{\gamma} = 1 + 0.1 (D_f/B)^*SQRT(N_{\phi})$ for $\phi > 10^{\circ}$ $N_{\phi} = tan^2(\pi/4 + \phi/2)$ h' is friction angle for local shear failure = tan	alysis depends upon the value of value ear failure is given by (from IS 6403 $N_{\gamma} s_{\gamma} d_{\gamma} i_{\gamma} W'$ r failure is given by (from IS 6403 : 12 (2) B $\gamma N'_{\gamma} s_{\gamma} d_{\gamma} i_{\gamma} W'$ (from IS 6403 : 12 (from IS 6403 : 12) (from IS 6403 : 12)	3 : 1981, page No 1981, page No. 8	
Assumption NOTE: The 5403 : 198' The ultimat 3) The ultimat Where, d d Where, d d DUTPUT The compu	Ins and formula used in calculation as per IS a type of failure used for bearing capacity and 1, Page No. 9, Table No. 3). te net bearing capacity in case of general shad $q_d = c N_c s_c d_c i_c + q (N_q-1) s_q d_q i_q + (1/2) B \gamma$ te net bearing capacity in case of local shear $q'_d = (2/3) c N'_c s_c d_c i_c + q (N'_q-1) s_q d_q i_q + (1/2)$ $d_c = 1 + 0.2 (D_f/B)^*SQRT(N_\phi)$ $d_q = d_\gamma = 1$ for $\phi < 10^\circ$ $d_q = d_\gamma = 1 + 0.1 (D_f/B)^*SQRT(N_\phi)$ for $\phi > 10^\circ$ $N_\phi = tan^2(\pi/4 + \phi/2)$ ther aided results for shear failure criteria are	alysis depends upon the value of value ear failure is given by (from IS 6403 $N_{\gamma} s_{\gamma} d_{\gamma} i_{\gamma} W'$ r failure is given by (from IS 6403 : 12 (2) B $\gamma N'_{\gamma} s_{\gamma} d_{\gamma} i_{\gamma} W'$ (from IS 6403 : 12 (from IS 6403 : 12) (from IS 6403 : 12)	3 : 1981, page No 1981, page No. 8	
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Assumption NOTE: The 5403 : 198 ⁻⁷ The ultimat 3) The ultimat q Where, d d Mhere, d d Mhere, d d DUTPUT The compu nterpolated	Ins and formula used in calculation as per IS a type of failure used for bearing capacity and 1, Page No. 9, Table No. 3). te net bearing capacity in case of general shad $q_d = c N_c s_c d_c i_c + q (N_q-1) s_q d_q i_q + (1/2) B \gamma$ te net bearing capacity in case of local shear $q'_d = (2/3) c N'_c s_c d_c i_c + q (N'_q-1) s_q d_q i_q + (1/2)$ $d_c = 1 + 0.2 (D_f/B)^*SQRT(N_\phi)$ $d_q = d_\gamma = 1$ for $\phi < 10^\circ$ $d_q = d_\gamma = 1 + 0.1 (D_f/B)^*SQRT(N_\phi)$ for $\phi > 10^\circ$ $N_\phi = tan^2(\pi/4 + \phi/2)$ ther aided results for shear failure criteria are	alysis depends upon the value of volue ear failure is given by (from IS 6403 $N_{\gamma} s_{\gamma} d_{\gamma} i_{\gamma} W'$ r failure is given by (from IS 6403 : 12 (2) B γ N' $_{\gamma} s_{\gamma} d_{\gamma} i_{\gamma} W'$ (from IS 6403 : 13 (1 (0.67 tan ϕ)	3 : 1981, page No 1981, page No. 8	



Director

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		<u></u>				00 C /
φ N		31.14		φ'		22.04
N _c		33.04		N' _c		16.92
N _q		20.96		N' _q		7.85
Nγ		26.54		Ν'γ		7.17
hape fa	ctors : (from IS	<u> 6403 : 1981, j</u>	page No. 8, Tab	ole No. 2)		
S.no.	Width(m)	Length (m)		Sc	Sq	Sγ
1	4.00	5.00		1.16	1.16	0.68
	0.00	0.00				
	0.00	0.00				
	0.00	0.00				
	0.00	0.00				
epth fa	ctors : (from IS	6403 : 1981, p	oage No. 9)			
S.no.	Depth(m)	Width(m)		dc	d _q	d _y
3.no. 1	4.00	4.00		1.35	1.18	1.18
		0.00				
		0.00				
		0.00				
clinatio	$i_c = (1 - \alpha / 90)^2$		$\frac{1}{i_q} = (1 - \alpha / 90)^2$			$i_{\gamma} = (1 - \alpha / \phi)^2$
clinatio		om IS 6403 : 19	-			$i_{\gamma} = (1 - \alpha / \phi)^2$ 1.00
	$\frac{i_c = (1 - \alpha / 90)^2}{1.00}$	om IS 6403 : 19	$i_q = (1 - \alpha / 90)^2$			
ater ta	$\frac{i_c = (1 - \alpha / 90)^2}{1.00}$	om IS 6403 : 19	$i_q = (1 - \alpha / 90)^2$ 1.00			
ater ta	$i_c = (1 - \alpha / 90)^2$ 1.00 ble factor : (fro	m IS 6403 : 19	$i_q = (1 - \alpha / 90)^2$ 1.00			1.00
ater ta	i _c = (1-α / 90) ² 1.00 ble factor : (fro Depth(m)	m IS 6403 : 19 m IS 6403 : 19 Width(m)	$i_q = (1 - \alpha / 90)^2$ 1.00	Z _w /B		1.00 W'
ater ta	i _c = (1-α / 90) ² 1.00 ble factor : (fro Depth(m)	m IS 6403 : 19 m IS 6403 : 19 Width(m) 4.00	$i_q = (1 - \alpha / 90)^2$ 1.00	Z _w /B		1.00 W'
ater ta	i _c = (1-α / 90) ² 1.00 ble factor : (fro Depth(m)	m IS 6403 : 19 m IS 6403 : 19 Width(m) 4.00 0.00 0.00 0.00 0.00	$i_q = (1 - \alpha / 90)^2$ 1.00	Z _w /B		1.00 W'
ater ta	i _c = (1-α / 90) ² 1.00 ble factor : (fro Depth(m)	m IS 6403 : 19 m IS 6403 : 19 Width(m) 4.00 0.00 0.00	$i_q = (1 - \alpha / 90)^2$ 1.00	Z _w /B		1.00 W'
<mark>/ater ta</mark> S.no. 1	i _c = (1-α / 90) ² 1.00 ble factor : (fro Depth(m)	m IS 6403 : 19 m IS 6403 : 19 Width(m) 4.00 0.00 0.00 0.00 0.00	$i_q = (1 - \alpha / 90)^2$ 1.00	Z _w /B		1.00 W'
<mark>/ater ta</mark> S.no. 1	i _c = (1-α / 90) ² 1.00 ble factor : (fro Depth(m) 4.00	m IS 6403 : 19 m IS 6403 : 19 Width(m) 4.00 0.00 0.00 0.00 0.00	$i_q = (1 - \alpha / 90)^2$ 1.00	Z _w /B	SBC in (t/m²)	1.00 <u>W</u> * 0.50
[/] ater ta S.no. 1 afe Bea	<u>i_c = (1-α / 90)²</u> 1.00 ble factor : (fro Depth(m) 4.00 rring Capacity Depth(m)	m IS 6403 : 19 m IS 6403 : 19 Width(m) 4.00 0.00 0.00 0.00 0.00	i _q = (1-α / 90) ² 1.00 81, page No. 9)	Z _w /B	SBC in (t/m ²) Local shear	1.00 <u>W</u> * 0.50
[/] ater ta S.no. 1 afe Bea	<u>i_c = (1-α / 90)²</u> 1.00 ble factor : (fro Depth(m) 4.00 ring Capacity	m IS 6403 : 19 m IS 6403 : 19 Width(m) 4.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	<u>i_q = (1-α / 90) ²</u> 1.00 81, page No. 9) Length (m) 5.00	Z _w /B -1.00	, ,	1.00 W' 0.50
<u>ater ta</u> S.no. 1 afe Bea S.no.	<u>i_c = (1-α / 90)²</u> 1.00 ble factor : (fro Depth(m) 4.00 rring Capacity Depth(m)	m IS 6403 : 19 m IS 6403 : 19 Width(m) 4.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	i _q = (1-α / 90) ² 1.00 81, page No. 9) 81, page No. 9 81, contemporal 81, page No. 9 81, contemporal 81, 	Z _w /B -1.00 General shear	Local shear	1.00 W' 0.50 Recommended
<u>ater ta</u> S.no. 1 afe Bea S.no.	<u>i_c = (1-α / 90)²</u> 1.00 ble factor : (fro Depth(m) 4.00 rring Capacity Depth(m)	m IS 6403 : 19 m IS 6403 : 19 Width(m) 4.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	<u>i_q = (1-α / 90) ²</u> 1.00 81, page No. 9) 81, page No. 9) 81, page No. 9 81, page No. 	Z _w /B -1.00 General shear	Local shear	1.00 W' 0.50 Recommended
<u>ater ta</u> S.no. 1 afe Bea S.no.	<u>i_c = (1-α / 90)²</u> 1.00 ble factor : (fro Depth(m) 4.00 rring Capacity Depth(m)	m IS 6403 : 19 m IS 6403 : 19 Width(m) 4.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	i _q = (1-α / 90) ² 1.00 81, page No. 9) 81, page No. 9 81, contemporal 81, page No. 9 81, contemporal 81, 	Z _w /B -1.00 General shear	Local shear	1.00 W' 0.50 Recommended
<u>ater ta</u> S.no. 1 afe Bea S.no.	<u>i_c = (1-α / 90)²</u> 1.00 ble factor : (fro Depth(m) 4.00 rring Capacity Depth(m)	m IS 6403 : 19 m IS 6403 : 19 Width(m) 4.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	<u>i_q = (1-α / 90) ²</u> 1.00 81, page No. 9) 81, page No. 9) 81, page No. 9 81, page No. 10 81, page No. 10 10, page No. 10, page 	Z _w /B -1.00 General shear	Local shear	1.00 W' 0.50 Recommended
Arriant S.no. 1 afe Bea S.no. 1 0TE: 7	<u>i_c = (1-α / 90)²</u> 1.00 ble factor : (fro Depth(m) 4.00 rring Capacity Depth(m) 4.00	m IS 6403 : 19 m IS 6403 : 19 Width(m) 4.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	<u>i_q = (1-α / 90) ²</u> 1.00 81, page No. 9) 81, page No. 9) 81, page No. 9) 81, page No. 9 81, page No.	Z _w /B -1.00 General shear	Local shear 15.65	1.00 W' 0.50 Recommended 35.11





NPUT DA	<u>TA</u>		Elevated
			BH-TNAL-02
Type of foo	oting		
1 C	Continuous Strip		
2 F	Rectangular	Rectangular	2
3 5	Square		
4 C	Circular		
Angle of int	ternal friction (ϕ°)		31.0
Cohesion (0.0
/oid ratio ($(e), e = (G.\gamma_w/\gamma_d) - 1$		0.6
Direction of	f load with vertical (°)		0.0
Density of f	foundation soil (t/m³) γ _{bulk}		1.7
-	ater table(m)		0.0
Factor of sa	afety		2.5
S.no.	Depth (m) of footing (D_f) below EGL	Width (m)	Length (m)
1	5.00	4.00	5.00
		0.00	0.00
		0.00	0.00
		0.00	0.00
		0.00	0.00
Assumptior	AILURE CRITERIA ns and formula used in calculation as per IS	-	nid ratio (see IS
Assumptior NOTE: The 5403 : 198 ⁻ The ultimat		alysis depends upon the value of vo	·
Assumptior NOTE: The 6403 : 198 ⁻ The ultimat 3)	ns and formula used in calculation as per IS e type of failure used for bearing capacity an 1, Page No. 9, Table No. 3).	alysis depends upon the value of vo ear failure is given by (from IS 6403	·
Assumptior NOTE: The 6403 : 198 ⁻ The ultimat 3) q	ns and formula used in calculation as per IS e type of failure used for bearing capacity an 1, Page No. 9, Table No. 3). te net bearing capacity in case of general sh	alysis depends upon the value of volume rear failure is given by (from IS 6403 $N_{\gamma}s_{\gamma}d_{\gamma}i_{\gamma}W'$	3 : 1981, page No
Assumptior NOTE: The 5403 : 198 ⁻⁷ The ultimat 3) The ultimat	ns and formula used in calculation as per IS e type of failure used for bearing capacity an 1, Page No. 9, Table No. 3). te net bearing capacity in case of general sh $q_d = c N_c s_c d_c i_c + q (N_q-1) s_q d_q i_q + (1/2) B \gamma$	alysis depends upon the value of vo ear failure is given by (from IS 6403 N _y s _y d _y i _y W' r failure is given by (from IS 6403 : ·	3 : 1981, page No
Assumptior NOTE: The 5403 : 198 The ultimat 3) The ultimat q Where,	Ins and formula used in calculation as per IS e type of failure used for bearing capacity an 1, Page No. 9, Table No. 3). te net bearing capacity in case of general sh $q_d = c N_c s_c d_c i_c + q (N_q-1) s_q d_q i_q + (1/2) B \gamma$ te net bearing capacity in case of local shea	alysis depends upon the value of vo ear failure is given by (from IS 6403 N _y s _y d _y i _y W' r failure is given by (from IS 6403 : ·	3 : 1981, page No
Assumptior NOTE: The 5403 : 198 The ultimat 3) The ultimat Q Where, d	Ins and formula used in calculation as per IS a type of failure used for bearing capacity an 1, Page No. 9, Table No. 3). te net bearing capacity in case of general sh $q_d = c N_c s_c d_c i_c + q (N_q-1) s_q d_q i_q + (1/2) B \gamma$ te net bearing capacity in case of local shea $q'_d = (2/3) c N'_c s_c d_c i_c + q (N'_q-1) s_q d_q i_q + (1/2) M_c$ $d_c = 1+ 0.2 (D_f/B)^*SQRT(N_{\phi})$	alysis depends upon the value of vo ear failure is given by (from IS 6403 $N_{\gamma}s_{\gamma}d_{\gamma}i_{\gamma}W'$ r failure is given by (from IS 6403 : - 2) B γ N' $_{\gamma}s_{\gamma}d_{\gamma}i_{\gamma}W'$	3 : 1981, page No 1981, page No. 8
Assumption NOTE: The 5403 : 198 The ultimat 3) The ultimat q Where, d	Ins and formula used in calculation as per IS a type of failure used for bearing capacity and 1, Page No. 9, Table No. 3). te net bearing capacity in case of general shad $q_d = c N_c s_c d_c i_c + q (N_q-1) s_q d_q i_q + (1/2) B \gamma$ te net bearing capacity in case of local shear $q'_d = (2/3) c N'_c s_c d_c i_c + q (N'_q-1) s_q d_q i_q + (1/2) d_c = 1 + 0.2 (D_f/B)*SQRT(N_\phi)$ $d_q = d_\gamma = 1$ for $\phi < 10^\circ$	alysis depends upon the value of vo ear failure is given by (from IS 6403 $N_{\gamma}s_{\gamma}d_{\gamma}i_{\gamma}W'$ r failure is given by (from IS 6403 : - '2) B γ N' $_{\gamma}s_{\gamma}d_{\gamma}i_{\gamma}W'$ (from IS 6403 : -	3 : 1981, page No
Assumption NOTE: The 5403 : 198 Fhe ultimat 3) Ghe ultimat Q Where, d d d	Ins and formula used in calculation as per IS a type of failure used for bearing capacity an 1, Page No. 9, Table No. 3). te net bearing capacity in case of general sh $q_d = c N_c s_c d_c i_c + q (N_q-1) s_q d_q i_q + (1/2) B \gamma$ te net bearing capacity in case of local shea $q'_d = (2/3) c N'_c s_c d_c i_c + q (N'_q-1) s_q d_q i_q + (1/2) M_c$ $d_c = 1+ 0.2 (D_f/B)^*SQRT(N_{\phi})$	alysis depends upon the value of vo ear failure is given by (from IS 6403 $N_{\gamma}s_{\gamma}d_{\gamma}i_{\gamma}W'$ r failure is given by (from IS 6403 : - '2) B γ N' $_{\gamma}s_{\gamma}d_{\gamma}i_{\gamma}W'$ (from IS 6403 : -	3 : 1981, page No 1981, page No. 8
Assumption NOTE: The 5403 : 198 The ultimat 3) The ultimat Where, d Where, d	Ins and formula used in calculation as per IS a type of failure used for bearing capacity an 1, Page No. 9, Table No. 3). te net bearing capacity in case of general sh $q_d = c N_c s_c d_c i_c + q (N_q-1) s_q d_q i_q + (1/2) B \gamma$ te net bearing capacity in case of local shea $q'_d = (2/3) c N'_c s_c d_c i_c + q (N'_q-1) s_q d_q i_q + (1/2) M_q$ $d_c = 1 + 0.2 (D_f/B)^*SQRT(N_{\phi})$ $d_q = d_{\gamma} = 1$ for $\phi < 10^{\circ}$ $d_q = d_{\gamma} = 1 + 0.1 (D_f/B)^*SQRT(N_{\phi})$ for $\phi > 10^{\circ}$	alysis depends upon the value of vo ear failure is given by (from IS 6403 N _γ s _γ d _γ i _γ W' r failure is given by (from IS 6403 : · 2) B γ N' _γ s _γ d _γ i _γ W' (from IS 6403 :	3 : 1981, page No 1981, page No. 8
Assumption NOTE: The 5403 : 198 The ultimat 3) The ultimat Where, d Where, d	Ins and formula used in calculation as per IS e type of failure used for bearing capacity and 1, Page No. 9, Table No. 3). te net bearing capacity in case of general sheat $d_d = c N_c s_c d_c i_c + q (N_q-1) s_q d_q i_q + (1/2) B \gamma$ te net bearing capacity in case of local sheat $d_d = (2/3) c N'_c s_c d_c i_c + q (N'_q-1) s_q d_q i_q + (1/2) d_c = 1 + 0.2 (D_f/B)*SQRT(N_{\phi})$ $d_q = d_{\gamma} = 1$ for $\phi < 10^{\circ}$ $d_q = d_{\gamma} = 1 + 0.1 (D_f/B)*SQRT(N_{\phi})$ for $\phi > 10^{\circ}$ $N_{\phi} = tan^2(\pi/4 + \phi/2)$	alysis depends upon the value of vo ear failure is given by (from IS 6403 N _γ s _γ d _γ i _γ W' r failure is given by (from IS 6403 : · 2) B γ N' _γ s _γ d _γ i _γ W' (from IS 6403 :	3 : 1981, page No 1981, page No. 8
Assumption NOTE: The 5403 : 198 The ultimat 3) The ultimat Where, d Where, d Mhere, d DUTPUT	Ins and formula used in calculation as per IS a type of failure used for bearing capacity and 1, Page No. 9, Table No. 3). the net bearing capacity in case of general shaddle are N _c s _c d _c i _c + q (N _q -1) s _q d _q i _q + (1/2) B γ the net bearing capacity in case of local sheat $d_d = (2/3) c N'_c s_c d_c i_c + q (N'_q-1) s_q d_q i_q + (1/2)$ $d_d = (2/3) c N'_c s_c d_c i_c + q (N'_q-1) s_q d_q i_q + (1/2)$ $d_d = (2/3) c N'_c s_c d_c i_c + q (N'_q-1) s_q d_q i_q + (1/2)$ $d_d = d_{\gamma} = 1 + 0.2 (D_f/B)^*SQRT(N_{\phi})$ $d_q = d_{\gamma} = 1 + 0.1 (D_f/B)^*SQRT(N_{\phi})$ for $\phi > 10^{\circ}$ $N_{\phi} = tan^2(\pi/4 + \phi/2)$ h' is friction angle for local shear failure = tan	alysis depends upon the value of vo ear failure is given by (from IS 6403 N _γ s _γ d _γ i _γ W' r failure is given by (from IS 6403 : · 2) B γ N' _γ s _γ d _γ i _γ W' (from IS 6403 : ·	3 : 1981, page No 1981, page No. 8
Assumption NOTE: The 5403 : 198 The ultimat 3) The ultimat Where, d d Mhere, d d DUTPUT The compu nterpolated	Ins and formula used in calculation as per IS e type of failure used for bearing capacity and 1, Page No. 9, Table No. 3). te net bearing capacity in case of general sheat $d_d = c N_c s_c d_c i_c + q (N_q-1) s_q d_q i_q + (1/2) B \gamma$ te net bearing capacity in case of local sheat $d_d = (2/3) c N'_c s_c d_c i_c + q (N'_q-1) s_q d_q i_q + (1/2) d_c = 1 + 0.2 (D_f/B)*SQRT(N_{\phi})$ $d_q = d_{\gamma} = 1$ for $\phi < 10^{\circ}$ $d_q = d_{\gamma} = 1 + 0.1 (D_f/B)*SQRT(N_{\phi})$ for $\phi > 10^{\circ}$ $N_{\phi} = tan^2(\pi/4 + \phi/2)$	alysis depends upon the value of vo ear failure is given by (from IS 6403 N ₇ s ₇ d ₇ i ₇ W' r failure is given by (from IS 6403 : : 2) B γ N' ₇ s ₇ d ₇ i ₇ W' (from IS 6403 : 1 (0.67 tan ϕ)	3 : 1981, page No 1981, page No. 8
Assumption NOTE: The 5403 : 198 The ultimat 3) The ultimat Where, d d Mhere, d d DUTPUT The compu nterpolated	Ins and formula used in calculation as per IS a type of failure used for bearing capacity and 1, Page No. 9, Table No. 3). te net bearing capacity in case of general shad $q_d = c N_c s_c d_c i_c + q (N_q-1) s_q d_q i_q + (1/2) B \gamma$ te net bearing capacity in case of local shear $q'_d = (2/3) c N'_c s_c d_c i_c + q (N'_q-1) s_q d_q i_q + (1/2)$ $d_c = 1 + 0.2 (D_f/B)^*SQRT(N_\phi)$ $d_q = d_\gamma = 1$ for $\phi < 10^\circ$ $d_q = d_\gamma = 1 + 0.1 (D_f/B)^*SQRT(N_\phi)$ for $\phi > 10^\circ$ $N_\phi = tan^2(\pi/4 + \phi/2)$ ther aided results for shear failure criteria are	alysis depends upon the value of vo ear failure is given by (from IS 6403 N ₇ s ₇ d ₇ i ₇ W' r failure is given by (from IS 6403 : : 2) B γ N' ₇ s ₇ d ₇ i ₇ W' (from IS 6403 : 1 (0.67 tan ϕ)	3 : 1981, page No 1981, page No. 8
Assumption NOTE: The 5403 : 198 ³ The ultimat 3) The ultimat Where, d d Where, d d DUTPUT The compu	Ins and formula used in calculation as per IS a type of failure used for bearing capacity and 1, Page No. 9, Table No. 3). te net bearing capacity in case of general shad $q_d = c N_c s_c d_c i_c + q (N_q-1) s_q d_q i_q + (1/2) B \gamma$ te net bearing capacity in case of local shear $q'_d = (2/3) c N'_c s_c d_c i_c + q (N'_q-1) s_q d_q i_q + (1/2)$ $d_c = 1 + 0.2 (D_f/B)^*SQRT(N_\phi)$ $d_q = d_\gamma = 1$ for $\phi < 10^\circ$ $d_q = d_\gamma = 1 + 0.1 (D_f/B)^*SQRT(N_\phi)$ for $\phi > 10^\circ$ $N_\phi = tan^2(\pi/4 + \phi/2)$ ther aided results for shear failure criteria are	alysis depends upon the value of vo ear failure is given by (from IS 6403 N ₇ s ₇ d ₇ i ₇ W' r failure is given by (from IS 6403 : : 2) B γ N' ₇ s ₇ d ₇ i ₇ W' (from IS 6403 : 1 (0.67 tan ϕ)	3 : 1981, page No 1981, page No. 8



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- 27	/ 11 nu	1-10				
see 🛿 😽	05 : 1981, Pag	e No S Table	NO. 3).			
OTE: T	Stype and Col	te used for be	aring capacity	analysis depend	s upon the valu	e of void ratio
		0.00	0.00			
		0.00	0.00			
		0.00	0.00			
		0.00	0.00			
1	5.00	4.00 0.00	5.00 0.00	57.69	18.77	41.44
4	E 00	4.00	5.00	General shear	Local shear	Recommended
S.no.	Depth(m)	Width(m)	Length (m)		SBC in (t/m ²)	
				1		
afe Beai	ing Capacity					
		0.00				
		0.00				
		0.00				
		0.00				
1	5.00	4.00		-1.25		0.50
S.no.	Depth(m)	Width(m)		Z _w /B		W'
			51, page 110. 3)			
lator tab	le factor : /fro	m IS 6403 · 40	81, page No. 9)			
	1.00		1.00			1.00
i	$_{\rm c} = (1 - \alpha / 90)^2$	2	$i_q = (1 - \alpha / 90)^2$			$i_{\gamma} = (1 - \alpha / \phi)^2$
clinatio	n factors : (fro	om IS 6403 : 19	81, page No. 9)		
		0.00				
		0.00				
		0.00				
		0.00				
1	5.00	4.00		1.44	1.22	1.22
S.no.	Depth(m)	Width(m)		dc	d_q	d_{γ}
						
epth fac	tors : (from IS	6403 : 1981, p	age No. 9)			
	0.00	0.00				
	0.00	0.00				
	0.00	0.00				
	0.00	0.00				
1	4.00	5.00		1.16	1.16	0.68
S.no.	Width(m)	Length (m)		Sc	Sq	Sγ
hape fac	tors : (from IS	<u> 6403 : 1981, p</u>	bage No. 8, Tab	<u>ele No. 2)</u>		
Νγ		25.99		Ν' _γ		7.06
N _q		20.63		N' _q		7.76
-		32.67		N'c		16.80
N _c						





	Corrected Total (mm) tnemetted			75.00				75.00						75.00		-1
	Rigidity Esctor			1.00				1.00						1.00]
	Depth Factor			0.799				0.747						0.683		
	Totsi Settlement (mm)	86.19	7.66			81.95	18,49				64.43	45.37	10			
	inemeitset sitsala iz (mm)	86.1896	7.6574			81.9488	18.4914				64.4251	45.3675				1
	ifo to suluboM (Kg/Cm ²)	356	260			356	260				356	260				
	Corrected Consolidation Settlement (mm)					2.1										
	tnemeltter Settlement (mm)															1
	(Balve (Cm ² /Kg)															1
	auleV-N sgersvA	50	34		k. ne	20	34				SO	34				1
-	themat at memory at wid Depth (ادھ/Cm2)	10.311	2.554			12.474	3.914				16.260	6.671]
0121 T-HPT 2000 VET SY NOTI PTO OTVA I VEWERT 150	Dispersed Breadth (m)	4.000	8.500			4.000	7,500				4.000	6.500				
	(m) Dispersed Length	5.00	9.500			5.00	8.500				5.00	7.500				
unu unu	Height of layer(m)	4.50	1.50			3.50	2.50				2.50	3.50				1
	(m) (m)			4,00				4.00						4,00		1
	(m) dtgnej			5.00		9. - 1		5.00						5.00		1
	Stress at Foundation level (Kg/Cm2)			10.31				12.47			61			16.26		ation .
-	Layer Thickness	4,50	1.50			3.50	2.50				2.50	3.50			6	131
	oT (m)	7.50	00.2			7.50	10.00				7.50	11.00			Corr	ic:or
	(m)	3.00	7.50			4.00	7,50				5.00	7.50			Bai	
	(m) Depth below FGL			00'E				4.00						2.00	0.	The Director
	rsyer	Layer 1	Layer 2		8	Layer 1	Layer 2				Layer 1	Layer 2			<u> </u>	

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SR-837_23-24

Mater Table depth considered for analysis = 0.00 m Solution So	Scour Depth = 0.00 m For End Bearing e.b) yeff c Ø Nc am ² gm/cc kg/cm ² deg					ŗ
Dia. of (m) Cut-off (m) Soli layers Properties of layers/for Skin Friction Plie Depth (m) from (m) to c gm/cc cm kg/cm^2 1.00 2.00 0.00 2.00 0.00 2.00 0.00 200 0.06 200 0.06 200 0.06 200 0.06 200 0.06 0.02 0.06 0.03 0.06 0.03 0.06 0.03 0.06 0.03 0.06 0.03 0.06 0.03 0.06 0.03 0.06 0.03 0.06 0.03 0.06 0.03 0.06 0.03 0.06 0.03 0.06 0.03 0.06 0.03 0.06 0.03 0.06 0.03 0.06 0.03 0.06 0.03 0.06 0.06 0.06 0.06 0.06 0.03 0.06 0.03 0.02 0.03 0.06 0.03 0.142 1.42 1.42 1.42 1.42 1.42 1.42 1.142 1.42 1.42 <th>ee Ø</th> <th></th> <th>Liquefactio</th> <th>Liquefaction Depth = 0.00 m</th> <th></th> <th></th>	ee Ø		Liquefactio	Liquefaction Depth = 0.00 m		
Plie Depth from to c Ø k α Veff Δ L pd(s.f) (m) (m) (m) (m) (m) (m) γ </th <th>kglom² c deg</th> <th></th> <th></th> <th></th> <th></th> <th></th>	kglom ² c deg					
(m) (m) (m) (m) (m) kg/cm^2 deg j gm/cc cm kg/cm^2 1.00 2.00 0.00 2.00 7.00 0.00 2.00 0.06 200 0.32 1.00 2.00 7.00 0.00 2.00 7.00 0.06 200 0.32 7.00 10.00 13.50 1.50 0.30 0.79 500 0.32 7.00 10.00 13.50 0.00 32 1.50 0.30 0.63 300 1.15 0.00 20.00 32 1.50 0.30 0.80 300 1.15 0.00 20.00 21.00 32 1.50 0.30 0.83 1.15 0.01 25.50 20.00 32 1.50 0.30 1.156 1.16 0.01 25.50 26.00 0.30 0.83 450 1.156 0.01 25.50 26.00 0.30 0.84 <t< th=""><th>kg/cm²</th><th>Nq</th><th>Ŋ</th><th>As/cm Ap</th><th>sb</th><th>g</th></t<>	kg/cm ²	Nq	Ŋ	As/cm Ap	sb	g
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				cm ² cm ²		t
	0.00	29.50	30.21	314.29 314.29 314.29 314.29 314.29 314.29 314.29 7857.14	44.85 55.99 92.22 102.12 46.04 46.04 207.16 23.02	371.87
					717.74	371.87
Qu,comp.= qs + Qp	Qu,uplift =	0.7 x Safe	Frictional Re	0.7 x Safe Frictional Resistance + Weight of Pile	t of Pile	
Qa,comp.= (717.74 + 371.87) / 2.5 Qa,comp.= 435.84 T	Qa,uplift = Qa,uplift =	0.7 × 717. 214.60	0.7 × 717.74/3 + 47.12 214.60 T	2		
Say Qa,comp.= 435.00 T	Qa,uplift =	214.00	F			



Answersten Constrained for anyors Constraine for anyors Constraine for anyors <	Reference POI 0.00 Turnet from the contractional of the contractinal of the contractional of the contractional of th	Length of Pile below cut of level =	t of level =		26.00 m			Bore	Bore Hole No =	BH-TN-0	No = BH-TN-01 Ch. (KM) Elevated	Elevated			Di	Dia of pile = 1.00 m	1.00 m	Cut	Cut-off Level = 2.00 m	: 2.00 m	below EGL	Ъ
Dual Cadim Second Properties of lynering	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	Restricting PD to 20D	a S	/ater Tabl 1alysis =	e depth c	onsidere	d for	0.00 m				Sco	ur Depth :	= 0.00 m				Liquefact	tion Depth	= 0.00 m		
In In<	Print Print <th< th=""><th></th><th>Soil lay</th><th>ers</th><th></th><th>Ā</th><th>operties of</th><th>f layers/for</th><th>Skin Frict</th><th>ion</th><th></th><th></th><th>For En</th><th>d Bearing</th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th></th<>		Soil lay	ers		Ā	operties of	f layers/for	Skin Frict	ion			For En	d Bearing								
Im Im<	10 100		from	to	υ	Ø	×	α	γeff	ΔL	pd (s.f)			о	Ø	Nc	Nq	Ny	As/cm	Ap	sb	g
100 200 <td>100 200 200 200 200 000 201 150 200 000 201 1420 214.20</td> <td></td> <td>(m)</td> <td>(m)</td> <td>kg/cm²</td> <td>deg</td> <td></td> <td></td> <td>gm/cc</td> <td>cm</td> <td>kg/cm²</td> <td>kg/cm²</td> <td>gm/cc</td> <td>kg/cm²</td> <td>deg</td> <td></td> <td></td> <td></td> <td>cm²</td> <td>cm²</td> <td>t</td> <td>t</td>	100 200 200 200 200 000 201 150 200 000 201 1420 214.20		(m)	(m)	kg/cm ²	deg			gm/cc	cm	kg/cm ²	kg/cm ²	gm/cc	kg/cm ²	deg				cm ²	cm ²	t	t
Qu,comp.= qs + Qp Qu,uplift = 0.7 x Safe Frictional Resistance + Weight of Pile Qa,comp.= (809.81 + 371.94) / 2.5 Qa,uplift = 0.7 x 809.81 / 3 + 51.05 Qa,comp.= 472.70 T Qa,uplift = 0.7 x 809.81 / 3 + 51.05 Qa,comp.= 472.00 T Qa,uplift = 240.01 T	Qu,comp.= qs + Qp Qu,uplift = 0.7 x Safe Frictional Resistance + Weight of F Qa,comp.= (809.81 + 371.94) / 2.5 Qa,uplift = 0.7 x 809.81 / 3 + 51.05 Qa,comp.= 472.70 T Qa,uplift = 240.01 T Say Qa,comp.= 472.00 T Qa,uplift = 240.00 T		0.00 2.00 110.00 21.00 21.00 25.50 25.50	2.00 7.00 10.00 22.00 22.00 28.00 28.00	0.0 0.0 0.0 0.0 0.0 0.0 0.0	3 3 3 3 3 3 3 3 3 3	1.50 1.50 1.50 1.50 1.50 1.50	0.30 0.30 0.30 0.30 0.30 0.30	0.60 0.79 0.80 0.82 0.82 0.83 0.83	200 500 350 350 450 250	0.06 0.32 0.63 1.15 1.56 1.56 1.56	5. 5.	0.84	00.0	32	თ	29.50	30.21	314.29 314.29 314.29 314.29 314.29 314.29 314.29	7857.14		
Qu,comp.= qs + Qp Qu,uplift = Qa,comp.= (809.81 + 371.94) / 2.5 Qa,uplift = Qa,comp.= 472.70 T Qa,uplift = Qa,comp.= 472.00 T Qa,uplift =	Qu,comp.= qs + Qp Qu,uplift = Qa,comp.= (809.81 + 371.94) / 2.5 Qa,uplift = Qa,comp.= 472.70 T Qa,uplift = Say Qa,comp.= 472.00 T Qa,uplift =																				809.81	371.94
Qa,comp.= (809.81 + 371.94) / 2.5 Qa,uplift = Qa,comp.= 472.70 T Qa,uplift = Qa,comp.= 472.00 T Qa,uplift =	Qa,comp.= (809.81 + 371.94) / 2.5 Qa,uplift = Qa,comp.= 472.70 T Qa,uplift = Say Qa,comp.= 472.00 T Qa,uplift =						Qu,com	=.d	qs + Qp						Qu,uplift =		0.7 x Safé	e Frictional	Resistance	+ Weight o	f Pile	
Qa,comp.= 472.00 T Qa,uplift = 240.00	Say Qa,comp.= 472.00 T Qa,uplift.= 240.00						Qa,com Qa,com	п. п. п.	(809.81 + 472.70	· 371.94) / T	2.5				Qa,uplift = Qa,uplift =		0.7 x 809 240.01	.81 / 3 + 51 T	.05			
	#EOC for Vratical Connectivity of allo in commensation = 0.5					Say	Qa,com	=.q	472.00						Qa,uplift :		240.00					



Mater Table depth considered for analysis Mater Table depth considered for manysis Dia. of (m) Cut-off (m) Soli layers Properties of layers/for Kin Friction A 100 2.00 0.00 2.00 0.00 2.00 0.00	Scour Depth = 0.00 m			Cut-off Level = 2.00 m	helow EGL	٦Ľ
Dia. of Pile Cut-off Depth Soli layers Properties of layers/for Skin Friction Pile Depth from to c g wff ΔL pd(s/f) (m) (m) (m) (m) (m) gamo c g wff ΔL pd(s/f) 1.00 2.00 0.00 2.00 7.00 0.00 31 1.50 0.30 0.80 320 0.03 0.20 0.066 200 0.066 200 0.066 200 0.066 200 0.066 200 0.022 0.02 0.030 0.32 1.50 0.330 0.80 330 0.83 300 0.1142 10.00 11.000 13.50 0.000 32 1.50 0.330 0.80 330 0.1142 11.00 21.00 21.00 32 1.50 0.330 0.82 1.42 1.42 11.01 25.50 30.00 0.00 32 1.50 0.330 0.83<			Liquef	Liquefaction Depth = 0.00 m		
Plie Depth from to c γ κ α \sqrt{eff} ΔL $pd(s_f)$ (m) (m) (m) (m) (m) (m) m γ	For End Bearing					
(m) (m) (m) (m) (m) kgum ² deg m kgum ² 1.00 2.00 0.00 2.00 0.00 2.00 0.06 200 0.06 1.00 2.00 7.00 0.00 31 1.50 0.30 0.79 500 0.03 7.00 10.00 13.50 0.00 32 1.50 0.30 0.80 300 0.63 7.00 13.50 0.00 32 1.50 0.30 0.80 300 1.15 0.00 21.00 0.00 32 1.50 0.30 0.83 450 1.14 0.00 21.00 0.00 32 1.50 0.30 0.83 1.14 0.00 20.00 0.00 32 1.50 0.30 0.15 1.14 0.00 20.00 0.00 32 1.50 0.30 0.14 1.14 0.00 20.00 0.00 32 1.50 <t< th=""><th>.f) Pd (e.b) yeff c</th><th>Ø Nc</th><th>Ng Ny</th><th>As/cm Ap</th><th>sb</th><th>g</th></t<>	.f) Pd (e.b) yeff c	Ø Nc	Ng Ny	As/cm Ap	sb	g
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	n ² kg/cm ² gm/cc kg/cm ²	deg		cm ² cm ²	t t	t
	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	32	29.50 30.21	314.29 314.29 314.29 314.29 314.29 314.29 7857.14	44.85 55.99 92.22 102.12 146.35 46.04 207.16 207.16	371.94
					901.88	371.94
Qu,comp.= qs + Qp		Qu,uplift = 0.	7 x Safe Frictior	0.7 x Safe Frictional Resistance + Weight of Pile	it of Pile	
Qa,comp.= (901.88 + 371.94) / 2.5 Qa,comp.= 509.53 T		Qa,uplift = 0. Qa,uplift = 2	0.7 x 901.88 / 3 + 54.98 265.42 T	54.98		
Say Qa,comp.= 509.00 T		Qa,uplift =	265.00 T			
*FOS for Vertical Capacity of pile in compression = 2.5 **FOS for Uplift Capacity of pile = 3.0						



Restricting PD to 20D Dia. of Cut-off Soil I Pile Depth from	Length of Pile below cut of level =	30.00 m			Bore I	Hole No =	Bore Hole No = BH-TN-01 Ch. (KM) Elevated	Ch. (KM)	Elevated			Dia	Dia of pile = 1.00 m	1.00 m	Cut-	Cut-off Level = 2.00 m	2.00 m	below EGL	ЗĽ
Cut-off Depth fro	Water Tabl analysis =	Water Table depth considered for analysis =	onsidere		0.00 m				Scou	Scour Depth = 0.00 m	0.00 m				Liquefacti	Liquefaction Depth = 0.00 m	0.00 m		
Depth	Soil layers		P	Properties of layers/for Skin	layers/for	Skin Friction	Ľ			For End	For End Bearing								
	to	c	Ø	×	α	γeff	ΔL	pd (s.f)	Pd (e.b)	γeff	с	Ø	Nc	Nq	Ny	As/cm	Ap	sb	Q
(m)	(m)	kg/cm ²	deg			gm/cc	сm	kg/cm ²	kg/cm ²	gm/cc	kg/cm ²	deg				cm ²	cm ²	t	t
1.00 2.00 2.00 2.00 2.00 2.00 1.00 2.00 2	2.00 7.00 13.50 16.50 21.00 21.00 25.50 30.00 32.00	0.0 00.0 00.0 00.0 00.0 00.0 00.0	3 3 3 3 3 3 3 3 3 3 3	1.50 1.50 1.50 1.50 1.50 1.50	0.30 0.30 0.30 0.30 0.30 0.30	0.60 0.79 0.80 0.82 0.82 0.83 0.83 0.84	200 500 350 350 200 200 200	0.06 0.32 0.63 1.15 1.56 1.56 1.56	. 56	0.84	0.00	3	ത	29.50	30.21	314.29 314.29 314.29 314.29 314.29 314.29 314.29 314.29	7857.14	44.85 55.99 92.22 46.04 46.04 207.16 92.07 16 92.07	372.00
-								1										993.95	372.00
				Qu,comp.=	=.	qs + Qp						Qu,uplift =		0.7 x Safe	Frictional F	0.7 x Safe Frictional Resistance + Weight of Pile	- Weight of	Pile	
				Qa,comp.= Qa,comp.=		(993.95 + 372) / 2.5 546.38 T	372) / 2.5 T					Qa,uplift = Qa,uplift =		0.7 × 993.9 290.83	0.7 × 993.95 / 3 + 58.9 290.83 T	o			
			Say	Qa,comp.=	. .	546.00	⊢					Qa,uplift =		290.00	F				



	Length of Pile below cut of level =	of level =	.,	32.00 m			Bore	Hole No =	BH-TN-01	Bore Hole No = BH-TN-01 Ch. (KM) Elevated	Elevated			Diŝ	Dia of pile =	1.00 m	Cut-	Cut-off Level = 2.00 m	2.00 m	below EGL	ы
Restricting PD to 20D	20D	Wa ana	Water Table analysis =	Water Table depth considered for analysis =	onsidere		0.00 m				Scou	Scour Depth = 0.00 m	: 0.00 m				Liquefacti	Liquefaction Depth = 0.00 m	: 0.00 m		
Dia. of Cut-off	off	Soil layers	s.		Pr	operties of	ayers/for	Properties of layers/for Skin Friction	uc			For End	For End Bearing								
		from	to	υ	Ø	×	α	γeff	ΔL	pd (s.f)	Pd (e.b)	γeff	υ	Ø	Nc	Νq	Ny	As/cm	Ap	sb	Q
				kg/cm ²	deg			gm/cc	cm	kg/cm ²	kg/cm ²	gm/cc	kg/cm ²	deg				cm ²	cm ²	t	t
Director Director (Project) + 116 of 125		2 2 0 0 1 1 2 2 2 0 0 1 1 2 2 0 0 1 1 2 2 0 0 1 1 2 2 0 0 1 1 2 2 2 2	2.00 7.00 13.50 20.00 22.00 33.00 34.00	0.0 00.0 00.0 00.0 00.0 00.0 00.0	32 33 33 33 33 33 33 33 33 33 33 33 33 3	1.50 1.50 1.50 1.50 1.50 1.50 1.50	0.30 0.30 0.30 0.30 0.30 0.30 0.30	0.79 0.79 0.80 0.82 0.82 0.84 0.84 0.84	200 500 350 350 450 450 400	0.00 0.32 0.63 1.15 1.56 1.56 1.56 1.56	5 8	0.8	0000	ğ	თ	29.50	30.21	314.29 314.29 314.29 314.29 314.29 314.29 314.29	7857.14	44.85 55.99 92.22 102.12 46.04 207.16 184.14 184.14	372.00
																				1086.02	2 372.00
						Qu,comp.=	=.0	qs + Qp						Qu,uplift =		0.7 x Safe	Frictional F	0.7 x Safe Frictional Resistance + Weight of Pile	+ Weight oʻ	f Pile	
						Qa,comp.= Qa,comp.=	н. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	(1086.02 + 583.21	(1086.02 + 372) / 2.5 583.21 T					Qa,uplift = Qa,uplift =		0.7 × 1086 316.24	0.7 × 1086.02 / 3 + 62.83 316.24 T	2.83			
				S	Say	Qa,comp.=	= d	583.00	 					Qa,uplift =		316.00	F				



Length of Pile below cut of level =	e below cu	it of level		34.00 m			Bore I	tole No =	Bore Hole No = BH-TN-01 Ch. (KM) Elevated	ch. (KM)	Elevated			Dia	Dia of pile =	1.00 m	Cut-	Cut-off Level = 2.00 m	2.00 m	below EGL	ਰ
Restricting PD to 20D) to 20D	- 10	Water Tab analysis =	Water Table depth considered for analysis =	considere		0.00 m				Scou	Scour Depth = 0.00 m	0.00 m				Liquefacti	Liquefaction Depth = 0.00 m	0.00 m		
Dia. of O	Cut-off	Soil layers	yers		۹.	roperties of	Properties of layers/for Skin Friction	Skin Frictic	u			For End	For End Bearing								
	Depth	from	to	С	Ø	k	α	γeff	۸L	pd (s.f)	Pd (e.b)	γeff	с	Ø	Nc	Nq	Ny	As/cm	Ap	sb	Q
(m)	(m)	(m)	(m)	kg/cm ²	deg			gm/cc	cm	kg/cm ²	kg/cm ²	gm/cc	kg/cm ²	deg				cm²	cm ²	t	t
8 8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	00 N	0.00 2.00 10.00 15.50 22.00 34.50 34.50	2.00 7.00 13.50 16.50 21.00 25.50 36.00 36.00	0.0 0.0 00.0 00.0 00.0 00.0 00.0	3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	1.50 1.50 1.50 1.50 1.50 1.50 1.50	0.30 0.30 0.30 0.30 0.30 0.30 0.30 0.30	0.60 0.79 0.80 0.82 0.82 0.83 0.83 0.83 0.84	200 500 350 350 450 150 150	0.06 0.32 0.63 1.15 1.56 1.56 1.56 1.56	1.56	0.84	0.00	g	თ	29.50	30.21	314.29 314.29 314.29 314.29 314.29 314.29 314.29 314.29	7857.14	44.85 55.99 92.22 102.12 46.04 207.16 207.16 71.77	372.00
																				1180.80	372.00
						Qu, comp.=	=.q	qs + Qp						Qu,uplift =		0.7 x Safe	Frictional F	0.7 x Safe Frictional Resistance + Weight of Pile	- Weight of	Pile	
						Qa, comp.= Qa, comp.=		(1180.8 + 372) / 2.5 621.12 T	372) / 2.5 Т					Qa,uplift = Qa,uplift =		0.7 × 1180.8 / 3 + 66.76 342.28 T).8 / 3 + 66. Т	76			
					Say	Qa,comp.=	р.=	621.00	F					Qa,uplift =		342.00	⊢				



Water Table depth consider analysis = Soli layers Soli layers from to c Ø (m) (m) kg/cm² deg 0.00 2.00 7.00 0.00 31 7.00 10.00 0.00 32 10.00 13.50 0.00 32 113.50 16.50 0.00 32 21.00 25.50 0.00 32 25.50 0.000 32 32	ed for 0.00 m Properties of layers/for Skin Friction	ore Hole No	Bore Hole No = BH-TN-01 Ch. (KM) Elevated	1 Ch. (KM)	Elevated			Dia	Dia of pile = 1.20 m	1.20 m	Cut	Cut-off Level = 2.00 m	2.00 m	below EGL	Ľ
Cut-off Soil layers c Ø Depth from to c Ø (m) (m) (m) kg/cm ² deg (m) (m) (m) kg/cm ² deg 2.00 0.00 2.00 7.00 0.00 31 7.00 10.00 13.50 0.00 32 10.00 32 10.00 13.50 16.50 0.00 32 24.00 32 24.00 32 25.50 0.00 32 25.50 0.00 32 </th <th>roperties of layers</th> <th>-</th> <th></th> <th></th> <th>Scol</th> <th>Scour Depth = 0.00 m</th> <th>= 0.00 m</th> <th></th> <th></th> <th></th> <th>Liquefact.</th> <th>Liquefaction Depth = 0.00 m</th> <th>0.00 m</th> <th></th> <th></th>	roperties of layers	-			Scol	Scour Depth = 0.00 m	= 0.00 m				Liquefact.	Liquefaction Depth = 0.00 m	0.00 m		
Depth from to c (m) (m) (m) kg/cm² (m) (m) (m) kg/cm² 2.000 0.000 2.000 0.000 7.000 10.000 0.000 113.50 16.50 0.000 113.50 16.50 21.00 0.000 24.000 24.000 0.000 25.50 0.000 25.500 26.000 0.000 0.000 0.000		/for Skin Friv	ction			For End	For End Bearing								
(m) (m) (m) kg/cm² 2.00 0.00 2.00 0.00 2.00 10.00 10.00 0.00 7.00 10.00 13.50 0.00 10.00 13.50 16.50 0.00 21.00 24.00 25.50 0.00 25.50 26.00 0.00 0.00		γeff	ΔL	pd (s.f)	Pd (e.b)	γeff	с	Ø	Nc	Nq	Ny	As/cm	Ap	sb	Q
2.00 2.00 2.00 2.00 2.00 7.00 0.00 2.00 7.00 10.00 0.00 10.00 13.50 16.50 0.00 21.00 24.00 24.00 0.00 25.50 25.50 0.00 25.50 26.00 0.00		gm/cc		kg/cm ²	kg/cm ²	gm/cc	kg/cm ²	deg				cm ²	cm ²	t	t
ndi	1.50 0.30 1.50 0.30 1.50 0.30 1.50 0.30 1.50 0.30 1.50 0.30 1.50 0.30 1.50 0.30 1.50 0.30 1.50 0.30 1.50 0.30	0.60 0.79 0.80 0.80 0.80 0.82 0.83 0.83 0.83 0.83 0.84 0.84	200 500 350 350 300 150 50	0.06 0.32 0.63 1.15 1.46 1.77 1.89		0.83	00.0	33	σ	29.50	30.21	377.14 377.14 377.14 377.14 377.14 377.14 377.14 377.14	11314.29	53.82 67.19 110.66 122.54 232.31 187.60 100.39 33.46 33.46	648.59
														907.97	648.59
	Qu,comp.=	qs + Qp	đ					Qu,uplift =		0.7 x Safe	Frictional	0.7 x Safe Frictional Resistance + Weight of Pile	Weight of	Pile	
	Qa,comp.= Qa,comp.=	(907.97 + 622.63	(907.97 + 648.59) / 2.5 622.63 T	2.5				Qa,uplift = Qa,uplift =		0.7 × 907.9 279.72	0.7 × 907.97 / 3 + 67.86 279.72 T	86			
Say	Qa,comp.=	622.00	Γ					Qa,uplift =		279.00	F				



Restricting PD to 20D	Length of Pile below cut of level =	26.00 m	_		Bore F	Bore Hole No = BH-TN-01 Ch. (KM) Elevated	BH-TN-01	Ch. (KM)	Elevated			Ď	Dia of pile = 1.20 m	1.20 m	Cut	Cut-off Level = 2.00 m	2.00 m	below EGL	ЗL
	Water Tabl analysis =	Water Table depth considered for analysis =	considere		0.00 m				Scou	Scour Depth = 0.00 m	: 0.00 m				Liquefact	Liquefaction Depth = 0.00 m	= 0.00 m		
	Soil layers		đ.	Properties of layers/for Skin Friction	f layers/for	Skin Frictic	Ļ			For End	For End Bearing								
Depth	from to	c	Ø	k	α	γeff	ΔL	pd (s.f)	Pd (e.b)	γeff	С	Ø	Nc	Nq	Ny	As/cm	Ap	sb	Q
(m) (m)	(m) (m)	kg/cm ²	deg			gm/cc	cm	kg/cm ²	kg/cm ²	gm/cc	kg/cm ²	deg				cm ²	cm ²	t	t
	2:00 7.00 10:00 10:00 13:50 16:50 21:00 24:00 25:50 25:50 25:50 28:00	0.00 00.00 00.00 00.00 00.00 00.00	3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	1.50 1.50 1.50 1.50 1.50 1.50	0.30 0.30 0.30 0.30 0.30 0.30	0.79 0.80 0.80 0.82 0.83 0.83 0.83	500 300 450 250 250	0.32 0.63 0.89 1.15 1.77 1.89 1.89	1.89	0.84	0.00	33	Ø	29.50	30.21	377.14 377.14 377.14 377.14 377.14 377.14 377.14 377.14	11314.29	53.82 67.19 110.66 122.54 187.60 160.39 167.32	648.73
	_																	1041.83	648.73
				Qu,comp.=	=.c	qs + Qp						Qu,uplift =		0.7 x Safe	Frictional	0.7 x Safe Frictional Resistance + Weight of Pile	+ Weight of	Pile	_
				Qa,comp.= Qa,comp.=		(1041.83 + 648.73) / 2.5 676.22 T	+ 648.73) / 2 T	2.5				Qa,uplift = Qa,uplift =		0.7 x 104 ⁻ 316.61	0.7 x 1041.83 / 3 + 73.51 316.61 T	3.51			
			Say	Qa,comp.=	=.d	. 00.979	F					Qa,uplift =		316.00	F				



	Length of Pile below cut of level =	2	28.00 m			Bore F	Bore Hole No = BH-TN-01 Ch. (KM) Elevated	BH-TN-01	Ch. (KM)	Elevated			Ō	Dia of pile = 1.20 m	1.20 m	Cu	Cut-off Level = 2.00 m	= 2.00 m	below EGL	ЭГ
Restricting PD to 20D	Wat anal	Water Table analysis =	Water Table depth considered for analysis =	nsiderec		0.00 m				Scol	Scour Depth = 0.00 m	= 0.00 m				Liquefac	Liquefaction Depth = 0.00 m	= 0.00 m		
Dia. of Cut-off	Soil layers	s		Prc	Properties of layers/for Skin Friction	layers/for	Skin Frictio	uc			For En	For End Bearing								
Depth	from t	to	c	Ø	k	α	γeff	۸L	pd (s.f)	Pd (e.b)	γeff	c	Ø	Nc	Nq	Ny	As/cm	Ap	sb	Qp
(m)			kg/cm ²	deg			gm/cc	cm	kg/cm ²	kg/cm ²	gm/cc	kg/cm ²	deg				cm ²	cm ²	t	t
	0.00 2. 2.00 7. 7.00 10 13.50 10 13.50 20 24.00 25 25.50 30 25.50 30 25.50 30 26.50 30 27.00 25 25.50 30 26.50 25 27.00 25	2.00 7.00 13.50 21.00 22.00 30.00 30.00	0.0000000000000000000000000000000000000	3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	1.50 1.50 1.50 1.50 1.50 1.50	0.30 0.30 0.30 0.30 0.30 0.30	0.60 0.79 0.80 0.83 0.83 0.83 0.84	200 500 350 350 300 450 450 450	0.06 0.32 0.89 1.15 1.77 1.89 1.89	2 8 8	0. 84	0 0 0	ğ	თ	29.50	30.21	377.14 377.14 377.14 377.14 377.14 377.14 377.14 377.14	1314.29	53.82 67.19 110.66 122.54 232.31 187.60 100.39 301.18	648.73
-		-											-				-	_	1175.68	648.73
					Qu,comp.=	ų,	qs + Qp						Qu,uplift =	IJ	0.7 x Safi	e Frictional	0.7 x Safe Frictional Resistance + Weight of Pile	+ Weight o	f Pile	
					Qa,comp.= Qa,comp.=		(1175.68 + 729.77	(1175.68 + 648.73) / 2.5 729.77 T	2.5				Qa,uplift = Qa,uplift =		0.7 x 117 353.49	0.7 × 1175.68 / 3 + 79.17 353.49 T	79.17			
			š	Say	Qa,comp.=		729.00	F					Qa,uplift =		353.00	F				
				-1													7			



Restricting PD to 20D Wate analy analy Dia. of Cut-off Soil layers Pile Depth from tr (m) (m) (m) (m)	Length of Pile below cut of level =	30.00 m			Bore	Hole No =	Bore Hole No = BH-TN-01 Ch. (KM) Elevated	Ch. (KM)	Elevated			Diê	Dia of pile = 1.20 m	1.20 m	Cut	Cut-off Level = 2.00 m	2.00 m	below EGL	ЭĽ
Cut-off Depth fro	Water Tabl analysis =	Water Table depth considered for analysis =	onsidere		0.00 m				Scou	Scour Depth = 0.00 m	: 0.00 m				Liquefact.	Liquefaction Depth = 0.00 m	: 0.00 m		
Depth	yers		Ā	Properties of layers/for Skin	'layers/for	Skin Friction	nc			For Enc	For End Bearing								
(m)	to	c	Ø	k	α	γeff	۸L	(J.s) bd	Pd (e.b)	γeff	С	Ø	Nc	Nq	Ny	As/cm	Ap	sb	Q
()	(m)	kg/cm ²	deg			gm/cc	cm	kg/cm ²	kg/cm ²	gm/cc	kg/cm ²	deg				cm^{2}	cm ²	t	t
1.20 2.00 2.00 2.00 2.00 2.00 2.00 2.00 1.20 10 21.00 2.00 21.00 2.00 224.00 2.00 20 2.00 20 2	2.00 7.00 13.50 21.00 22.00 32.00 32.00	0.00 00.00 00.00 00.00 00.00 00.00	3 3 3 3 3 3 3 3 3 3 3 3	1 :50 1 :50 1 :50 1 :50 1 :50 1 :50 1 :50	0.30 0.30 0.30 0.30 0.30 0.30	0.60 0.79 0.80 0.83 0.83 0.83 0.84 0.84	200 500 350 350 350 450 200 200	0.06 0.32 0.89 1.15 1.77 1.89 1.89 1.89	. 89	.0 8.	0 0 0	33	Ø	79 70	30.21	377.14 377.14 377.14 377.14 377.14 377.14 377.14 377.14	11314.29	53.82 67.19 110.66 122.54 187.60 100.39 301.18 133.86 133.86	648. 73
																		1309.54	648.73
				Qu,comp.=	=.0	qs + Qp						Qu,uplift =		0.7 x Safe	Frictional	0.7 x Safe Frictional Resistance + Weight of Pile	+ Weight of	Pile	
				Qa,comp.= Qa,comp.=	o.= 	(1309.54 + 783.31	(1309.54 + 648.73) / 2.5 783.31 T	2.5				Qa,uplift = Qa,uplift =		0.7 × 1309 390.38	0.7 x 1309.54 / 3 + 84.82 390.38 T	4.82			
		07	Say	Qa,comp.=	=.q	783.00	F					Qa,uplift =		390.00	г				



Length of	Length of Pile below cut of level =	ut of level	п	32.00 m			Bore Hole	Hole No =	BH-TN-01	No = BH-TN-01 Ch. (KM) Elevated	Elevated			Dia	Dia of pile =	1.20 m	Cut-	Cut-off Level = 2.00 m	2.00 m	below EGL	ы
Restricting PD to 20D	PD to 20D		Water Table depth considered for analysis =	ole depth .	considere		0.00 m				Scou	Scour Depth = 0.00 m	0.00 m				Liquefacti	Liquefaction Depth = 0.00 m	0.00 m		
Dia. of	Cut-off	Soil layers	iyers		Ē	Properties of layers/for Skin Friction	^F layers/for	Skin Frictic	ň			For End	For End Bearing								
Pile	Depth	from	to	υ	Ø	×	α	γeff	ΔL	pd (s.f)	Pd (e.b)	γeff	c	Ø	Nc	Nq	Ny	As/cm	Ap	sb	g
(m)	(m)	(m)	(m)	kg/cm ²	deg			gm/cc	cm	kg/cm²	kg/cm ²	gm/cc	kg/cm ²	deg				cm ²	cm²	t	t
87	0002 OF COLUMN DE COLUMN D	0.00 2.00 7.00 10.00 13.50 24.00 25.50 30.00	2.00 7.00 13.50 16.50 24.00 24.00 34.00 34.00	0.00 0.00 0.00 0.00 0.00 0.00 0.00	33 33 33 33 33 33 33 33 33 33 33 33 33	1.50 1.50 1.50 1.50 1.50 1.50	0.30 0.30 0.30 0.30 0.30 0.30	0.60 0.79 0.80 0.82 0.83 0.83 0.84 0.84	200 500 350 350 350 450 450 400	0.06 0.32 0.89 1.15 1.77 1.89 1.89 1.89	1.89	0.84	0.00	ğ	თ	29.50	30.21	377.14 377.14 377.14 377.14 377.14 377.14 377.14 377.14 377.14	11314.29	53.82 67.19 110.66 187.60 100.39 301.18 267.71 267.71	648. 83
																				1443.40	648.83
						Qu, comp.=	=. Ф	qs + Qp						Qu,uplift =		0.7 x Safe	Frictional F	0.7 x Safe Frictional Resistance + Weight of Pile	+ Weight of	Pile	
						Qa,comp.= Qa,comp.=	". ".	(1443.4 + 648.83) / 2.5 836.89 T	648.83) / 2 T	5				Qa,uplift = Qa,uplift =		0.7 × 1443. 427.27	0.7 × 1443.4 / 3 + 90.48 427.27 T	48			
					Say	Qa,comp.=	р.=	836.00	F					Qa,uplift =		427.00	Т				



Length of	Length of Pile below cut of level =	ut of level	п	34.00 m			Bore Hole		BH-TN-01	No = BH-TN-01 Ch. (KM) Elevated	Elevated			Dia	Dia of pile = 1.20 m	1.20 m	Cut	Cut-off Level = 2.00 m	2.00 m	below EGL	Ч
Restricting PD to 20D	PD to 20D	-	Water Table depth considered for analysis =	ole depth (:	considere	d for	0.00 m				Scoul	Scour Depth = 0.00 m	0.00 m				Liquefacti	Liquefaction Depth = 0.00 m	0.00 m		
Dia. of	Cut-off	Soil layers	ayers		Ā	roperties of	f layers/for	Properties of layers/for Skin Friction	uc			For End	For End Bearing								
Pile	Depth	from	to	υ	Ø	×	α	γeff	ΔL	pd (s.f)	Pd (e.b)	γeff	υ	Ø	Nc	Nq	Ny	As/cm	Ap	sb	g
(m)	(m)	(m)	(m)	kg/cm ²	deg			gm/cc	cm	kg/cm ²	kg/cm ²	gm/cc	kg/cm ²	deg				cm²	cm ²	t	÷
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	80 COLLOR RAIL COLLOR DI	0.00 2.00 7.00 13.50 24.00 25.50 30.00 34.50	2.00 7.00 10.00 16.50 24.00 24.00 34.50 36.00 36.00	0.0 0.0 00.0 00.0 00.0 00.0 00.0	3 2 2 2 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	1.50 1.50 1.50 1.50 1.50 1.50 1.50	0.30 0.30 0.30 0.30 0.30 0.30 0.30	0.60 0.79 0.80 0.83 0.83 0.84 0.84 0.88 0.88	200 500 350 350 300 450 450 150 150	0.06 0.32 0.89 1.15 1.89 1.89 1.89 1.89	68. 0	0.84	0. 0	3	Ø	58 29	30.21	377.14 377.14 377.14 377.14 377.14 377.14 377.14 377.14 377.14	11314.29	53.82 67.19 110.66 187.60 100.39 301.18 301.18 104.33	
																				1581.19	648.83
						Qu, comp.=	=.d	qs + Qp						Qu,uplift =		0.7 x Safe	Frictional F	0.7 x Safe Frictional Resistance + Weight of Pile	- Weight of	Pile	
						Qa,comp.= Qa,comp.=	п. п. п. d.	(1581.19 + 648.83) / 2.5 892.01 T	+ 648.83) / Т	2.5				Qa,uplift = Qa,uplift =		0.7 × 1581. 465.08	0.7 x 1581.19 / 3 + 96.13 465.08 T	5.13			
					Say	Qa,comp.=	=.q	892.00	F					Qa,uplift =		465.00	F				



	Late		d capacity of	Pile	1		
			I-BH-TN-01		-		
		Ch. (l	KM): Elevated				
Type of Strata = Sandy							
Le = Embedded Length of Pile in Met	er =	32.000	m Fck	c = 35.0	N/mm ² D	= 1	00 cm
Bed level	0.0 m						
Pile cap bottom level	-2.0 m						
Scour Depth	0.0 m						
E = Young's Modulus of Pile (Kg/cm ²)		=	5000 🔨	F _{ck}	N/mm ² =	295803.	99 Kg/cm ²
I = Moment of Inertia (cm ²)		=	πxD ⁴ /64		=	4908738	8.5 cm ⁴
K ₁ = Constant for Sandy / Normally Cor	solidated Clay		(Kg/cm ³)		=	0.705	
T, Relative stiffness factor in Sand	ſ	ī =	El 5 K ₁	_	=	290.3	cm
For Long Pile If L _e > 4T							
L1 =					=	0.000	cm
L ₁ T					=	0.00	
For Fixed Head Pile							
L _f T					=	2.20	From Fig. 4
Lf					=	639.03	cm
Equivalent length of cantilever L=	L1+L _F : 0.0	0 +	639.03265		=	639.03	cm
Y = Pile Head Deflection (Cm)		=	Q(L ₁ + L _F) ³ 12 El	(for fixed Hea	d pile)		
			Q =	Lateral Loa	d in Kg		
Lateral Load For Pile Head Deflect	tion .5 cm		Q		=	33385.36	Kg
					=	33.39	т
Safe Lateral resistance of Pile = Late	ral resistance co	orrespond	ing to deflection 1	.0% of Pile Dia	ameter at scour		1.0
					=	66.77	т
					Say	66	т

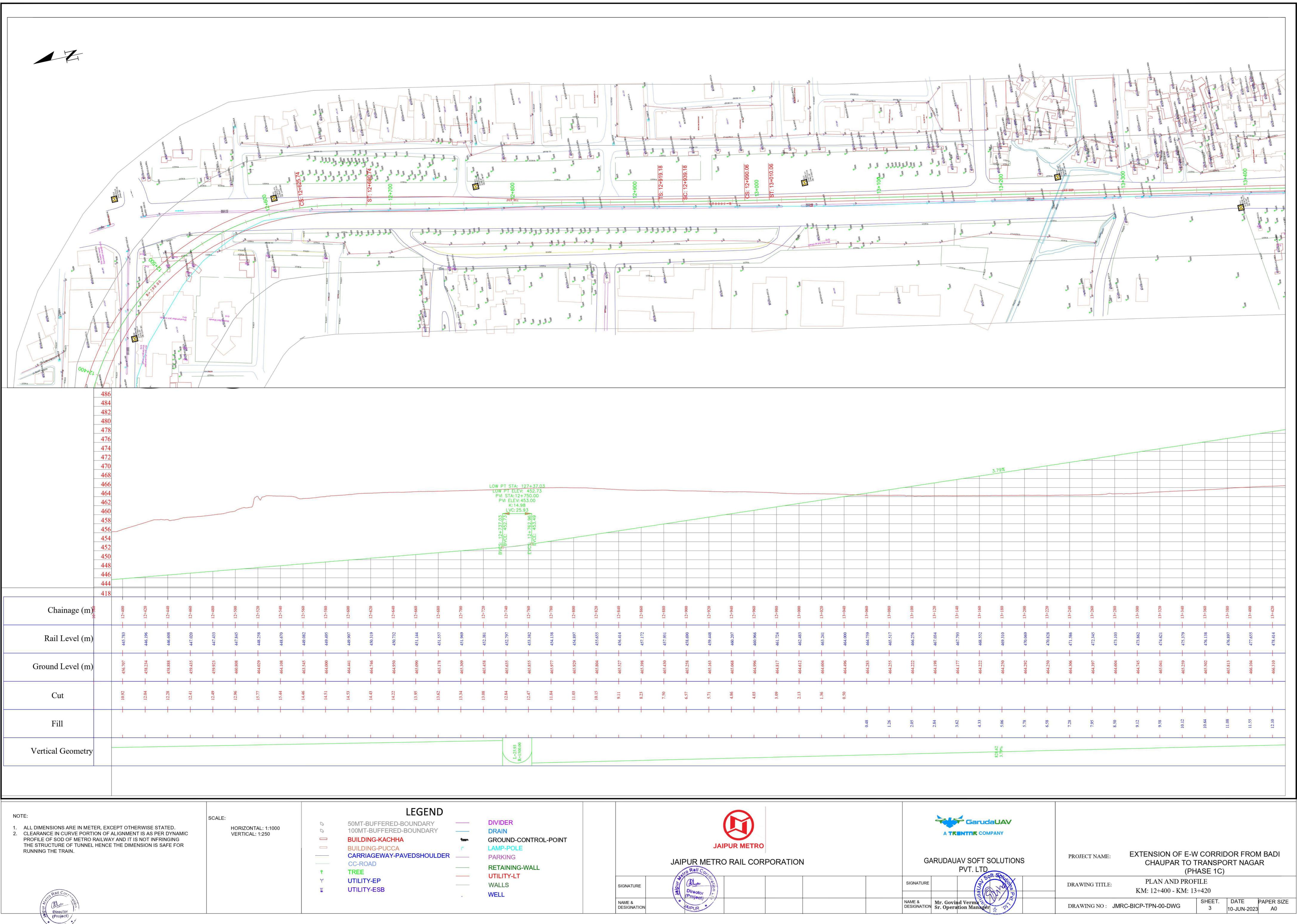




Le = Embedded Length of Pile in Meter = 32.000 m Fck = 35.0 N/mm ² D = 120 cm Bed level 0.0 m Pile cap bottom level -2.0 m Scour Depth 0.0 m E = Young's Modulus of Pile (Kg/cm ²) = $5000\sqrt{F_{ck}}$ N/mm ² = 295803.99 Kg/cm ² I = Moment of Inertia (cm ²) = $xxD^{1}/64$ = 10178760.2 cm ⁴ K ₁ = Constant for Sandy / Normally Consolidated Clay (Kg/cm ³) = 0.705 T, Relative stiffness factor in Sand T = $\sqrt{\frac{EI}{K_1}}$ = $\frac{10000}{K_1}$ cm For Long Pile If L ₆ > 4T L1 = $\frac{1}{K_1}$ = $\frac{10000}{K_1}$ cm For Fixed Head Pile L ₁ = $\frac{1}{K_1}$ = $\frac{10000}{K_1}$ cm For Fixed Head Pile L ₁ = $\frac{1}{K_1}$ = $\frac{10000}{K_1}$ cm Y = Pile Head Deflection (Cm) = $\frac{Q(L_1 + L_F)^3}{12 EI}$ (for fixed Head pile) Lateral Load For Pile Head Deflection 5 cm Q = Lateral Load in Kg Lateral Load For Pile Head Deflection 5 cm Safe Lateral resistance of Pile = Lateral resistance corresponding to deflection 1.0% of Pile Diameter at scour level 1.2 E 107.26 T		Later	al Loa	d capacity of F	Pile	-		
Type of Strata = Sandy Late = Embedded Length of Pile in Meter = 32.000 m Fck = 35.0 N/mm ² D = 120 cm Bed level 0.0 m Pile cap bottom level 2.0 m Scour Depth 0.0 m E = Young's Modulus of Pile (Kg/cm ²) = 5000 F _a . N/mm ² = 295803.99 Kg/cm ² 1 = Moment of Inertia (cm ²) = $\pi D^4/64$ = 10178760.2 cm ⁴ K ₁ = Constant for Sandy / Normally Consolidated Clay (Kg/cm ³) = 0.705 T. Relative stiffness factor in Sand T = $\sqrt{\frac{EI}{K_1}}$ = 335.9 cm For Long Pile If L _a > 4T T = $\sqrt{\frac{EI}{K_1}}$ = 0.000 cm E = 0.000 cm Control Fried Head Pile Lateral Lead For Pile Head Deflection (Cm) = $\frac{Q(L_1 + L_F)^3}{12 EI}$ (for fixed Head Pile) T = $\frac{Q(L_1 + L_F)^3}{12 EI}$ (for fixed Head Pile) Carter at Load For Pile Head Deflection .5 cm C = $\frac{Q(L_1 + L_F)^3}{2}$ (for fixed Head Pile) C = $\frac{44.693}{12}$ T Safe Lateral resistance of Pile = Lateral resistance corresponding to deflection 1.0% of Pile Diameter at scour level T = 107.26 T								
Le = Embedded Length of Pile in Meter = 32.000 m Fck = 35.0 N/mm ² D = 120 cm Bed level 0.0 m Pile cap bottom level -2.0 m Scour Depth 0.0 m E = Young's Modulus of Pile (Kg/cm ²) = $5000\sqrt{F_{ck}}$ N/mm ² = 295803.99 Kg/cm ² I = Moment of Inertia (cm ²) = $xxD^{1}/64$ = 10178760.2 cm ⁴ K ₁ = Constant for Sandy / Normally Consolidated Clay (Kg/cm ³) = 0.705 T, Relative stiffness factor in Sand T = $\sqrt{\frac{EI}{K_1}}$ = $\frac{10000}{K_1}$ cm For Long Pile If L ₆ > 4T L1 = $\frac{1}{K_1}$ = $\frac{10000}{K_1}$ cm For Fixed Head Pile L ₁ = $\frac{1}{K_1}$ = $\frac{10000}{K_1}$ cm For Fixed Head Pile L ₁ = $\frac{1}{K_1}$ = $\frac{10000}{K_1}$ cm Y = Pile Head Deflection (Cm) = $\frac{Q(L_1 + L_F)^3}{12 EI}$ (for fixed Head pile) Lateral Load For Pile Head Deflection 5 cm Q = Lateral Load in Kg Lateral Load For Pile Head Deflection 5 cm Safe Lateral resistance of Pile = Lateral resistance corresponding to deflection 1.0% of Pile Diameter at scour level 1.2 E 107.26 T			Ch. (I	KM): Elevated				
Pile cap bottom level 2.0 m Scour Depth 0.0 m E = Young's Modulus of Pile (Kg/cm ²) = $5000 \sqrt{F_{ex}}$ N/mm ² = 295803.99 Kg/cm ² I = Moment of Inertia (cm ²) = $xxD^4/64$ = 10178760.2 cm ⁴ K ₁ = Constant for Sandy / Normally Consolidated Clay (Kg/cm ³) = 0.705 T, Relative stiffness factor in Sand T = $\sqrt{\frac{EI}{K_1}}$ = 335.9 cm For Long Pile If L ₂ > 4T L1 = $\frac{1}{T}$ = $\frac{1}{\sqrt{T}}$ = 0.000 cm L1 = 0.000 cm Equivalent length of cantilever L = L1+L _F : 0.00 + 739.38059 = 739.38 cm Y = Pile Head Deflection (Cm) = $\frac{Q(L_1 + L_F)^3}{12 EI}$ (for fixed Head pile) Lateral Load For Pile Head Deflection 5 cm Q = Lateral Load in Kg Lateral Load For Pile Head Deflection 5 cm Safe Lateral resistance of Pile = Lateral resistance corresponding to deflection 1.0% of Pile Dameter at scour level 1.2 = 107.26 T		=	32.000	m Fck	= 35.0	N/mm ² D	= 1	20 cm
$I = Moment of Inertia (cm2) = mxD4/64 = 10178760.2 cm4$ $K_{1} = Constant for Sandy / Normally Consolidated Clay (Kg/cm3) = 0.705$ $T, Relative stiffness factor in Sand T = s = 335.9 cm$ $T = s = \frac{EI}{K_{1}} = 335.9 cm$ For Long Pile if L _e > 4T $I = I = I = 0.000 cm$ $I = 0.000$	Pile cap bottom level	-2.0 m						
$K_{1} = Constant for Sandy / Normally Consolidated Clay (Kg/cm3) = 0.705$ T, Relative stiffness factor in Sand $T = \sqrt{3} \frac{EI}{K_{1}} = 335.9 \text{ cm}$ For Long Pile If L _a > 4T $I = \frac{1}{K_{1}} = 0.000 \text{ cm}$ $I = 0.00 \text{ cm}$ $I = 0.00$ For Fixed Head Pile $L_{1} = 2.20 \text{ From Fig. 4}$ $I = 739.38 \text{ cm}$ Equivalent length of cantilever $L = L1+L_{F}: 0.00 + 739.38059 = 739.38 \text{ cm}$ $Y = Pile \text{ Head Deflection (Cm)} = \frac{Q(L_{1} + L_{F})^{3}}{12 \text{ EI}} (\text{for fixed Head pile})$ $I = I$ $Q = Lateral Load in Kg$ $Q = 44693.67 \text{ Kg}$ $I = 44.69 \text{ T}$ Safe Lateral resistance of Pile = Lateral resistance corresponding to deflection 1.0% of Pile Diameter at scour level $I = 107.26 \text{ T}$	E = Young's Modulus of Pile (Kg/cm ²)		=	5000 🖯	F _{ck}	N/mm ² =	295803.	99 Kg/cm ²
T, Relative stiffness factor in Sand $T = \sqrt{3} \frac{EI}{K_1} = 335.9 \text{ cm}$ For Long Pile If L ₀ > 4T L1 = $\frac{1}{K_1} = 0.000 \text{ cm}$ $\frac{1}{T} = 0.000 \text{ cm}$ $\frac{1}{T} = 0.000 \text{ cm}$ For Fixed Head Pile L ₁ = 2.20 From Fig. 4 T Lf = 739.38 cm Equivalent length of cantilever L = L1+L _F : 0.00 + 739.38059 = 739.38 cm Y = Pile Head Deflection (Cm) = $\frac{Q(L_1 + L_F)^3}{12 EI} (\text{for fixed Head pile})$ Lateral Load For Pile Head Deflection .5 cm Q = Lateral Load in Kg Lateral Load For Pile Head Deflection .5 cm Q = 44693.67 Kg = 44693 T Safe Lateral resistance of Pile = Lateral resistance corresponding to deflection 1.0% of Pile Diameter at scour level = 107.26 T	I = Moment of Inertia (cm^2)		=	πxD ⁴ /64		=	1017876	0.2 cm ⁴
$T = \sqrt{5} K_{1}$ For Long Pile If L _o > 4T L1 =	K ₁ = Constant for Sandy / Normally Conse	olidated Clay		(Kg/cm ³)		=	0.705	
L1 = $= 0.000$ cm = 0.00 For Fixed Head Pile L ₁ T For Fixed Head Pile L ₁ T Lf = 739.38 cm Equivalent length of cantilever L= L1+L _F : 0.00 + 739.38059 = 739.38 cm Y = Pile Head Deflection (Cm) = $\frac{Q(L_1 + L_F)^3}{12 El}$ (for fixed Head pile) Lateral Load For Pile Head Deflection .5 cm Q = Lateral Load in Kg Lateral Load For Pile Head Deflection .5 cm Q = 44.69 T Safe Lateral resistance of Pile = Lateral resistance corresponding to deflection 1.0% of Pile Diameter at scour level 1.2 = 107.26 T	T, Relative stiffness factor in Sand	т	=	、	_ -	=	335.9	cm
$\frac{L_{f}}{T} = \frac{2.20}{From Fig. 4}$ $= \frac{2.20}{739.38} From Fig. 4$ $= 739.38 cm$ $= 739.38 cm$ $= 739.38 cm$ $Y = Pile Head Deflection (Cm) = \frac{Q(L_{1} + L_{F})^{3}}{12 El} (for fixed Head pile)$ $= \frac{Q(L_{1} + L_{F})^{3}}{12 El} (for fixed In Kg)$ $= 44.693.67 Kg$ $= 44.69 T$ Safe Lateral resistance of Pile = Lateral resistance corresponding to deflection 1.0% of Pile Diameter at scour level 1.2 = 107.26 T	For Long Pile If L _e > 4T L1 = L <u>1</u> T							cm
Equivalent length of cantilever L= L1+L _F : 0.00 + 739.38059 = 739.38 cm $Y = Pile \text{ Head Deflection (Cm)} = \frac{Q(L_1 + L_F)^3}{12 \text{ El}} (\text{ for fixed Head pile}) \\ 12 \text{ El} \\ Q = Lateral Load in Kg \\ Lateral Load For Pile Head Deflection .5 cm} Q = 44693.67 \text{ Kg} \\ = 44.69 \text{ T} \\ Safe Lateral resistance of Pile = Lateral resistance corresponding to deflection 1.0% of Pile Diameter at scour level 1.2 \\ = 107.26 \text{ T} \\ \end{bmatrix}$	L _f					=	2.20	From Fig. 4
12 El Q = Lateral Load in Kg Lateral Load For Pile Head Deflection .5 cm Q = 44693.67 Kg = 44.69 T T T Safe Lateral resistance of Pile = Lateral resistance corresponding to deflection 1.0% of Pile Diameter at scour level 1.2 = 107.26 T	Lf Equivalent length of cantilever L=	L1+L _F : 0.00	+	739.38059				
Lateral Load For Pile Head Deflection .5 cm Q = 44693.67 Kg = 44.69 T Safe Lateral resistance of Pile = Lateral resistance corresponding to deflection 1.0% of Pile Diameter at scour level = 107.26 T	Y = Pile Head Deflection (Cm)		=	12 EI				
= 107.26 T	Lateral Load For Pile Head Deflection	n .5 cm				=		-
	Safe Lateral resistance of Pile = Latera	I resistance cor	respond	ing to deflection 1.	0% of Pile Dia			1.2
Say 107 T							107.26 107	т т







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							L=25.93 R=1500.00																						3.79%		

LEGEND				
50MT-BUFFERED-BOUNDARY 100MT-BUFFERED-BOUNDARY BUILDING-KACHHA BUILDING-PUCCA CARRIAGEWAY-PAVEDSHOULDER CC-ROAD TREE UTILITY-EP UTILITY-ESB	*	DIVIDER DRAIN GROUND-CONTROL-POINT LAMP-POLE PARKING RETAINING-WALL UTILITY-LT WALLS WELL	SIGNATURE NAME & DESIGNATION	JAIPUF

JAIPUR METRO	A TRENTIR COMPANY
JR METRO RAIL CORPORATION	GARUDAUAV SOFT SOLUTIONS PVT. LTD
liteotor roject)	SIGNATURE
PUR	NAME & Mr. Govind Verma & P DESIGNATION Sr. Operation Manager

Name of Work: Contract ICB No.JP/EW/1C (Underground) /03: "Design and Construction of Twin Tunnel by Shield TBM, Underground Station (Ramg	janj (
Underground Ramp from Badi Chaupar dead end Ch:10387.860 to Underground ramp end Ch:13040 of Jaipur Metro Phase-1C including Entry Exit Str	ructı
Sanitary Installations and Drainage Works at Jaipur, Rajasthan, India."	

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S.No	Reference Volume/ Clause/ Page no of tender documents	Reference to tender document clause	Queries	Engineer's Reply
1	Vol 2, GCC, Clause 1.8, Employer's use of Contractor's Document, Pg 11	The Contractor shall be deemed (by signing the Contract) to give to the Employer a non-terminable, transferable, non- exclusive royalty-free licence to copy, use and communicate the Contractor's Documents, including making and using modifications of them.	Bidder seeks deletion of non-terminable, transferable, non-exclusive royalty-free licence to copy, use and communicate the Contractor's Documents, including making and using modifications of them"	Not agreed
2	Vol 2, GCC, Clause 2.2, Access to and Possession of the Site, Pg 12	If the Contractor suffers delay from failure on the part of the Employer to grant right of access to, or possession of the Site, the Contractor shall give notice to the Engineer in a period of 28 days of such occurrence. After receipt of such notice, the Engineer shall proceed to determine any extension of time to which the Contractor is entitled and shall notify the Contractor accordingly. For any such delay in handing over of site, Contractors will be entitled to only reasonable extension of time and no monetary claims, whatsoever shall be paid or entertained on this account	Bidder seeks that if the contractor's performance of the work is delayed due to non-availability of access to site, then the contractor shall not only be entitled to Extension of time but also cost.	Not agreed
3	Vol 2, GCC, Clause 2.4, Assignment by the Employer, Pg, 12	The Employer shall be fully entitled without the consent of the Contractor, to assign the benefit of the part thereof and any interest therein or thereunder to any third Party.	Bidder seeks deletion of the following "without the consent of the contractor"	Not agreed



nj Chaupar), Cut and Cover Tunnel Box and ctures, Architectural finishing, water supply,

S.No	Reference Volume/ Clause/ Page no of tender documents	Reference to tender document clause	Queries
4	Vol 2, GCC, Clause 4.23, Unforeseeable Physical Conditions,	 If, during the execution of the Works, the Contractor shall encounter physical conditions, which, in his opinion, could not have been reasonably foreseen by an experienced Contractor, the Contractor shall forthwith give written notice thereof to the Engineer and if, in the opinion of the Engineer, such conditions could not have been reasonably foreseen by an experienced Contractor, then the Engineer may certify and the Employer may pay reasonable additional cost to which the Contractor shall have been put by reason of such conditions in the following cases: a) for complying with any instruction which the Engineer may issue to the Contractor in connection therewith, and b) for any proper and reasonable measures approved by the Engineer which the Contractor may take in the absence of specific instructions from the Engineer, as a result of such conditions or obstructions being encountered. The decision of the Engineer as to the additional cost shall be final and binding 	Bidder seeks that "Compensation Amount has to be mutually agreed upon". The decision of the Engineer as to the additional cost shall not be final and binding
5	Vol 2, GCC, Clause 5.8 Intellectual Property Rights and Royalties, Pg 31	Insofar as the patent, copyright or other intellectual property rights in any Plant, Design Data, plans, calculations, drawings, documents, Materials, know- how and information relating to the Works shall be vested in the Contractor, the Contractor shall grant to the Employer, his successors and assignees a royalty - free, non- exclusive and irrevocable licence (carrying the right to grant sub-licences) to use and reproduce any of the works, designs or inventions incorporated and referred to in such Plant, documents or Materials and any such know-how and information for all purposes relating to the Works (including without limitation the design, manufacture, installation, reconstruction, Testing, commissioning, completion, reinstatement, extension, repair and operation of the Works.	Bidder seeks that Contractor shall not grant to the Employer a non-exclusive irrevocable and royalty- free licence (carrying the right to grant sub-license) to use, repair, copy, modify, enhance, adapt and translate in any form such Software for his own use.
6	Vol 2, GCC, Clause 7.5 Testing, Pg 36	The Engineer shall give the Contractor not less than 24 hours' notice of his intention to attend the tests.	The bidder seeks that instead of 24hrs, reasonable time should be allowed



	Engineer's Reply
be to	Not agreed
ver ,	Not agreed
9	Not agreed

S.No	Reference Volume/ Clause/ Page no of tender documents	Reference to tender document clause	Queries
7	Vol 2, GCC, Clause 7.10.2, Cost of uncovering the work already covered up, Pg 37	The Contractor shall uncover any part or parts of the Works, or make openings in or through the same, as the Engineer may from time to time direct, and shall reinstate and make good such part or parts, to the satisfaction of the Engineer. If any such part or parts have been covered up, or put out of view after compliance with the requirement of Sub-clause 7.11.4 and the Works are found to be executed in accordance with the Contract, the expenses of uncovering, making openings in or through, reinstating and making good the same, shall be borne by the Employer, but if the Works are found to be defective, costs shall be borne by the Contractor. In case after completion of a part of the Work, the part of Work is not fully consistent with the Employer's Requirements and there is no way to change the same, in that case, the same (provided it has no implication on safety and operation) shall be accepted only at a Contractor's deemed variation at lower negotiated price. The decision of the Engineer in this regard shall be final and binding on the Contractor.	Bidder seeks deletion of the following "The decision of the Engineer in this regard shall be final and binding on the Contractor"
8	Vol 2, GCC, Clause 8.3, Delay, Pg 39	Failure or delay by the Employer or the Engineer, to hand over to the Contractor the Site necessary for execution of Works, or any part of the Works, or to give necessary notice to commence the Works, or to provide necessary Drawings or instructions or clarifications or to supply any material, Plant or Machinery, which under the Contract, is the responsibility of the Employer, shall in no way affect or vitiate the Contract or alter the character thereof; or entitle the Contractor to damages or compensation thereof but in any such case, the Engineer shall extend the time period for the completion of the Contract, as in his opinion is/are reasonable.	Bidder seeks that in case of delay by the Employer or the Engineer to hand over the site necessary for execution of works, the contractor shall be entitled to extension of time and Cost.
9	Vol 2, GCC, Clause 8.4.1, Extension of time for completion, Pg 39	However, the Contractor shall not be entitled to any extension of time where the instructions or acts of the Employer or the Engineer are necessitated by or "Inclement Weather Condition" intended to cure any default of or breach of Contract by the Contractor or where any delay is due to "Inclement Weather Condition"	Bidder seeks that Contractor shall be entitled to extension of time due to Inclement Weather Condition"
10	Vol 2, GCC, Clause 8.5, Liquidated Damages for Delay, Pg 41		Bidder seeks deletion of this clause

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	Engineer's Reply
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or	Not agreed
to	
n	As per the tender conditions
	Not agreed

S.No	Reference Volume/ Clause/ Page no of tender documents	Reference to tender document clause	Queries	Engineer's Reply
11	Vol 2, GCC, Clause 10.3 Extension of Contract Period, Pg 43	The Contract Period shall be extended by a period, after the Works are taken over, during which the Works or any Section or item of Plant, Rolling Stock, cannot be used, for the purposes for which they are intended, by reason of a defect or damage.	Bidder seeks that the actual Period of Extension must be clearly defined. It cannot be for an infinite period.	No change in bidding conditions.
12	Vol 2, GCC, Clause 10.5, Removal of Defective Work, Pg 44	If the defect or damage is such that it cannot be remedied expeditiously on the Site and if the Employer gives consent, the Contractor may, remove from the Site for the purposes of repair any part of the Works, which is defective or damaged. This consent may require the Contractor to increase the amount of Performance Security by the full replacement cost of these items or to provide other appropriate Security acceptable to the Employer	Bidder seeks that Employer may not increase the amount of the Performance Security by the full replacement cost of the defective or damaged Plant if such damage or defect is not attributable to the Bidder.	Not agreed
13	Vol 2, GCC, Clause 10.11, Emergency Defect Rectification, Pg 45	If any defect or damage, is one requiring immediate attention from safety, environmental or operational viewpoint, the Engineer has the authority to proceed with rectification in any manner suitable and deduct such sums from the Contract Price.	Bidder seeks that if defect or damage is not caused by the Contractor, the Engineer may not deduct sum from the Contract Price.	Not agreed
14	Vol 2, GCC, Clause 13.3.1, Notice of Termination by the Contractor, Pg 56	The Contractor may give notice requiring the Employer to remedy the default within 28 days after receipt of the notice. If the Employer fails to remedy the default or fails to propose steps reasonably acceptable to the Contractor to do so and in that case, the Contractor may terminate the Contract after issue of 14 days' notice to the Employer with a copy to the Engineer. In this case, the Contractor shall be compensated as per Sub clause 13.3.4. The Engineer's decision on the certified amount payable on this account shall be final and binding.	Bidder seeks deletion of this clause "The Engineer's decision on the certified amount payable on this account shall be final and binding."	Not agreed



S.No	Reference Volume/ Clause/ Page no of tender documents	Reference to tender document clause	Queries	Engineer's Reply
15	Vol 2, GCC, Clause 13.3.5, Payment on Termination, Pg 57	In case termination/foreclosure of the Contract under whatsoever circumstances, any remaining Tools, Plants, Equipment's and surplus materials of Employer with Contractor will be returned to the Employer in good condition at Employer's depot at Contractor's cost. In case of the failure of the Contractor to do so, the Employer will be entitled to recover their cost from the Contractor from the amount becoming due to the Contractor or from any other money due in any other Contracts. The decision of the Engineer of the amount to be recovered will be final and full credit at rates initially charged to the Contractor shall be allowed for such materials. Similarly, the Employer shall be entitled to recover the cost of the unreturned material, Plant, Equipment and Tools from theContractor where such material has been supplied free of cost or on lease basis to the Contractor as stipulated in the Conditions of Contract.	Bidder seeks that, the Amount to be recovered from the Employer shall be decided by the Contractor and seeks deletion of the clause "The decision of the Engineer of the amount to be recovered will be final and full credit at rates initially charged to the Contractor shall be allowed for such materials".	Not agreed
16	Vol 2, GCC, Clause 14.1, Indemnity, Pg 58	Risk and Responsibility All sums payable by way of compensation under these conditions shall be considered reasonable compensation payable to the Employer, without reference to the actual loss or damage sustained, and whether or not any damage shall have been sustained. The decision of the Engineer as to compensation claimed shall be final and binding.	Bidder seeks that, "The Decision of the Engineer as to compensation claimed shall not be final and Binding."	Not agreed
17	Vol 2, GCC, Clause 16.6, Resumption of Work, Pg 62	The obligations under the Contract shall be resumed as soon as practicable after the event has come to an end or ceased to exist. In case of doubt or dispute, whether a particular occurrence should be considered an "event" as defined under this Clause, the decision of the Engineer shall be final and binding.	Bidder seeks that the decision of the Engineer shall not be final and binding.	Not agreed
18	Vol 2, GCC, Clause 17.6, Conciliation, Pg 63	The Conciliation shall be undertaken by one Conciliator selected from a panel of Conciliators maintained by the Employer. The Conciliator shall assist the Parties to reach an amicable settlement in an independent and impartial manner.	Bidder seeks that "the Conciliator shall be appointed mutually"	Not agreed
19	Vol 2, GCC, Clause 17.7, Conciliation Procedure, Pg 63	There will be no objection if Conciliator so nominated is a serving employee of JMRC who would be Deputy HOD level officer and above.	Bidder seeks deletion of this clause.	Not agreed



Procedure for Appointment of Arbitrators: n case of Sole Arbitrator : Within 60 days from the day when a written and valid demand for Arbitration is received by MD,JMRC, the Employer will forward a panel of 03 names to the Contractor. The Contractor shall have to choose one Arbitrator from the panel of three, to be appointed as Sole Arbitrator within 30 days of dispatch of the request by the Employer. In case the Contractor fails to choose one Arbitrator within 30 days of dispatch of the request of the Employer then MD,JMRC shall appoint any one Arbitrator from the panel of 03 Arbitrators, as sole Arbitrator. Procedure for Appointment of Arbitrators: n case of Three Arbitrator: a) Within 60 days from the day when a written and valid demand for Arbitration is received by MD,JMRC, the Employer will orward a panel of 5 names to the Contractor. The Contractor will then give his consent for any one name out of the panel to be appointed as one of the Arbitrators within 30 days of dispatch of the request by the Employer. b) Employer will decide the second Arbitrator for whom consent was given by the Contractor, within 30 days from the receipt of the consent for one name of the Arbitrator. In case the Contractor fails to give his consent within 30 days of dispatch of the request of the Employer. b) Employer will decide the second Arbitrator for whom consent was given by the Contractor, within 30 days from the receipt of the consent for one name of the Arbitrator form the Contractor. In case the Contractor fails to give his consent within 30 days of dispatch of the request of the Employer then MD,JMRC shall nominate both the Arbitrators from the panel. C) The third Arbitrator shall be chosen by the two Arbitrators to appointed by	of arbitrators suggested by the Employer.
 h case of Three Arbitrator: a) Within 60 days from the day when a written and valid demand for Arbitration is received by MD,JMRC, the Employer will brward a panel of 5 names to the Contractor. The Contractor will then give his consent for any one name out of the panel to be appointed as one of the Arbitrators within 30 days of dispatch of the request by the Employer. b) Employer will decide the second Arbitrator. MD,JMRC shall appoint the wo Arbitrators, including the name of one Arbitrator for whom consent was given by the Contractor, within 30 days from the receipt of the consent for one name of the Arbitrator. In case the Contractor fails to give his consent within 30 days of dispatch of the request of the Employer then MD,JMRC shall nominate both the Arbitrators from the panel. 	mutually by the parties without any reference to the panel of arbitrators suggested by the Employer. There shall be three arbitrators and each party shall nominate one arbitrator and the two appointed
the Parties out of the panel of 05 Arbitrators provided to Contractor or from the arger panel of Arbitrators to be provided to them by Employer at the request of two appointed Arbitrators (if so desired by them) and who shall act as Presiding Arbitrator. In case of failure of the two appointed Arbitrators to reach upon consensus within a period of 30 days from their appointment date, then, upon the request of either or both Parties, the Presiding Arbitrator shall be appointed by the Managing Director, JMRC.	
 (C) The Contractor will replace free of cost to the Employer any defect or failure of equipment provided in the Works for a period of 36 months from the date of Taking Over of the last Section of the Works. (D) The Contractor agrees that any design modification be required to any section or component due to any defect; the period of 36 months shall re- commence from the date when the modified part is commissioned into service, and such modification shall be carried out free of cost to the Employer in all sub- systems and systems for all sections. 	Bidder seeks that the replacement period for defect or failure of equipment for a period of 36 months at free cost is exorbitant. Bidder seeks that the Design Modification for any defect shall be made at free of cost and maintenance for a period of 36 months is exorbitant.
n	 any defect or failure of equipment provided in the Works for a period of 36 months from the date of Taking Over of the last Section of the Works. (D) The Contractor agrees that any design nodification be required to any section or component due to any effect; the period of 36 months shall re-commence from the date when the modified part is commissioned into service, and such modification shall be carried out free of cost to the

	Engineer's Reply
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S.No	Reference Volume/ Clause/ Page no of tender documents	Reference to tender document clause	Queries
23	Vol 2, GCC, Appendix C, Clause 3 Contractor Warranty, Pg 75	Insofar as the copyright or other intellectual property rights in any plans, calculations, drawings, documents, materials, plant, know- how and other information relating to the Works shall be vested in the Contractor, the Contractor grants to the Employer his successors and assigns a royalty free, non- exclusive and irrevocable licence (carrying the right to grant sub-licences) to use and reproduce any of the works designs or inventions incorporated and referred to in such documents or materials and any such know-how and information for all purposes relating to the Works or the Mass Rapid Transport System.	Bidder seeks that Contractor shall not grant to the Employe a non-exclusive irrevocable and royalty- free licence (carrying the right to grant sub-license) to use, repair, copy, modify, enhance, adapt and translate in any form such Software for his own use.
24	Vol 2, SCC, Clause 17.9 Arbitration, Pg 18	Arbitration Sub-Clause 17.9.2 (i) In case of Sole Arbitration: Within 60 days from the day when a written and valid demand for arbitration is received by Director Projects, JMRC on behalf of MD, JMRC, the Employer will forward a panel of 03 names to the Contractor. Sub-Clause 17.9.2(ii)(a) Within 60 days from the day when a written and valid demand for arbitration is received by Director Projects, JMRC on behalf of MD, JMRC, the Employer will forward a panel of 05 names to the Contractor.	 Bidder seeks that any dispute arising from the contract shall be referred to arbitration and the arbitrators will be appointed mutually by the parties without any reference to the panel of arbitrators suggested by the Employer. In case of Sole Arbitrator, the Arbitrator shall be appointed mutually between the Parties. In case of Arbitration with three Arbitrators: Each Party shall appoint one Arbitrator and the two appointed arbitrator shall appoint the presiding arbitrator.
25	Vol3/ Employer's Requirements/Function al	2.8 Construction Depot and Dumping Yard	Kindly provide the dimensions and topography of casting yard land for layout planning
26	Vol3/ Employer's Requirements/	Appendix 2A Works Areas	Kindly provide the work area drawing at Station & Ramp Location
27	Vol3/ Employer's Requirements/	Appendix 2B Contract Key Dates and Completion Date	Kindly modify the start of TBM Initial Drive KD-6 to 45w & KD -7 to 51w since date provide currently is difficult to construct shaft & procure TBM's in short span
28	Tender Drawings		Kindly provide CAD file of the Tender drawing for ease of working
29	Tender Drawings		Kindly confirm whether contractor can adopt segmental tunnel lining as universal ring
	(Project VAIPUE	(1) *,*	of 35

	Engineer's Reply
er	Not agreed
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t	Not agreed
e	
all	
F	35000 sqm casting yard area shall be
	provided within lead of 45km. Please refer SN-21 of
	Addendum/Corrigendum No-01
	Please refer Appendix 2A of Employer
	Requirement
<u>s</u>	Will be as per the tender conditions
r	Not agreed
	Bidder may propose his own structure. It
	shall be approved by Engineer.

S.No	Reference Volume/ Clause/ Page no of tender documents	Reference to tender document clause	Queries	Engineer's Reply
30	Volume-4/ODS/Clause- 4.1/32	Outline Design Specification.	Train crush load data not available in tender document. Please clarify.	Please refer cl. 4.3.3 D of ODS for cut & cover of Tender documents
31	Volume-4/ODS/Clause- 4.1/32	Outline Design Specification.	Appendix for Ridership data not available in tender document. Please clarify.	As per loading pattern given in ODS, ridershi data is not required for design purpose
32	Volume-5/Bid drawing	Drawing number – JMRC-STN-RGC-TED-ARP-11001.	All entries - area is only available but permanent land take boundary is not available in tender drawings. Please clarify.	Permanent land is marked with hatch and RGC (Required Ground Coverage) is mentioned on the site level drawing (JMRC-STN-RGC-TED-ARP-11001)
33	Volume-3/Bid Document/Employers requirement- Appendix	Employers' requirement- Appendix	Space matrix for Underground station not available in tender document. Please clarify.	Room areas have been shown in layout plans in Tender Drawings .
34	Volume-5/Bid drawing	Drawing number – JMRC-STN-RGC-TED-ARP-13001.	Only OTE is showing in the cross section. UPE- Under platform extract is not shown in drawings. Please clarify	Tender Condition Prevails
35	Volume-5/Bid drawing	Drawing number – JMRC-STN-RGC-TED-ARP-11001.	All entries are open to sky in Badi Chaupar Metro station; can we consider the same for Ramganj Chaupar. Please clarify.	All entries are planned open to sky as station site is in the Heritage zone.
36	Volume-5/Bid drawing	Drawing number – JMRC-STN-RGC-TED-ARP-13001.	Platform screen door is not shown in section, can we consider there is not PSD in platform Level. Please clarify.	PSD are not considered.
37	Volume-5/Bid drawing	Drawing number – JMRC-STN-RGC-TED-ARP-13002.	In the section drawing below concourse false ceiling a line is indicated, please clarify if it is smoke down stand.	Yes it is
38	Volume-4/ODS/Clause- 4.1/32	Outline Design Specification.	Since it is a Design and construction. Standards for Station architectural works (queuing length, passenger handling, Emergency Evacuation from Public Areas, Platform design standards, Concourse design standard, Escalator, stairs, lift design standards etc.) is not available in the tender document. Please clarify.	Please refer Vol. V. No change in bidding condition
	CL Director (Project) JAIPUR		standards etc.) is not available in the tender document.	

S.No	Reference Volume/ Clause/ Page no of tender documents	Reference to tender document clause	Queries	Engineer's Reply
39	Volume-3/Employer's Requirements/Function al/Clause – 2.1/Page 18	Restoration of Heritage Kund as per direction of the employer	Kindly, share the detail drawings of Ramganj Chaupar Intersection fountain details & Heritage Kund for the purpose of planning and costing for reinstatement.	Bidder may visit site
40	Volume-3/Employer's Requirements/Function al/Clause – 8/Page 27	Entrances and all other points of access to the underground stations and tunnels shall be adequately protected against flooding. Levels shall be maintained considering HFL in that area. The critical parameters for this proposed and other design purposes shall be either Highest Flood Level (HFL) or Ground Level (G.L) whichever is higher in that area.	Kindly, share the HFL data for considering the same in fixing the height of podium level for Existing ground level.	Please refer CGWB website
41	Volume-5/Bid drawing	Tunnel Alignment Layout	The tunnel alignment is passing below the existing building at chainage 11+680 to 12+726m approx. Kindly, provide the foundation details of the existing building along the alignment & influence zone of tunnel.	Refer cl. 2.3 of Employer Requirement (detailed building condition survey is in the scope of contractor)
42	Volume-3/Employer's Requirement/Function al/Clause- 2.1 Scope under Lump Sum Price (Schedule A):/Page 15	Demolition/dismantling of any existing structures (below & above ground level), roads, footpath, RCC drain or any type of drain, kerb stone, pavers, central verge, boundary wall, grill, gate, railing, fencing, signage's, underground tanks, any overhead &underground utilities, street lighting, transformer, signaling system, bus shelters, public/private/religious structures and any other services etc. required for the work and disposal of same as directed by Engineer. bidder must visit the site and ascertain actual magnitude of quantum of work involved for road, footpath, RCC Drain or any type of drain, kerb stone, pavers, overhead & underground utilities, central verge, boundary wall, signage's, grill, gate railing, fencing, bus shelters, existing structures (below & above ground level) and any other services, etc., and nothing shall be payable on this account. Retrieved materials obtained from demolition/dismantling shall be property of the contractor.	The details of work area boundary and number of buildings to be demolished are required. Please provide.	please refer volume V and VII and also refer cl. 2.3 of Employer Requirement along with bidder may visit the site
43	Volume-3/Employer's Requirements/ Construction/Clause – 8. DAMAGE AND INTERFERENCE/Page 47	The alignment is passing near the heritage/protected monuments. The contractor shall ensure to protect these monuments during the construction of work.	Kindly, share the details of all the Heritage/monument buildings in the proposed alignment and the number of buildings to be protected during construction activity.	All the Heritage/monument buildings in the proposed alignment shall be protected and also bidder may visit site



S.No	Reference Volume/ Clause/ Page no of tender documents	Reference to tender document clause	Queries	Engineer's Reply
44	Volume-5/Bid drawing	Drawing No. GEN-JMRC-1C-ALG-TD-002-A1 (2 OF 4)	As per the General Arrangement drawings for Underground stretch it is mentioned that 2 Nos. of Entry Structures are "FUTURE ENTRY STRUCTURES". Kindly, clarify whether these Entry/Exit structures are in scope of current tender or not.	Please refer revised drawing no. GEN-JMRC- 1C-ALG-TD-002-R1
45	Volume III - Employer Requirement	The alignment is passing near the heritage/protected monuments	Kindly provide the details of heritage structures present all along the alignment.	Bidder may visit the site
46	Volume-V	GEN-JMRC-1C-ALG-TD-001, General Arrangement Drawing for Under Ground Stretch (Sheet 1 of 4)	Kindly provide the design drawing / as built drawing of the existing shaft at the start chainage of Phase-1C.	There is no existing shaft, Bidder may propose his own proposal . It shall be approved by Engineer.
47	Volume V	GEN-JMRC-1C-ALG-TD-002 to 004, General Arrangement Drawing for Under Ground Stretch (Sheet 2 to 4)	Beyond Chainage 11+560 towards ramp, existing ground levels details are missing. Kindly provide.	Please refer revised drawing no. GEN-JMRC- 1C-ALG-TD-002-R1, GEN-JMRC-1C-ALG-TD 003-R1 and GEN-JMRC-1C-ALG-TD-004-R1
48	Volume V	GEN-JMRC-1C-ALG-TD-002, General Arrangement Drawing for Under Ground Stretch (Sheet 2 of 4)	Proposed Ancillary building near Ramgunj Chaupar Station, is located at existing structure location. Kindly provide the structure details.	Refer cl. 2.3 of Employer Requirement (detailed building condition survey is in the scope of contractor). Bidder may also visit the site
49	Volume-V	GEN-JMRC-1C-ALG-TD-002 to 004, General Arrangement Drawing for Under Ground Stretch (Sheet 2 of 4)	Kindly provide the ROW details for Station, Shaft, Cut & Cover and Underground ramp.	Shall be as per existing rules of Local Authority
50	Volume V	CCV-JMRC-1C-STR-TD-14003, Open Ramp, Cut & Cover General Arrangement	Section B-B (roof slab with fill) indicated for the section in underground ramp, which shall be at the end of C&C cover. Please clarify.	Please refer revised drawing no. CCV-JMRC- 1C-STR-TD-14003-R1
51	Volume V	Drawing number GEN-JMRC-1C-ALG-TD-001, Page Number 04 of 06	It is not mentioned whether the vertical Alignment details provided is with respect to UP Line or DN Line. Kindly provide the alignment details with respect to both UP Line, DN Line.	general aranagement drawing is related to alignment detail
52	Volume V		It is seen that the curve between Chainage 12+345 to 12+660 has a radius of only 210 m, which seems to be critical, and radius is lesser than common metros alignment radius. Kindly suggest alternatives if possible.	the radius of curve is for alignment which is as per SOD.

S.No	Reference Volume/ Clause/ Page no of tender documents	Reference to tender document clause	Queries
53	Volume V	Drawing number GEN-JMRC-1C-ALG-TD-004, Sheet Number 04 of 04	The launching shaft details are given in the drawing. But there is no mention of retrieval shaft. Kindly provide details regarding how and where the TBMs are to be retrieved.
54	Volume V	Drawing number GEN-JMRC-1C-ALG-TD-004, Sheet Number 04 of 04	Kindly provide the width of cut and cover and underground ramp portions.
55	Volume V	JMRC-STN-RGC-TED-ARP-11005	Is there any structure connection between utility gallery and entry / exit RGC-2. Kindly clarify.
56	Volume-V; Volume-VII	GEN-JMRC-1C-ALG-TD-001 to 004, General Arrangement Drawing for Under Ground Stretch (Sheet 1 to 4); Topographical Survey Report, JMRC-BICP-TPN-00-DWG, Plan and Profile	The ground levels mentioned in the alignment drawings and the topographical survey for the respective chainage do not match. Kindly clarify which reduced levels should be followed.
57	Volume-VII	Geotechnical Investigation Report	Kindly provide any geotechnical investigation data for chainage 12+490 to 13+040, if available.
58	Volume-VII	Topographical Survey Report, JMRC-BICP-TPN-00-DWG, Plan and Profile	The topography survey report for chainage 12+440 to 13+040 is missing. Kindly provide the same if available.
59	Volume-VII	Topographical Survey Report, JMRC-BICP-TPN-00-DWG, Plan and Profile	Kindly provide the dilapidation report for buildings beneath which the tunnel alignment is crossing.
60	Volume VII	Geotechnical report	Employer shall provide rock core pictures (if any available) from the sub soil investigation carried out.
61	Volume VII	Geotechnical report	In case of rocks, UCS/Point load index values are not provided. Kindly provide if available.
62	General	-	Kindly provide the Key plan for the project alignment
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	Engineer's Reply
ire	Retrieval of TBM shall be as per construction proposal from contractor and approved by Engineer
	The width of cut and cover and underground ramp portion shall be as per the requirement of SOD and minimum width of walkway
ţy	The connection is not necessary, to be provided as per detailed design.
9	Please refer revised drawing no. GEN-JMRC- 1C-ALG-TD-001-R1, GEN-JMRC-1C-ALG-TD- 002-R1, GEN-JMRC-1C-ALG-TD-003-R1 and GEN-JMRC-1C-ALG-TD-004-R1
1	Please refer Addendum/ Corrigendum No 01
	Please refer Addendum/ Corrigendum No 01
ath	Refer cl. 2.3 of Employer Requirement (detailed building condition survey is in the scope of contractor)
	Please refer Addendum/ Corrigendum No 01 for Rock Core Picture.
ot	Due to poor quality and minimal core recovery, UCS/ Point Load test were not required on the rock samples as per the codal guidelines.
	kindly refer GAD is available in Vol. V bidding document

S.No	Reference Volume/ Clause/ Page no of tender documents	Reference to tender document clause	Queries	Engineer's Reply	
63	General	-	Kindly provide the location details of cross passages and number of cross passages along the tunnel with and without sump.	Follow NBC-2016 for number of cross passages, Exact location will be as per site conditions.	
64	General	-	Kindly provide the centre-to-centre distance between the tunnels.	minimum center to center distance of bored tunnel shall be two times the outer diameter of Tunnel	
65	General	-	It is seen that along the either side of the alignment, there are many densely spaced buildings. Furthermore, for a small stretch, the tunnel path will pass under these buildings. Hence kindly provide the foundation details of these existing buildings.	Refer cl. 2.3 of Employer Requirement (detailed building condition survey is in the scope of contractor) and bidder may also visit the site	
66	General	_	Please provide building survey details along the alignment.	Refer cl. 2.3 of Employer Requirement (detailed building condition survey is in the scope of contractor) and bidder may also visit the site	
67	General	-	Kindly provide Design Basis Report for Bored tunnel and cut and cover tunnels.	bidder may refer to Chapter 4 & Chapter 5 of ODS.	
68	ITB - C18 Bid fee/ bid document cost - Page 14	 (1) In case of open competitive bidding, two-stage bidding, rate contract, electronic reverse auction, bid security shall be 2% or as specified by the State Government of the estimated value of subject matter of 	We request employer for clarification on the no. of stages in bidding as It was mentioned single Stage on Bid document cover.	It is single stage 2 envelope bidding process	
69	GCC - Clause 1.5 Definition and Interpretation - Page 10	 1.5 Priority of Documents a) The Contract Agreement; b) The Letter of Acceptance; c) Pre and Post bid proceeds d) Form of Bid e) BOQ/Payment schedule f) NIB g) ITB h) The Outline Design Specifications (Design Criteria) and Outline Construction Specifications; or any other specification i) Drawings j) The Employer's Requirements k) The Special Conditions of Contract; l) The General Conditions of Contract; m) The Contractor's Proposal; and n) Any other document forming part of the Contract. 	We request employer to shift Contractor's Proposal next to LOA.	Not agreed	
	Director (Project) * JAIPUR 12 of 35				

S.No	Reference Volume/ Clause/ Page no of tender documents	Reference to tender document clause	Queries	Engineer's Reply		
70	GCC - Clause 1.10 Definition and Interpretation - Page 12	1.10 Compliance with Statutes, Regulations and Laws The Contractor shall be bound to give all notices required by statute, regulations or bye-laws, as aforesaid and to pay all fees and bills payable in respect thereof. The Contractor will arrange necessary clearances and approvals before the Work is taken up.	We request employer to provide the list of approvals to be procured by the Contractor and request the employer to provide necessary assistance for acquiring such approvals.	Will be dealt as per tender condition		
71	GCC - Clause 2.2 - Page 12	2.2 The Employer shall grant the Contractor right of access to, and / or possession of, the Site progressively for the completion of Works. Such right and possession may not be exclusive to the Contractor. If the Contractor suffers delay from failure on the part of the Employer to grant right of access to, or possession of the Site, the Contractor shall give notice to the Engineer in a period of 28 days of such occurrence. After receipt of such notice, the Engineer shall proceed to determine any extension of time to which the Contractor is entitled and shall notify the Contractor accordingly. For any such delay in handing over of site, Contractors will be entitled to only reasonable extension of time and no monetary claims, whatsoever shall be paid or entertained on this account.	We request employer to 1) Request to provide timelines for Access to site. 2) Request to provide the status of % of land acquired and the sequence of handing over of land. Along with EOT, kindly provide the Prolongation cost.	Will be dealt as per tender condition		
72	GCC - Clause 4.2 - Page 16	(4) Enhanced performance security for variation: If the original contract price increased either by due to contractor's or due to employer's variation, the 10 % amount shall be deducted from the each running bill equal to amount of variation of the original contract price.	We request employer to provide refund details of Enhanced performance security.	Please refer cl. 4.2.3 of GCC		
73	GCC - Clause 4.12 - Page 22	4.12 Rights of way and Facilities The Employer will acquire and provide land for Permanent Works and right of way (within JMRC's land) for access thereto over routes established by the Contractor. The Contractor shall bear all cost and charges for special or temporary rights of way which he may require including those for access to the Site.	We request employer. i) To provide the date of right of way To get clarification regarding the % of land acquired.	Will be dealt as per tender condition		



S.No	Reference Volume/ Clause/ Page no of tender documents	Reference to tender document clause	Queries	Engineer's Reply
74	GCC - Clause 4.23 Page 25	If, during the execution of the Works, the Contractor shall encounter physical conditions, which, in his opinion, could not have been reasonably foreseen by an experienced Contractor, the Contractor shall forthwith give written notice thereof to the Engineer and if, in the opinion of the Engineer, such conditions could not have been reasonably foreseen by an experienced Contractor, then the Engineer may certify and the Employer may pay reasonable additional cost []	We request employer to include reasonable EOT upon inspection of the site condition.	Please refer clause 8.4.1 (g) of GCC
75	GCC - Clause 8.1 Page 39	8.1 [] The Contractor shall not commence the construction, manufacture or installation of the Works or of any part of the Works unless and until the Engineer has endorsed the relevant Working Drawings in accordance with the Employer's Requirements.	We request employer for Timelines for Engineer approvals.	Will be dealt as per tender condition
76	GCC - Clause 8.4.2 Page 40	8.4.2 The Contractor shall not be entitled to an extension of time by reason of any delay to any activity in carrying out of the Works unless in the opinion of the Engineer such delay results in or may be expected to result in a delay to completion of the Works, or achievement of any Stage by the relevant Key Date. Whether or not the Contractor fails to achieve any Milestone by reason of any delay shall not by itself be material to the Contractor's entitlement to an extension of time.	We request employer for EOT for delay not attributable to the Contractor.	Will be dealt as per tender condition
77	GCC - 8.5 Page 40	8.5 Liquidated damages for Delay Time is the essence of the Contract. Appendix-1 to the Form of Bid shall include in respect of the Works and in respect of any Stage, a percentage of the total Contract value which will be recoverable from the Contractor as Liquidated Damages for delay in completion of the Works or in achievement of a stage by a particular Key Date. []	We request employer for refund of LD after achieving subsequent milestones.	Will be dealt as per tender condition



S.No	Reference Volume/ Clause/ Page no of tender documents	Reference to tender document clause	Queries	Engineer's Reply
78	GCC - Clause 8.5 Page 40	8.5 Liquidated damages for Delay [] The aforesaid Liquidated Damages do not, however, include the sums payable by the Employer to Designated Contractors on account of delay caused by the Contractor to Designated Contractors. Such sums shall be recoverable from the Contractor in addition to any Liquidated Damages payable under this clause, the total ceiling limit of which is 15% of the Contract value including Liquidated Damages levied under the provision of Appendix 1 to the Form of Bid.	We request employer to delete this "Such sums shall be recoverable from the Contractor in addition to any Liquidated Damages payable under this clause, the total ceiling limit of which is 15% of the Contract value including Liquidated Damages levied under the provision of Appendix 1 to the Form of Bid"	Will be dealt as per tender condition
79	GCC - Clause10.1 - Page 43 Completion of Outstanding Work and Remedying Defects	10.1 Completion of Outstanding Work and Remedying Defects [] Provided that, if any part of the Works or sub- systems or component of that part has been replaced, renewed or repaired except minor repair, the "Defects Liability Period" in respect of that part or sub-system or components of that part shall start from the date such replacement, renewal or repair has been completed to the satisfaction of the Engineer.	We request employer to confirm that replacement or repairs shall be performed only until Defect liability period.	As per tender condition
80	GCC - Clause10.9 - Page 44 Performance certificate	10.9 Performance Certificate [] Contractor would continue to remain liable to the Employer for any cost, loss, damage or compensation which arises from hidden or latent defect in the work executed by the Contractor under the Contract, even if such hidden and latent defects arise after the expiry of Defect Liability period or grant of Performance Certificate by the Employer[]	We request employer to provide the duration of latent defect period.	As per tender conditions
81	GCC -Clause 10.10 Page 44 Unfulfilled Obligations	10.10 Unfulfilled Obligations After the Performance Certificate has been issued, the Contractor and the Employer shall remain liable for the fulfilment of any obligation, which remains unperformed at that lime.	We request employer to correct the word "lime" to "time"	Please refer Addendum/ Corrigendum No 01
82	GCC - Clause 11.6 - Page 49 Payment of Interim and Final	11.6 Payment of Interim and Final After preliminary scrutiny and certification by the Engineer, payment of 80% of the certified interim amount shall be made by the Employer within 15 working days as far as possible. [] The balance 20% shall be paid within 28 working days as far as possible, from the date of the preliminary certification of the bill by the Engineer.	We request employer for interest in case of delayed payment.	As per tender conditions



S.No	Reference Volume/ Clause/ Page no of tender documents	Reference to tender document clause	Queries	Engineer's Reply		
83	GCC - Clause 12.1 Variations - Page 53	12.1 (4) e) An amount of 20% of items B.(i) a), b), c) and d) above to allow for Contractor's overheads including water/electricity charges and labour cess etc., profits and corporate taxes etc. No such percentage shall be applicable to the estimated cost of Materials supplied free of cost to the Contractor.	We request employer. i) request clarification for sub clause B(i) because such clause doesn't exist. It is presumed that GST is applicable over and above.	 (i) Please refer SN 20 of Addendum/ Corrigendum No 01 (ii) Yes, GST is over and above. However, while deriving the rates of such items the base rate of individual component shall be taken exclusive of GST. 		
84	GCC- Clause 13.2.1 Conditions leading to Termination of Contract - Page 54	 13.2.1 The Employer shall be entitled to terminate the Contract if the Contractor or any one of its constituents, (g) fails to adhere to the agreed programme of work by margin of 10% of the stipulated period or 21 days, whichever is earlier, or fails to complete the Works or parts of the Works within the stipulated or extended period of completion, or is unlikely to complete the whole Work or part thereof within time because of poor record of progress; or 	We request employer for clarification weather such 10% will be calculated for individual Key dates or after the project completion period.	Individual Key Dates		
85	GCC- Clause- 17.7 Conciliation Procedure Page 63	17.7 Conciliation Procedure [] There will be no objection if Conciliator so nominated is a serving employee of JMRC who would be Deputy HOD level officer and above.[]	We request employer to delete this Clause and request to nominate retired employee of JMRC.	Not agreed		
86	SCC - 4.9 Site Data - Page 04	[] The Bidder should satisfy himself with the data furnished and make his own investigations, if required, for submitting his offer. Any change in design or construction methodology later during execution on account of change will be borne by the Contractor. []	by Employer, the Contractor can be eligible for payment.	Not agreed (The bidder has mentioned PCC in place of SCC)		
87	SCC - 5.3 Submission of Documents - Page 10	Where the consent of the Engineer is required, the Engineer shall notify the Contractor in writing of his decision either within such period as may expressly be stipulated in the Contract or otherwise within a reasonable time.	We request employer to confirm the review period as 21 days as mentioned in Clause 5.3 GCC.	As per the tender conditions (The bidder has mentioned PCC in place of SCC)		



S.No	Reference Volume/ Clause/ Page no of tender	Reference to tender document clause	Queries		
5.140	documents	Reference to tender document clause	Queries		
88	SCC - 11.1.3 Price variation - Page 13	V = VI + Vs + Vc + Vf + Vm V = Total adjustment on account of all factors VI = Adjustment on account of labour component Vs = Adjustment on account of Steel component Vc = Adjustment on account of Cement component Vf = Adjustment on account of Fuel/Lubricant component Vm = Adjustment on account of Machinery and Equipment	Request to provide Adjustment for Aggregates also.		
89	SCC - 11.1.3 Price variation - Page 16	 (iv) Price Variation during Extended Period of Completion In case the indices increase above the indices applicable to a bill made on the last date of original completion period or the extended period under Sub- Clauses 8.4.1 of GCC, the price adjustment for the period of extension under Sub-Clause 8.4.3 of GCC will be limited to the amount payable as per the indices applicable to a bill made on the last date of the original completion period or the extended period under Sub-Clauses 8.4.1 of GCC as the case may be. In case the indices fall below the indices applicable to a bill made on the last date of the original completion period or the extended period under Sub-Clauses 8.4.1 of GCC, then the lower indices will be adopted for Price Adjustment for the period of extension under Clause 8.4.3 of GCC 			
90	SHE - 20.6 Installation of CCTV Cameras - Page 49	20.6 Storage back-up of minimum 15 days to be ensured at all times, failing which penalty shall be imposed.	We request employer for details regarding Penalty.		
91	Employer requirements - General - 11 (iv)Construction Interface - Page 8	The preparation of appropriate traffic diversion scheme for the work and its approval from the respective authorities/agencies shall be in the scope of the contractor.	We request employer to provide necessary assistance for procuring such approvals.		



	Engineer's Reply
)_	Please refer cl. 20 of SCC where Cost Coefficient of Steel is mentioned. For adjustment of aggregated not agreed (The bidder has mentioned PCC in place of SCC)
<u>า</u>	As per tender condition
	(The bidder has mentioned PCC in place of SCC)
y.	refer SHE cl. 56
	Employer assistance shall be provided as per tender condition

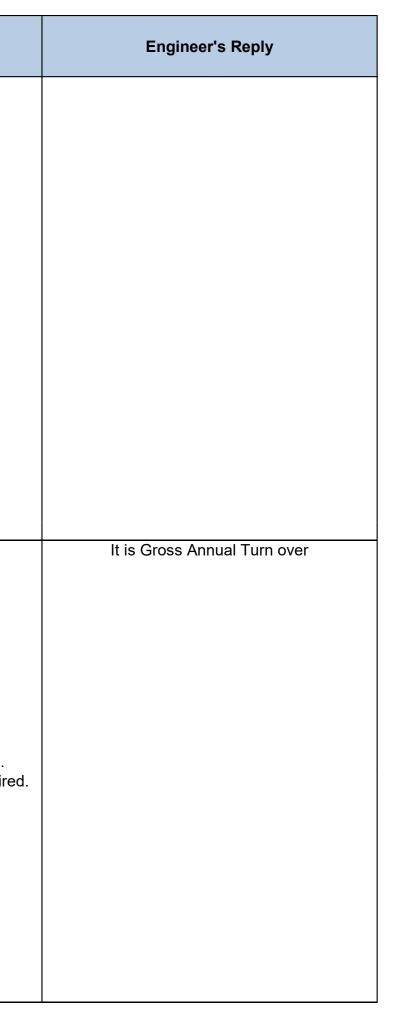
	Reference Volume/			
S.No	Clause/ Page no of tender	Reference to tender document clause	Queries	Engineer's Reply
	documents			5 17
92	Employer requirements - General - TREES - Page 48	The felling of trees is governed by the Rajasthan Forest Department. The Contractor is not permitted to cut any trees without the permission of the Employer. The Employer has assessed the number of trees existing within the right-of- way and will arrange permission from Forest Department cutting back or removal of trees which are deemed to be affected by the right of way (i.e., within the limits of permanent works) construction works. Contractor shall facilitate/liaison with the respective department. The trees requiring to be felled, will be removed from ground level up by the Contractor prior to commencement of the works. The Contractor will not be permitted to cut or remove any further trees. [] The payment of tree cutting, removal, transportation required in this item shall be paid extra in Schedule 'B'.	Please make a note of it. And request for EOT in case of delay In obtaining permissions.	Will be dealt as per tender condition
93	Employer requirements - General - Appendix 12 Utilities - Page 145	The Contractor shall take into consideration time taken for utility diversions into overall programme for the contract. However the efforts shall be made to avoid shifting/disturbance of any utility and try to work by supporting the same but the required services being provided by these utilities shall be maintained at all the times at the cost of the contractor.	We request employer for necessary Cost and time compensation in case of Uncharted utilities.	Will be dealt as per tender condition
94	FORM OF BID – APPENDIX-1 [REQUIREMENTS UNDER GENERAL CONDITIONS OF CONTRACT] Page 6	Amount of Performance Security - 10% of the Contract Price in types and proportions of currencies in which the contract price is payable.	We request employer to reduce performance security requirement to 3-5% of the contract price.	Not agreed
95	FORM OF BID – APPENDIX-1 [REQUIREMENTS UNDER GENERAL CONDITIONS OF CONTRACT] Page 6	Liquidated Damages - (ii) The maximum limit of Liquidated Damages shall be 10% of the total Contract Value.	We request employer to reduce LD Cap to 5% of contract Value	Not agreed



S.No	Reference Volume/ Clause/ Page no of tender documents		Reference to tend	er document clause	Queries	
96		C12.1 The Bid) a s profes propos	As this is the tendering stage and as bidder is alread required to provide multiple undertakings for the provision of project-personnel with the required qualifications and experience during execution after award, we request employer to ask for Resumes/CVs of only the Key-Staff Mentioned in the Annexure-3 of ITB at page 56 of 132 of the pdf file "Vol1NIB_ITB_FOBE-proc" at the tendering stage			
		S.No.	perience of such Project personnel is Designation of Project Personnel	given under Annexuré-4. Minimum no. of Project- Personnel required	Penalty on Non- Deployment per month per person	
			Kev Staff			
		1.	Project Manager (Team Leader)	1	Rs. 5 lakh/month for Expatriates* &Rs 3.0 lakhs for Local exper	
		2.	Deputy Project Manager (Tunnels & Underground station)	2	Rs 2.00 lakhs/month	
		3.	Deputy Project Manager (Casting Yard)	1	Rs 2.00 lakhs/month	
		4.	Interface Manager	1	Rs 2.00 lakhs/month	
		5.	Planning Engineer	1	Rs 2.00 lakhs/month	
		6. 7.	Structural/Design Engineer Quality Assurance Engineer	1	Rs 2.00 lakhs/month	
		8.	Chief Safety Manager	As per Conditions of contract on Safety & Health and Environment	As per Conditions contract on Safety Health ar Environment	
	Instruction to Bidders – C12.1 Staffing Schedule and Related Details Pg 33 + Annexure-3 [As per clause C12.1] MINIMUM ORGANISATION STRUCTURE REQUIRED Pg 56 of 132 +	Prog ii) We prov	confirm to deploy project-personne gramme agreed by the Engineer in to confirm to deploy minimum manp vided in Conditions of Contract on apower over and above the minimur	erms of Sub-Clause 4.13 of Ge ower as per Safety & Health Safety & Health and Environm n manpower stated above, if th	CC. and Environment Org ent. We also confirm	
	Undertaking Pg 58 of 132 +					
	Undertaking Pg 61 of 132					of 35

	Engineer's Reply
ady	Not agreed
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e df age.	

S.No	Reference Volume/ Clause/ Page no of tender documents	Reference to tender document clause					Queries		
					UNDER	RTAKING:			
		i) qu	We confirm to deple ualification & experience	oy project- e.	personnel	as per the	above-ment	ioned minim	lun
		0	We confirm to deploy rganization as require nvironment.	y manpowe ed under	er requirem Conditions	ent of Safety of Contract	& Health a on Safety	nd Environm & Health a	ier an
					SIG	NATURE OF	AUTHORIZ	EDSIGNATO	R
								LF OF BIDD	
97		FORM OF BID-APPENDIX 18 FINANCIAL DATA (FINANCIAL STANDING) Applicant's legal name							
				Year 2018-19	Year 2019- 20	Year 2020-21	Year 2021-22	Year 2022-23	
		1	Total Assets			e			
		2	Current Assets						
		3	Total External Liabilities		<u>.</u>	r			
	FORM OF BID-APPENDIX	4	Current Liabilities					a	The item no. 11 "Gross Annual" seems incomplete.
		5	Annual Profits Before			e 9 - 9		10	We request employer to clarify on the parameter required
	FINANCIAL DATA Pg 30		Taxes Annual Profits After						
		7	Taxes Net Worth [=1-3]						
		8	Working Capital [=2- 4]						
		9	Return on Equity						
		10.	Annual turnover (from construction work)					Sello Rell Col	
	RailCo	11.	Gross Annual					Director (Project)	
	No Rail Co		ITRACT ICB No: JP/EW/1C(Under	ground)/03Vol-	1/FOB			30	
1	Director (Project								



S.No	Reference Volume/ Clause/ Page no of tender documents	Reference to tender document clause	Queries
98	Clause 2.2 of GCC Access to and Possession of the Site	The Employer shall grant the Contractor right of access to, and / or possession of, the Site progressively for the completion of Works. Such right and possession may not be exclusive to the Contractor.	Please specify the timelines within which the site shall be handed over.
99	Vol3/ Employer's Requirements/Functional 11. URBAN PLANNING FUNCTIONAL REQUIREMENTS	The Station Site Plans are based on the urban planning design carried out by the Employer and specific land acquisition plans have been submitted to the concerned govt. authority and to the concerned land owning agencies of Govt. of India/Rajasthan Govt., for approval.	Please provide the status of land acquisition for the project
100	Cl. 1.4 of Vol3/ Employer's Requirements/Functional	The Contractor shall be responsible for obtaining all necessary approvals from the relevant Public/Government/Local/Statutory or any agencies in the design and construction of the Works.	JMRCL being Government Authority is in better position to take approval from Public/Government/Local/Statutory or any agencies. Bidder request Employer to obtain all necessary approvals from the relevant Public/Government/Local/Statutory or any agencies for effective progress of work and avoid delays.
101	CI. 2.8 2.8 CONSTRUCTION DEPOT & DUMPING AREA Vol3/ Employer's Requirements/Functional	For casting yard, batching plant and other activities a plot of land of approx. 20,000Sqmapprox.will be made available by JMRC on as is where is basis within 25 Km from the work site free of cost	Please provide the tentative location of Casting Yard.



	Engineer's Reply
0	Will be dealt as per tender condition
ct.	For main station building land acquisition is not required. However, aquisition of land for ancillary building etc is under process.
o r	Will be dealt as per tender condition
	Please refer SN-21 of Addendum/ Corrigendum No 01

S.No	Reference Volume/ Clause/ Page no of tender documents	Reference to tender document clause	Queries	Engineer's Reply
102	Clause 8.5 of GCC	Time is the essence of the Contract. Appendix-1 to the Form of Bid shall include in respect of the Works and in respect of any Stage, a percentage of the total Contract value which will be recoverable from the Contractor as Liquidated Damages for delay in completion of the Works or in achievement of a stage by a particular Key Date. The total amount of Liquidated Damages in respect of the Works in all stages shall, however, not exceed the limit of Liquidated Damages stated in the Appendix to the Form of Bid. The aforesaid Liquidated Damages do not, however, include the sums payable by the Employer to Designated Contractors on account of delay caused by the Contractor to Designated Contractors. Such sums shall be recoverable from the Contractor in addition to any Liquidated Damages payable under this clause, the total ceiling limit of which is 15% of the Contract value including Liquidated Damages levied under the provision of Appendix 1 to the Form of Bid.	Bidder request the Employer to reimburse the LD levied towards a key date if the subsequent key date/completion of works is achieved timely.	Will be dealt as per tender condition
103	Cl. 11.2.1 (Mobilisation Advance) of GCC	In respect of works costing more than Rs. 50.00 Crore (Rs. Fifty Crore) only the JMRC will, if provided in bidding document and requested by the Contractor to make mobilization advance, payment to the Contractor (at 9% per annum interest compounded annually basis) to assist in defraying the initial expenses that necessarilybe incurred by the Contractor for mobilization. The total of such advance payments and the number & timing of instalments is stated here under-	Bidder request Employer to provide Interest Free Mobilization Advance.	Not agreed
104	Cl. 11.2.2 (Advance against Plant and Machinery) of GCC	Deleted	Bidder request Employer to provide interest free advance against Plant and Machinery of 5% of Contract Price.	Not agreed
105	FORM OF BID – APPENDIX-1 i. Amount of Performance Security	10% of the Contract Price in types and proportions of currencies in which the contract price is payable. In the event of variations during the execution of the contract which result in payments to the Contractor over and above the contract price, the Performance Security shall be adjusted in accordance with clause 4.2 of GCC.	Bidder request Employer to reduce the amount of Performance Security to 3% of Contract Price as per the standard practice in construction industry.	Not agreed
106	Clause 11.1.4 (Change in Taxes/Duty) of SCC		Bidder understands that there are no changes in the SCC and the Clause 11.1.4 of GCC is applicable. Please confirm.	Yes, understanding is correct

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S.No	Reference Volume/ Clause/ Page no of tender documents	Reference to tender document clause	Queries	Engineer's Reply
107	Bonus		In the event the Project Completion Date occurs prior to the Scheduled Completion Date, the Contractor shall be entitled to receive a payment of bonus being a standard practice in the construction industry. Bidder request Authority to introduce bonus clause in the contract agreement.	Not agreed
108	Submission Date	General	We request you to provide minimum 4 weeks of time for bid submission after final release of pre- bid clarifications and addendums if any.	Please refer SN-01 of Addendum/ Corrigendum No 01
109	GCC Cl. No. 4.2.4 Page No. 17 of GCC Gaurantees & Warranties	 Within 30 days of the date of Letter of Acceptance of the Bid, the Contractor shall submit to the Employer: (i) An Undertaking in the approved format from a Parent Company, the identity of which shall have been submitted in writing to the Employer prior to acceptance of the Bid and against which the Employer shall have raised no objection. (ii) A written Guarantee in the approved format from a Parent Company, the identity of which shall have been submitted in writing to the Employer prior to acceptance of the Bid and against which the Employer shall have raised no objection. (ii) A written Guarantee in the approved format from a Parent Company, the identity of which shall have been submitted in writing to the Employer prior to acceptance of the Bid and against which the Employer shall have raised no objection. (iii) A warrantee in the approved format from the Contractor. 	Generally the Parent Company guarantee & undertakings is mandatory for the bidders who draw technical and financial credentials of the parent company and such guarantees are not required for the agencies who are bidding on their own individual credentials. The Bidder is participating in the bid process based on its own individual capacity (both financial & technical) and hence Parent Company guarantee & undertakings are not required. Kindly confirm. You may kindly note that such requirements are never asked for, in tenders of other metros and Govt departments.	per GCC.
110	GCC Cl. No. 11.2 Page No. 46 of GCC Mobilization / Advance payment and Interest on advance	In respect of works costing more than Rs. 50.00 Crore (Rs. Fifty Crore) only the JMRC will, if provided in bidding document and requested by the Contractor to make mobilization advance, payment to the Contractor (at 9% per annum interest compounded annually basis) to assist in defraying the initial expenses that necessarily be incurred by the Contractor for mobilization.	The interest cost will be part of bidder's estimate, will increase the quoted price. We request you to amend the clause as follows. The Authority shall make an <i>Interest free mobilisation</i> <i>advance</i> , to ease the project cash flow. Also, Interest free advances are adopted by various metro rail clients.	Not agreed



S.No	Reference Volume/ Clause/ Page no of tender documents	Reference to tender document clause	Queries
111	Employer's Requirements/ Functional Cl. No. 2.8 Page 24 Construction Depot & Dumping area	For casting yard, batching plant and other activities a plot of land of approx. 20,000 Sqm approx .will be made available by JMRC on as is where is basis within 25 Km from the work site free of cost.	 Bidder requests to provide a plot of land of <i>atleast. 60,000 sqm</i> for the casting yard and batching plant setup <i>within 20 km from the work site.</i> It is also requested to provide exact <i>location of Work area marked in Google Map</i> for ready reference. Also, please provide the handing over schedule of work area.
112	NIB Cl. 1.1.2 Page No. 3 Bid Security	Amount of Bid Security: INR 14.34 Crores (In favour of Jaipur Metro Rail Corporation Limited, payable at Jaipur , Rajasthan)	The amount of bid security as given in the reference tender clause amounts to 2% of the approximate cost of work which is unusual. Bidder requests to reduce the same to 1% of the project cost i.e. INR 7.17 crores
113	GCC CI. 8.5 & FOB Appendix 1 & Employer's Requirements Appendix 2B	Liquidated Damage for not achieving the key dates - 0.01% of the fixed lump sum price quoted in schedule "A" per week of delay for the key date.	Bidder requests to issue an amendment stating "Delay Damages levied will be refunded if the other key dates or overall completion date is adhered to". Kindly consider the same.
114	GCC Cl. 4.2 Performance Security Amount	The amount of performance security shall be five percent, or as may be specified in the bidding documents, of the amount of supply order in case of procurement of goods and services and ten percent of the amount of work order in case of procurement of works.	Bidder requests to consider the performance security as five percent of the amount of work order in case of procurement of works.
115	Volume 4 Part 1 Clause 4.3.12 Groundwater	Loads due to water pressure shall be calculated using a unit weight of 10 kN/m3 The Ground water table (Base value) shall be considered as maximum (in terms of RL) of Ground water table from a) data published by Central Ground Water board (CGWB), (b) Ground water table reported in Geotechnical report provided by JMRC in tender documents, (c) Ground water table reported in Geotechnical report provided by Design & Build contractor. The design Ground water table shall be taken as 4.0m higher than the Base value for evaluation of effects for design purposes during service stage.	Please provide data published by Central Ground Water Board.
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	Engineer's Reply
0 1	Please refer SN-21 of Addendum/ Corrigendum No 01
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er	Not agreed
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t	
	Will be delat as per tender condition.
s	
	Not agreed
	Please refer CGWB website

S.No	Reference Volume/ Clause/ Page no of tender documents	Reference to tender document clause	Queries
116	Volume 4 Part 1 Cl. No. 4.3.6 Seismic Loads Annexure 7 Load Combination	a) Load Combinations for ODE (Operating Design Earthquake) PGA for ODE: 0.075g b) Load Combinations for MDE (Maximum Design Earthquake): PGA for MDE: 0.15g	ODE & MDE value in the seismic loads and in combination is different. Kindly confirm which to follow.
117	Volume 4 Part 1 Cl. No. 4.3.15 One Strut Failure		 Incase of splayed strut, is the failure considered for whole strut or the single splay. It is not possible to design the waler if the whole strut including splayed strut is considered as failure. Kindly clarify. Also, does one strut failure system applies for anchor/bolts system also?
	(Project AIPUF	t) ***	of 35

	Engineer's Reply
n	Please refer Page no. 81AR1 to 90R1 of ODS
ed	 Yes, condition to be checked for both the cases i.e failure of Splay and failure of complete strut. Yes

S.No	Reference Volume/ Clause/ Page no of tender documents	Reference to tender document clause	Queries	Engineer's Reply
118	Volume 4 Part 1 Cl. no. 4.3.2 Note-9	Live Load surcharge shall be minimum as 20 kN/m2 at ground level (fill depth greater than 1.3m) or from actual load dispersion in case it gets higher than 20 kN/m2 for the areas under roads etc.	As per Cl. 4.3.11 Live Load surcharge shall be considered as 24kPa for areas under road. There is discrepancy between Cl. 4.3.2 note-9 and Cl. 4.3.11. Please confirm which loading to be followed.	24kPa to be considered.
119	Employer's Requirements Appendix 2B Contract Key Dates & Completion Dates	KD-06 Start of initial drive TBM 1 - 35 weeks (8.1 months) KD-07 Start of initial drive TBM 2 - 45 weeks (10.4 months) KD-08 Completion of tunnel incl. Cross passages & 1st stage of track bed concrete - 90 weeks (20.7 months)	KD 06 & KD 07 - It is impossible for any TBM manufacturer to deliver the TBMs in such a short duration. They usually take minimum 12 months for the delivery of TBMs at EX work after the purchase order is placed. Delivery to EX work - 12 months Delivery to site - 1.5 months Assembly of TBM - 1.5 months Total months - 15.0 months Also, there is discrepancy in the Project duration which is 40 months and the final Key Date which is 36.8 months. Keeping in view of the above, we have proposed revised Key dates in Annexure-1. Please accept the same.	Not agreed for extension of KD06, KD07 and Annexure-1. Final KD23 & KD24 are self explanatory.
120	Volume V Drawings General	-	CAD files of the drawings shall be provided. This is required for technically sound and financially competitive bidding.	Not agreed



S.No	Reference Volume/ Clause/ Page no of tender documents	Reference to tender document clause	Queries	Engineer's Reply
121	Volume III ER - Functional 2.1 Scope under Lump Sump Price (Sch A)	(ii) Design and Construction of one underground station viz Ramganj Chaupar by Top down Cut & Cover method along with entry/exit structures and associated structures such as ancillary buildings, Utilities galleries, AC plants room, ASS rooms, TVF rooms, system rooms and all other rooms, shafts, pump houses, water tanks, diesel generator set room or enclosure, sumps etc. as shown in the bid drawings provided with bid documents. The layout/length of Utility Gallery connecting ancillary building(which is proposed inside the vacant area of Ramganj Chaupar police station compound)with Station Structure shown in the bid Drawings Is indicative, Contractor is required to submit its proposal indicating layout/design of this utility gallery during actual execution stage for approval of The Employer and the cost of constructing the same will be considered to be included in quoted Lump Sum Price.	Since the Architectural design is not in scope of the Contractor, the Contractor shall propose the layout for the utility gallery considering structural and construction feasibility only for Client's approval.	Will be dealt as per tender condition
122	Volume III ER - Functional 2.1 Scope under Lump Sump Price (Sch A)	-	All Architectural and MEP drawings will be provided by the DDC appointed by the Client.	Will be dealt as per tender condition
123	Volume III ER - Functional 8. Operational Requirements		Since Architectural and MEP drawings will be provided by Client, the provisions of this clause do not apply to the Contractor.	Will be dealt as per tender condition



S.No	Reference Volume/ Clause/ Page no of tender documents	Reference to tender document clause	Queries	Engineer's Reply
124	Volume III ER - Functional 8. Operational Requirements	 (v) In the design and construction of the Works, the Contractor shall, as a fundamental objective and as a priority, ensure that passengers, staff and the public will, throughout the operational period of the Jaipur MRTS, and within the confines thereof, be provided with safe environment as is reasonably possible. The Contractor's attention is drawn to Clause 13 of this Employer's Requirements . Functional, concerning the role of the Commissioner of Metro Railway Safety (CMRS). (vi) The design of the works shall be such that the Forecast Passenger Flows can be met without congestion occurring and without risk to the safety of passengers or metro employees including during any emergencies. Exits and passages, in particular. should be suitably designed and provided. (vii) Escalator pits shall be designed to enable drainage by gravity flow system. However, where length of the drainage is exceptionally long, the pumping system may be considered subject to approval of Engineer. Installation of pumps is not in the scope of th is contract. 	Since Architectural and MEP drawings will be provided by Client, the provisions of this clause do not apply to the Contractor.	Will be dealt as per tender condition
125	Volume III ER - Functional 9. Functional Requirements of Pumping Installations	 9. FUNCTIONAL REQUIREMENTS OF PUMPING INSTALLATIONS (i) Water pump installations shall be designed for unmanned operation, controlled through liquid level controllers, capable of pumping the requisite amount of waler lo the ulili or lo the ground I over head tanks. (ii) The pumping installation shall withstand the corrosive effects of normal waler supply, seepage waler and sewage and serve for !he anticipated life of !he equipment. The discharge velocity for sewage I seepage pumping shall not be less than 0.751/sec. (iii) The pipe line size should be such lha! !he velocity head does not exceed !he normal static head except for the fire pump which is governed by separate criteria. The valve controls and regulating mechanisms shall be designed for automatic operation. 	Since Architectural and MEP drawings will be provided by Client, the provisions of this clause do not apply to the Contractor.	Will be dealt as per tender condition
126	General		It is requested to the Employer to provide details of existing Badi Chaupar UG station including tunnel details towards the start of the alignment.	Please refer Bid Drawing No GEN-JMRC-1C- ALG-TD-001
127	Volume-V Alignment GAD	GEN-JMRC-1C-ALG-TD-002/003/004	No Ground Level is mentioned from CH:11580 to CH:12700. Please provide the same	Please refer revised drawing no. GEN-JMRC- 1C-ALG-TD-002-R1, GEN-JMRC-1C-ALG-TD- 003-R1 and GEN-JMRC-1C-ALG-TD-004-R1
128	Volume-V Alignment GAD	GEN-JMRC-1C-ALG-TD-001/002/003/004	The drawings are not clearly visible. Better quality PDF requested	Please refer revised drawing no. GEN-JMRC- 1C-ALG-TD-001-R1, GEN-JMRC-1C-ALG-TD- 002-R1, GEN-JMRC-1C-ALG-TD-003-R1 and GEN-JMRC-1C-ALG-TD-004-R1
129	Volume-V Alignment GAD	GEN-JMRC-1C-ALG-TD-001/002/003/004	Please provide .kmz of alignment for a better understanding of the area	Not agreed
	(Project VAIPUS	28	of 35	

S.No	Reference Volume/ Clause/ Page no of tender documents	Reference to tender document clause	Queries	Engineer's Reply
130	Volume-V General	General	Please provide the acad version of the drawings	Not agreed
131	Volume-VII Topo Survey Report	JMRC-BICP-TPN-00-DWG, Sheet 1 & 2	Ground Level mentioned in L-section is not matching with Alignment GAD provided in Volume-5. In some places, Rail Level also not matching. Please issue the correct Alignment GAD based on Topo Survey Drawings	Please refer revised drawing no. GEN-JMRC- 1C-ALG-TD-001-R1, GEN-JMRC-1C-ALG-TD 002-R1, GEN-JMRC-1C-ALG-TD-003-R1 and GEN-JMRC-1C-ALG-TD-004-R1
132	General	General	Please provide Utility drawings for Station, Tunnel and C&C stretch	please refer Vol. VII
133	General	General	Please mention, if there are any Historical Structure, Structures of special interest, Railway Crossings, Flyover, Underpass, Foot over Bridge, or Water bodies falling inside the influence zone	Bidder may visit the site
134	Volume-V Instrumentation Drawings	INT-JMRC-1C-STR-TD-15001/15002/15003/15004	Please confirm, Contractor understood those drawings are for reference/tender purposes only and the Contractor will produce his own drawings during detailed design and there is no requirement to follow those tender drawings blindly	Will be dealt as per tender and site condition
135	Volume-IV ODS/OCS, Appendix-18, SOD	Schedule of Dimension, SOD	Please provide the latest SOD	attached SOD is latest.however any update / revision in SOD is issued by Ministry of Railways/RDSO/JMRC etc shall also be applicable.
136	Volume-III ER, Appendix-15	Real Time Monitoring	Please provide a scheme/guidelines for real-time monitoring	Tender condition prevails.
137	Volume IV, 4 ODS for Cut & Cover Clause 4.3.12	Ground Water	Please provide the CGWB data of the groundwater table	please refer CGWB website
	Director (Project)			1

JAIPUR

S.No	Reference Volume/ Clause/ Page no of tender documents	Reference to tender document clause	Queries
138	Volume-IV :5 ODS for Bored Tunnel, Clause 5.3	Tunnel Lining Segment	Instrumentation and monitoring to demonstrate the performance of the installed linings". Contractor seeking clarification, if they need to install any instrumented segment. Please provide guidelines
139	Volume-IV :5 ODS for Bored Tunnel, Clause 6.5.2	Load Factor and Combinations	Load factors of 1.5 applied to ground & water load in the combination of 2. DL+EQ seems to be on the higher side. Please check.
140	Volume IV, 5 ODS for Bored Tunnel, Clause 2.7.18	Cross Passage	For the allowable crack width for the NATM tunnel, reference shall be made to IS-456, please confirm.
141	Volume IV, 5 ODS for Geotechnical Works	Tunnel Profile Construction Methods	Change in the spacing between the tunnels determined by numerical analysis may change the horizontal alignment.
142	Volume IV, 6 ODS for Geotechnical Works, Clause 2.3	Other Ground- Investigation Methods	Full-Scale groundwater pumping tests shall be performed only in case the water is encountered in the borehole. In the Geotechnical investigation data available, no groundwater is encountered up to the drill depth in any of the boreholes.
143	Volume IV, 6 ODS for Geotechnical Works, Clause 3.1	(a) Tunnel Seismic Prediction (TSP) & (b) Geo-Electrical Real-Time Ground Prediction while TBM Boring:	These tests to predict the geological condition ahead of the cutter head shall be performed depending on the site constraint and requirement. Please modify the clause.
144	Volume V, Section S.14 OCS for Civil Works, Clause 14.5.3, Sub Clause 15.5.3.3	Final Tunnel Support (NATM Tunnel Support)	Please specify the minimum grade of concrete for the permanent lining of the NATM Tunnel.
145	Volume V, Drawings TUN-JMRC-1C-STR-TD- 14002	Details of TBM segment Lining	Can a universal segment ring arrangement be considered? Please confirm.



	Engineer's Reply
	Scheme for Instrumentation and Monitoring of Tunnel Lining segment shall be approved by the Engineer.
).).	No change in bidding conditions.
	Confirmed
y 	the alignment is fixed however, if any changes are proposed because of design requirement during construction phase same may be approved by Engineer.
d is	No change in bidding conditions.
ie	Not agreed
	M35
?	Yes however, Bidder may propose his own structure. It shall be approved by Engineer.

S.No	Reference Volume/ Clause/ Page no of tender documents	Reference to tender document clause	Queries
146	1.1.3.1 Eligible Applicants: vii. Page 8	LEAD PARTNER / NON-SUBSTANTIAL PARTNERS / CHANGE IN JV / CONSORTIUM a. Lead partner must be a substantial partner in the JV / Consortium i.e it should have a minimum of 26% participation in the JV / Consortium. Each substantial partner in case of JV / Consortium shall have experience of executing at least one "similar work" of value of minimum 40% of NIB value in last 07 years.	We request the Authority to review the eligibility requiremen as mentioned herein and amends the eligibility criteria of each substantial partners as requested below:- Lead partner must be a substantial partner in the JV / Consortium i.e it should have a minimum of 26% participation in the JV / Consortium. Each substantial partner in case of JV / Consortium shall have experience of executing at least one work (Any Civil Infrastructure work) o value of minimum 40% of NIB value in last 07 years. Please do the needful as requested above.
147	1.1.3.2 Minimum Eligibility Criteria: Page 11 - 12 of 20	 A. Work Experience: The Bidders will be qualified only if they have successfully completed similar work(s) during last seven years ending last day of the month previous to the month of Bid submission as given below: i. At least one "similar work"* of value of INR 573.78crore or more. OR ii. Two "similar works"*each of value of INR 358.62 crore or more. OR iii. Three "similar works"*each of value of INR 286.89 crore or more. *The "Similar works" for this contract shall be either A1 or A2. A1. "Tunneling work in urban environment by Shield TBM with finished internal diameter of minimum 5.0 mtr, along with or without underground station(s) (which may/may not include architectural finishing/E&M work) ". Additional Work Experience: Experience of having completed Tunneling work(s) in urban environment of minimum 02 KM Tunnel length put together from maximum of 03 Works by Shield TBM (in case of twin 	We request the Authority that in JV, any member of JV shal be allowed to meet the 100 % Technical Eligibility criteria as mentioned herein.



	Engineer's Reply
ent	Not agreed
of of	
all as	Not agreed

S.No	Reference Volume/ Clause/ Page no of tender documents	Reference to tender document clause	Queries
		 "A. Work Experience: The Bidders will be qualified only if they have successfully completed similar work(s) during last seven years ending last day of the month previous to the month of Bid submission as given below: i. At least one "similar work" of value of INR 573.78crore or more. OR ii. Two "similar works"*each of value of INR 358.62 crore or more. OR iii. Three "similar works"*each of value of INR 286.89 crore or more. 	
		*The "Similar works" for this contract shall be either A1 or A2. A1. "Tunneling work in urban environment by Shield TBM with finished internal diameter of minimum 5.0 mtr, along with or without underground station(s) (which may/may not include architectural finishing/E&M work)". Additional Work Experience: Experience of having completed Tunneling work(s) in urban environment of minimum 02 KM Tunnel length put together from maximum of 03 Works by Shield TBM (in case of twin tunnel, each tunnel shall be counted as a separate Tunnel for calculation of length of tunnel finished internal dia of minimum 5.0 mtr diameter either in Works under A above or any 03 Works irrespective of value of Works. AND	



Engineer's Reply

S.No	Reference Volume/ Clause/ Page no of tender documents	Reference to tender document clause	Queries
		 Experience of having completed at least one work of underground station either in Works under A above or any Work irrespective of value of Work (which may/may not include architectural finishing/E&M Works). OR A2. " A1. "Tunneling work in urban environment by Shield TBM with finished internal diameter of minimum 5.0 mtr, along with or without underground station(s) (which may/may not include architectural finishing/E&M work) ". Additional Work Experience: Experience of having completed Tunneling work(s) in urban environment of minimum 02 KM Tunnel length put together from maximum of 03 Works by Shield TBM (in case of twin tunnel, each tunnel shall be counted as a separate Tunnel for calculation of length of tunnel" 	
148	General	Due Date Extension	We are keenly interested to participate in the above bid, but looking into the clarity required for participation in bid as requested above and looking into the size and complexity of project, we request the Authority to please provide 4 weeks' time for submission of bid from the date of pre bid reply received from your end for submitting a comprehensive bid



	Engineer's Reply
, but as ty of eeks' oly e bid.	Please refer SN-01 of Addendum/ Corrigendum No 01

S.No	Reference Volume/ Clause/ Page no of tender	Reference to tender document clause	Queries
4.40	documents		
149	1.1.3.1, VII (a) of NIB, Volume-1 Eligible Applicants	Each substantial partner in case of JV/Consortiu m shall have experience of executing at least one "similar work" of value of minimum 40% of NIB value in last 07 years.	We presume that, in case of JV/Consortium, any member of the JV/Consortium can meet the said minimum technical criteria and all consortium members combinedly meet the entire PQ criteria. As the similar type of projects are rare and limited in our country, a very small number of entities will have the said criteria. For the departments such as CMRL (Chennai Metro Rail Limited) and UPMRC (Uttar Pradesh Metro Rail Corporation), It is predominantly stated as, the required criteria can be met by any one member or collectively in case of JV/Consortium. In view of the above we request you to change the condition i.e., each substantial partner in case of JV/Consortium shall have experience of Executing at least one similar work. And allow the JV/Consortium with collective accomplishment of PQ. So that, financially sound companies can also be partnered with technically skilled companies for participating in the tender, resulting in witnessing a competitive bidding for the said project
150	Clause 1.1.3.1, vii, b	"Each non-substantial partner should have a minimum of 20% participation in the JV/Consortium. Partners having less than 26% participation will be termed as non-substantial partner, and their financial soundness shall not be considered for the evaluation of JV/Consortium. In the Bid for Civil work, a Joint Venture / Consortium to qualify, each of its non- substantial partners must have experience of executing at least one civil work of minimum 20% of NIB value in the last 07 years. The Bidder shall submit details of the above works in the Performa of Appendix-17 & 17A of FOB as per Notes to Clause 1.1.3.2.A of NIB	1. We seek clarification on the term "Civil Work" mentioned in Clause 1.1.3.1, vii, b. According to our understanding, firms with experience in Civil Works such as Road Work, Highway Work, Flyover Work, Bridge Work, etc., would be eligible. Could you confirm if our understanding is correct? 2. Additionally, we would like clarification on whether the completion of a Road Project would be considered qualifying experience under Clause 1.1.3.1, vii, b.
151	General		. We also request clarification on whether the contracting authority approves subcontracting for this project. As we currently lack experience in Tunnel work, we are exploring the possibility of partnering with another contractor. Kindly inform us if the authority allows subcontracting and specify the percentage of work that can be approved for subcontracting

Engineer's Reply
Not agreed
 Civil Work is defined under volume 4 part 1 of Outline construction specifications for Phase1C & 1D of Civil Works.
2. Yes
for partnering Bidder may refer to NIB Clause vii and for subconrtracting Bidder may refer to GCC Clause 4.5 & SCC Clause 4

S.No	Reference Volume/ Clause/ Page no of tender documents	Reference to tender document clause	Queries	Engineer's Reply
152	NIB Clause 1.1.3.1 vii	 a. Lead partner must be a substantial partner in the JV / Consortium i.e it should have a minimum of 26% participation in the JV / Consortium. Each substantial partner in case of JV / Consortium shall have experience of executing at least one "similar work" of value of minimum 40% of NIB value in last 07 years. 	The above criteria is not alliowing enthusiastic bidders like us to participate in tendering for the subject project and hence limiting the competiiton. We request you to modify the criteria similar to other metro organozations like Chennai metro, MMRDA.	Not agreed
153	NIB Clause 1.1.3.1 vii	Work experience of only substantial partner (partner with share of more than 26% or more in JV/Consortium) shall be considered for the evaluation of JV/Consortium	We request to delete this clause	Not agreed

